

SUCCESS LAKE
Tule River, California

WATER CONTROL MANUAL

APPENDIX IV

To

Master Water Control Manual
Tulare Lake Basin, California

JANUARY 1982

DEPARTMENT OF THE ARMY
SACRAMENTO DISTRICT, CORPS OF ENGINEERS
SACRAMENTO, CALIFORNIA

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SUCCESS LAKE
TULE RIVER, CALIFORNIA

WATER CONTROL MANUAL

JANUARY 1982
REVISED DECEMBER 1987

Department of the Army
Sacramento District, Corps of Engineers
Sacramento, California

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SUCCESS LAKE

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PERSONNEL CONCERNED IN THE OPERATION OF SUCCESS RESERVOIR

	UNIT	OFFICE PHONE	NAME	HOME PHONE
<p>PROJECT OFFICE PORTERVILLE, CALIFORNIA</p>	<p>SUCCESS RESERVOIR</p>	<p>209-784-0215 (Porterville)</p>	<p>B. PROCTER PARK MANAGER</p>	<p>209-784-0575 (Porterville)</p>
<p>DEPARTMENT OF THE ARMY SACRAMENTO DISTRICT CORPS OF ENGINEERS SACRAMENTO, CALIFORNIA</p>	<p>DISTRICT ENGINEER</p> <p>RESERVOIR CONTROL SECTION</p> <p>HYDROLOGIC FACILITIES OPERATIONS BRANCH</p>	<p>916-440-2232*</p> <p>916-440-3405*</p> <p>916-440-3168*</p> <p>916-440-3167*</p> <p>916-440-2378*</p> <p>916-440-2112*</p> <p>916-440-2327*</p> <p>916-440-2305*</p>	<p>COL. A. E. WILLIAMS DISTRICT ENGINEER</p> <p>R. A. NEAL CHIEF</p> <p>C. D. MATLOCK</p> <p>M. E. VERKE</p> <p>J. T. JOHNSON</p> <p>M. L. HELM CHIEF</p> <p>A. E. SMITH, JR. CHIEF, OPERATIONS & MAINTENANCE SECTION</p>	<p>916-791-0478 (Roseville)</p> <p>916-487-2985</p> <p>916-967-4994</p> <p>916-687-7212</p> <p>916-961-1918</p> <p>916-652-5280</p>
<p>IRRIGATION INTERESTS</p>	<p>TULE RIVER ASSOCIATION c/o LOWER TULE RIVER IRRIGATION DIST. P.O. BOX 511 WOODVILLE PORTERVILLE, CALIFORNIA</p> <p>TULARE LAKE BASIN WATER STORAGE DIST. 1109 WHITLEY AVE. CORCORAN, CALIFORNIA 93212</p>	<p>209-784-2598 (Porterville)</p> <p>209-686-4716 (Tulare)</p> <p>209-992-4127 (Corcoran)</p>	<p>R. L. SCHAFER WATERMASTER</p> <p>B. GRAHAM MANAGER</p>	<p>209-733-1329 (Visalia)</p> <p>209-582-7603 (Hanford)</p>

FTS: SACRAMENTO 448-2000

NOTE: *BETWEEN 4:30 PM AND 7:45 AM, OR ON SATURDAY, SUNDAY OR HOLIDAYS USE 916-452-1535 (FLOOD SEASON ONLY)

SUCCESS RESERVOIR, TULE RIVER, CALIFORNIA

REV. 01-OCT-82



USACE Sacramento District Datum Documentation Report

Project: Success Lake and Dam

NGVD 29To NAVD 88 Datum Conversion Factor: add 2.61 ft.

Datum Conversion Procedure: The USACE Mapping Unit and A-E Contractor performed field measurements with known historical elevations. All documentation and raw data is filed with the USACE Sacramento District Mapping Unit. All survey and gage control is in US feet and is tied to NGS monument AC6136. For questions or comments contact the Sacramento District Datum Coordinator. The results of this survey produced an averaged difference between NGVD 29 and NAVD 88 of 2.61 feet for the USACE Success Lake and Dam civil works project.

Station ID	COE-NGVD29 record	NAVD 88	Difference
AC6136 (KT 200)	696.97	699.60	2.63
52	671.03	376.64	2.61
59	584.77	587.36	5.59
56	656.91	659.52	2.61
			Average = 2.61
Averaged Delta = 2.61ft conversion factor			

Accuracy Statement: The NAVD88 datum conversion accuracy is: ± 0.25 feet to real work NAVD 88 elevations per EC- 1110-2-6065 Comprehensive Evaluation of Project Datums. The stated conversion factor is for planning, operations, water management and legacy conversion only. All future design work and survey work shall adhere to the NAVD 88 datum and follow EM 1110-1-1005 Control and Topographic Surveying. Contact the USACE Sacramento District’s survey unit or the district’s datum coordinator for current survey control.

SUCCESS LAKE TULE RIVER, CALIFORNIA

PERTINENT DATA

GENERAL

Drainage areas

Tule River below Success Dam . . .	393.0 sq. mi.
S. Fork Tule River near Success . .	109.0 sq. mi.
Tule River near Springville	247.0 sq. mi.
N. Fork of M. Fork Tule River near Springville	39.3 sq. mi.

Flows at dam site

Mean annual (1904-1980)	137,400 ac-ft
Mean daily (1904-1980)	190 cfs

Max. mean daily recorded

inflow (6 Dec 66)	40,000 cfs
Max. instantaneous recorded inflow (6 Dec 66)	76,900 cfs
Standard project peak inflow . . .	67,500 cfs
Standard project peak outflow . . .	43,650 cfs
Spillway design peak inflow	200,000 cfs
Spillway design peak outflow . . .	126,000 cfs

RESERVOIR

Elevation

Inactive pool	559.0 feet
Flood control pool (bottom)	587.0 feet
Gross pool	652.5 feet
Taking line	658.0 feet
Spillway design flood pool	686.8 feet

Area

Inactive pool	83 acres
Flood control pool (bottom)	379 acres
Gross pool	2,477 acres
Taking line	2,832 acres
Spillway design flood pool	4,441 acres

Storage capacity

Inactive pool	557 ac-ft
Flood control pool (bottom)	6,540 ac-ft
Gross pool (nominal capacity)	82,300 ac-ft
Standard project flood pool	130,000 ac-ft
Spillway design flood pool	202,700 ac-ft

Reservoir length at gross

pool elev.	3.5 miles
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SPILLWAY (Uncontrolled Broad-Crested)

Location	In saddle near right abutment
Crest length	200 feet
Crest elevation	652.5 feet
Total excavation	
Head at gross pool	3.26 feet
Head at spillway design flood pool	34.3 feet
Max. capacity (SDF pool)	126,000 cfs

MAIN DAM (Earthfill)

Elevation, top of dam	691.5 feet
Freeboard, above spillway design flood pool	4.7 feet
Maximum height	142 feet
Length of crest	3,490 feet
Width of crest	22.5 feet
Width of roadway	16.0 feet
Upstream slope	1 on 3.75; 1 on 3.0; 1 on 2.5 at crest
Downstream slope	1 on 3.0; 1 on 2.5 at crest
Total excavation	490,000 cu. yds.
Total volume of embankment	4,900,000 cu. yds.

FRAZIER DIKE (Earthfill)

Elevation, top of dike	691.5 feet
Freeboard, above spillway design flood pool	4.7 feet
Length of crest	7,650 feet
Width of crest	20 feet
Width of roadway	16 feet
Maximum height	42 feet
Upstream slope	1 on 2.75
Downstream slope	1 on 2.75
Total excavation	67,000 cu. yds.
Total volume of embankment	660,000 cu. yds.

MAIN OUTLET

Conduit (concrete-lined tunnel)

Diameter	12.0 feet
Intake structure elev., invert	559.0 feet
Outlet elev., invert	551.0 feet
Length	687.0 feet

Gates (number and size)

Service gates (hydraulically operated slide)	2 - 5'8" x 10'0"
Emergency gates (hydraulically operated slide)	2 - 5'8" x 10'0"

Total capacity of outlets with water surface

At elev. 587.0 (6,540 ac-ft)	3,200 cfs
At elev. 652.5 (82,300 ac-ft)	6,300 cfs

PIONEER IRRIGATION DITCH OUTLET

Steel pipe (concrete encased)

Diameter	42 inches
Length	687.0 feet
Gross head	103.5 feet

Gates (number and size)

Service gate (double disc type gate valve)	1 - 42" diameter
Emergency gate (double disc type gate valve)	1 - 42" diameter

Total discharge capacity (full valve opening)

At elev. 560.0 (91 ac-ft)	75 cfs
At elev. 652.5 (82,300 ac-ft)	284 cfs



NOTICE TO USERS OF THIS MANUAL

Regulations specify that this Water Control Manual be published in looseleaf form, and only those sections, or parts thereof, requiring changes will be revised and printed. Therefore this copy should be preserved in good condition so that inserts can be made to keep the manual current.



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EXHIBIT

A. Standing Instructions to Damoperator

I - INTRODUCTION

1-01. Authorization. The Success Lake Water Control Manual, Tule River, California, is an Appendix to the Tulare Lake Basin Master Water Control Manual. It is prepared in accordance with instructions contained in EC 1110-2-208; EM 1110-2-3600, and ETL 1110-2-251.

1-02. Purpose and Scope. This manual provides a detailed plan for water control and management at the Success Lake project on the Tule River, California.

1-03. Related Manuals and Reports. This manual is Appendix IV to the Tulare Lake Basin Master Water Control Manual. Other related reports are as follow:

<u>Title</u>	<u>Date</u>
Master Water Control Manual	1 Dec 53
Tulare Lake Basin, California	
App I - Pine Flat Lake	Nov 53 (Rev. Sep 79)
App II - Isabella Lake	May 53 (Rev. Jan 78)
App III - Terminus Dam (Lake Kaweah)	Jun 62 (Rev. Nov 71) (Rev. Nov 81)
Maintenance Manual	Aug 63
Review of Spillway Adequacy	Nov 78
Definite Project Report	Dec 49
DM 1 - Spillway Design Flood	Nov 55
DM 2 - Dam & Appurtenances, 4 Volumes Report, App A and B & Plates	Jul 56
DM 3 - Real Estate	Apr 56
Supp 1 Real Estate	Jan 57
DM 5 - Reservoir Regulation	Dec 56
DM 6 - General Design	Jan 57 (Rev. 1 Dec 58)
DM 7 - Reservoir Clearing	Nov 57
DM 8 - Initial Public Use Facilities	Feb 61
DM 9 - Master Plan	Jun 61
DM 9B-C1 - Recreational Development at Areas 3, 4, and 10	Feb 64
DM 10 - Operators Quarters and Fallout Protection	Aug 62
Supp 1 Operators Quarters and Fallout Protection	Feb 67
DM 11 - Additional Recreation Development at Tule Recreation Area (Formerly Areas 3 and 4)	Nov 68
DM 12 - Master Plan	Dec 77

1-04. Project Owner. Success Lake is owned by the U.S. Government.

1-05. Operating Agency. The Sacramento District, U.S. Army Corps of Engineers operates Success Lake. Duties related to the control of outflows are performed by the Park Manager or by a designated Damoperator. The Park Manager has a normal tour of duty at the dam of eight hours per day, five days a week. At other times, the Park Manager may be contacted at his residence at the project. Project personnel will be on duty weekends and holidays and at other-than-normal working hours as necessary for effective

project operation. Operational responsibilities are explained in detail in Exhibit A. Business and home phone numbers of the individuals responsible for project operation are given at the beginning of this manual and at the beginning of Exhibit A.

1-06. Regulating Agencies. The operation plan for Success Lake for flood control was developed by the Corps of Engineers, Sacramento District, with the objective of gaining the greatest possible benefits from flood control, irrigation and recreation.

Releases for purposes other than flood control are directed by the Tule River Watermaster who represents the Pioneer Water Company, the Vandalia Irrigation District, Porterville Irrigation District, the Lower Tule River Irrigation District and the downstream Kaweah River and Tule River Associations. These organizations are known collectively as the Tule River Association. The Watermaster's work and home phone numbers are listed at the beginning of this manual and at the beginning of Exhibit A.

II - DESCRIPTION OF PROJECT

2-01. Location. Success Lake is located on the Tule River, California, about 6 miles east of Porterville, California. The project can be reached by driving east from Porterville on State Highway 190. Its location is shown on plate 1.

2-02. Purpose. Success Lake provides storage for flood control, conservation and other purposes.

2-03. Physical Components. The Success Project consists of a dam and reservoir on the Tule River. It intercepts the runoff from 391 square miles of mountainous area. Pertinent data for the project are tabulated at the front of this manual. A general site plan and recreation development are shown on plate 2. Success Dam is an earthfill structure with a maximum height of 142 feet and a length of 3,490 feet. The top of the dam at elevation 691.5, provides 4.7 feet of freeboard above the spillway design flood pool at elevation 686.8 feet. A plan and profile of the dam are shown on plate 3.

A rolled earthfill dike known as Frazier Dike, 42 feet high and 7,650 feet long extends across Frazier Valley about 3-1/2 miles northwest of the dam. A plan, profile and sections are shown on plate 4.

At normal full pool (elevation 652.5), the reservoir extends about 3.5 miles from the dam in an easterly direction. The capacity of Success Lake at normal full pool was originally 85,400 acre-feet, but sedimentation has reduced it to about 82,300 acre-feet. The area at normal full pool is about 2,477 acres. Area and capacity curves are presented on plate A-1, and a table of areas and capacities is presented on plate A-2.

The outlet works consist of one 12-foot circular conduit-type gated outlet with intake invert elevation at 559 feet and one 42-inch gated concrete-encased steel pipe under the main conduit, with invert elevation at 553 feet. The main outlet is controlled by two 5'8" x 10'0" hydraulically operated slide gates (with two 5'8" x 10'0" hydraulically operated emergency slide gates) and has a capacity of 3,200 c.f.s. at elevation 587 feet, at which the storage is 6,540 acre-feet. The rating curves for various gate openings for this outlet are shown on plate A-3. The smaller outlet takes off from the main outlet upstream from the slide gates. It is controlled by a 42" diameter double disc type valve service gate (with similar emergency gate) and has a capacity of 75 c.f.s. at pool elevation 560 feet, or 284 c.f.s. at gross pool elevation of 652.5 feet. This outlet serves Pioneer Irrigation Ditch which formerly diverted water from Tule River upstream from the damsite. A rating curve for Pioneer Ditch is shown on plate A-5. A plan, profile and sections of the control tower and outlet works are shown on plates 5 and 6.

The spillway is ungated and is excavated through overburden into the rock of a natural saddle about 900 feet from the right abutment of the main dam. It has a crest width of 200 feet and a safe discharge capacity of 126,000 cubic feet per second when the reservoir water surface is at spillway design flood pool (elevation 686.8 feet). A plan, profile, and sections of the spillway are shown on plate 7 and a rating curve is shown on plate A-4.

TABLE 2-01

RECREATION FACILITIES AT SUCCESS LAKE

Area	: Camp	: Picnic	: Launch	: Restroom Facilities			: Car-	: Parking
	: Sites	: Sites	: Lanes	: Flush	: Vault	: Portable 1/	: Car	: Trailer
Observation					1		20	
Tule	104 <u>2/</u>	31 <u>3/</u>	6 <u>4/</u>	7		24	50	200
Gill						6	160 <u>5/</u>	
Wildlife						2		
Rocky Hill	223 <u>5/</u>		2	1		24	50	125
Bartlett Park		54 <u>6/</u>		4				

4

- NOTES: 1/ Average. (More may be added if demand indicates).
2/ Includes 2 sites reserved for handicapped use.
3/ Includes 6 group sites (each group site will accommodate 20+ people).
4/ Six lanes available for high lake levels - 3 for low lake levels.
5/ Primitive.
6/ Includes 12 group sites. Group sites consist of 6 sites accommodating over 150 persons, and 6 sites accommodating 40-60 persons.
7/ Approximate figure. Parking is random along side of roads.

2-04. Related Control Facilities. The Success Project consists of the dam and reservoir and appurtenant facilities. No other improvements outside the reservoir area were made under the authority of this project. However, local interests have made channel improvements downstream.

2-05. Real Estate Acquisition. Project lands consist of approximately 4,116 acres acquired in fee, 57.8 acres under easement, and 0.2 acres under lease or permit. The minimum take line for this land is at elevation 658. The project land boundaries are shown on plate 2.

2-06. Public Facilities. Most recreation use of Success Lake presently occurs in and originates from the developed south and west shores of the lake and at Bartlett Park. Some use occurs at the undeveloped Gill area and in the partially developed wildlife management area. Success Lake has one of the best bass fisheries in the San Joaquin River Basin. Other recreation at Success Lake includes picnicing, camping, waterskiing, hunting, swimming, pleasure boating and sightseeing. In addition, opportunities for specialized activities such as hunting dog trials and horseback riding are also provided. Recreation facilities currently available at Lake Success are listed on Table 2-01 and the locations are shown on plate 2.

Accurate visitation records have been kept for Success Lake since 1964 when 603,200 recreation days were recorded. Annual visitation from 1964 through 1980 is as follows:

TABLE 2-02
ANNUAL VISITATION AT SUCCESS LAKE

1964	603,200
1965	568,050
1966	565,990
1967	400,960
1968	590,430
1969	533,300
1970	627,450
1971	549,890
1972	514,200
1973	691,340
1974	615,450
1975	775,280
1976	724,440
1977	696,750
1978	801,750
1979	569,840
1980	<u>933,500</u>
Mean	633,000

III - HISTORY OF PROJECT

3-01. Authorization. The investigation which led to the recommendation to construct Success Lake was authorized 22 June 1936. The project was authorized for construction by the 22 December 1944 Flood Control Act as follows:

"The Plan for Terminus and Success Reservoirs on the Kaweah and Tule Rivers for Flood Control and other purposes in the San Joaquin Valley, California, in accordance with the recommendations of the Chief of Engineers in Flood Control Committee Document Number 1, Seventy-eighth Congress, Second Session, is approved, and there is hereby authorized \$4,600,000 for initial and partial accomplishment of the plan."

3-02. Planning and Design. In Committee Document Number 1, 78th Congress, 2nd Session, dated 1944, the Chief of Engineers recommended a reservoir capacity of 50,000 acre-feet. However, subsequent studies made for the basic report indicated that, to provide adequate flood control, the storage capacity should be 115,000 acre-feet. The State of California and Tulare Lake interests questioned the economic feasibility of this increase. This is noted in the District Engineers report to the Chief of Engineers dated 1 June 1948. The report is in House Document 367, 81st Congress, 1st Session dated 1950.

Further investigations were made, and by letter of 6 July 1949, subject: "Preliminary Definite Project Report, Success Project, Tule River, California," the District Engineer transmitted a report recommending a capacity of 75,000 acre-feet, on the grounds that such capacity was necessary for flood control and that a larger capacity was not economically justified. The 75,000 acre-foot capacity was approved by the Chief of Engineers in 2nd endorsement dated 5 August 1949 to the basic letter of 6 July 1949. At a conference between representatives of OCE, SPD and the Sacramento District on 9 May 1956 it was decided to provide an additional 5,000 acre-feet of capacity for sedimentation reserve, which increased the planned total gross pool capacity to 80,000 acre-feet.

3-03. Construction. Construction funds were initially appropriated in fiscal year 1957 but relatively little was accomplished until fiscal year 1959 due to inadequacy of authorized funds. Construction on the main dam and appurtenances was begun during October 1958. Closure of the dam was initiated 4 April 1960 and was completed 20 January 1961. The project was certified complete and accepted by the Government for operation on 15 May 1961. State Highway 190 and the county road were relocated.

3-04. Related Projects. Success Lake is part of a system of reservoirs providing flood protection to Tulare Lakebed and adjacent areas. The other reservoirs are Pine Flat Lake, Lake Kaweah, and Isabella Lake. Kaweah River water may enter the Tule River via Elk Bayou.

The Friant Kern Canal crosses the Tule River approximately eleven miles downstream from Success Dam. It delivers irrigation water to the Tule River and has the potential to export flood waters if necessary.

Upstream and downstream control structures are discussed in paragraphs 4-10 and 4-11.

3-05. Modifications to Regulations. The flood control diagram in the original flood control manual dated June 1961 was based on a total reservoir capacity of 80,000 acre-feet: 75,000 acre-feet for flood control during the rain flood season and 5,000 acre-feet, below elevation 587, for silt and recreation purposes. However, after the project was constructed, it was found that the reservoir contained more than 80,000 acre-feet at gross pool (elevation 652.5). A November 1965 survey showed that the reservoir capacity at gross pool was actually 85,400 acre-feet and that 6,800 acre-feet of this capacity was below elevation 587. Since certain recreation facilities were installed based on that elevation it was decided to make the silt and recreation pool 6,800 acre-feet. The additional 3,600 acre-feet of space above elevation 587 was designated as winter flood control reservation when necessary to compensate for any decrease in irrigation and spreading demands. Additional surveys were made in 1978. The flood control diagram dated July 1981 in this manual is based on the 1978 survey. The current gross pool storage is 82,300 acre-feet and the storage below elevations 587 is 6,540 acre-feet.

The lines delineating the flood control space requirements during the rainflood season have been altered on the July 1981 diagram to more accurately portray the period of rainflood hazard.

The snowmelt operation requirements have been changed on the July 1981 diagram based on past operating experience and hypothetical routings of snowmelt floods (1906 to 1981). The objective of the snowmelt operation requirements is to minimize releases in excess of irrigation and spreading demand.

3-06. Principal Regulation Problems. Since completion of Success Lake, there have been no principal regulation problems. However, several large floods which included the largest rainflood of record (December 1966) and the second largest snowmelt flood of record (April-July 1969) have occurred. Operations during these floods demonstrated that Success Lake does not provide the degree of protection as presumed during the design stage. Discussions of these floods are covered in paragraphs 8.02c and d. Another potential regulatory problem is the high rate of sediment buildup in the reservoir. Sediments are accumulating at about twice the 1956 projected rate. Current projected deposition rates indicate that gross pool storage will be less than 75,000 acre-feet by the year 2020. Sediment deposition has a compound effect on the project by reducing available space for flood control, conservation, and recreation usage.

IV - WATERSHED CHARACTERISTICS

4-01. General Characteristics. The watershed above the dam is a fan-shaped mountainous area of about 391 square miles on the western slope of the southern Sierra Nevada. The Tule River is formed by three main forks flowing from the high eastern border of the basin in a southwesterly or westerly direction to their junction near the foothill line. The North, Middle, and South Forks are fed by numerous small streams with slopes ranging from 400 to about 1,000 feet per mile. The soil cover below 9,000 feet elevation ranges from moderate to deep. Vegetal cover is distributed approximately as follows:

TABLE 4-01

VEGETAL COVER ON TULE RIVER BASIN

Description	Elevation (ft. msl)	Percent of Basin Area
Grass lands (with scattered brush)	500- 3,000	9.3
Brush lands (chaparral, etc.)	2,500- 9,000	17.0
Deciduous forest (with brush, scattered conifers, and grass)	500- 7,000	48.9
Light coniferous	5,000-10,000	19.6
Heavy coniferous	6,000- 8,000	4.3
Sub-alpine forest	8,000-10,000	0.5
Bare rock	8,000-10,000	<u>0.4</u>
TOTAL		100.0

The area is sparsely settled and suitable for grazing, lumbering, mining, and recreation. More than half of the basin is within the Sequoia National Forest, and the southern portion of it comprises the Tule River Indian Reservation. The Tule River flows about 3 miles through low foothills below Success Dam and emerges on the valley floor near Porterville. There are no major tributaries between Success Dam and Porterville, the major potential damage area below the project. Porterville is located on the right bank of the Tule River.

Below Porterville the area becomes predominately agricultural along the river to Tulare Lakebed where the river terminates. Normally, diversions for agriculture cause the river to dry up before it gets to the lakebed.

4-02. Topography. The area above the dam is steep mountainous terrain. Below the dam there are foothills which transition into an alluvial fan and flatlands gently sloping to Tulare Lakebed. Elevations range from about 10,000 feet in the mountains to 550 feet at the dam, 450 feet at Porterville and down to 175 feet in Tulare Lakebed. The percent of area above various elevations is shown below:

TABLE 4-02

PERCENT OF AREA ABOVE GIVEN ELEVATIONS
IN TULE RIVER BASIN

<u>Elevation (feet)</u>	<u>Percent of Area Above Elevation</u>
550	100
2,000	75
4,000	45
5,000	33
6,000	22
8,000	5
10,050	0

A topographical map is shown on plate 8, an area elevation curve is shown on plate 9, and a stream profile is shown on plate 10.

4-03. Geology and Soils. The intrusion of the Sierra Nevada Batholith through metamorphosed sediments has created a complicated rock structure in the Tule River Basin. Glacial and stream erosion have cut deeply leaving large areas of exposed granite and roof pendants of metamorphosed rock. Alluvial deposits cover the narrow canyon floors and the wide alluvial fan where the Tule River emerges from the foothills onto the San Joaquin Valley floor. Lake deposits are found at the rivers terminus in Tulare Lakebed.

A number of minor faults are located within the basin area. Major faults nearby include the Garlock and San Andreas faults, within 90 miles, White Wolf fault within 75 miles and the Sierra Nevada and Pond-Poso faults within 50 miles.

4-04. Sediment. Storage space below elevation 587 feet has been reserved for sedimentation. A system of 27 sedimentation ranges was established by ground survey methods before reservoir operation was initiated. Two of these ranges cross the river below the dam, two above gross pool elevation on the river; and the remaining ranges are so spaced that no range represents more than 10 percent of the potential sediment accumulation in the reservoir. Each range is straight and is marked by a permanent monument above gross pool at each end. Each profile is recorded on a permanent drawing to a horizontal scale of 1 inch to 20 feet, with an attached table showing the coordinates of all survey points. The range locations are shown on plate 11. Reconnaissance surveys of the sedimentation ranges are made as deemed necessary; generally after major events. General surveys of the reservoir area have been made in 1960, 1965, 1967, 1968, 1973 and 1977. The surveys show that approximately 186 acre-feet of sediment per year has accumulated in Success Lake. In addition to surveys of the reservoir area, the sediment concentration of outflow from the reservoir is measured each month or at intermittent intervals from a one-gallon sample of outflow water taken immediately below the outlets of the dam. An estimate of sediment outflow of 4 acre-feet per year was computed from the 20 year record of outflow volume and the concentration of solid sediment indicated by sample measurements.

4-05. Climate. The valley area is characterized by hot, dry summers and moderate winters. At high elevations the summers are cool and the winters severe.

a. Temperature. Temperatures within the basin vary considerably. On the valley floor the summer highs go well over 100°F. while the winter lows may go below freezing. At the higher elevations, the summer highs are generally less than 100°F. while the winter lows may go below 0°F. The mean monthly and annual temperatures at three stations within or near the Tule River Basin are shown below:

TABLE 4-03

MEAN MONTHLY AND ANNUAL TEMPERATURES (°F)

Month	Success Dam (elev. 590)	Grant Grove (elev. 6600)	Three Rivers Edison PH #2 (elev. 950)
Oct	66.0	49.9	64.2
Nov	54.7	40.5	53.9
Dec	46.3	35.3	47.2
Jan	46.1	33.2	46.3
Feb	51.2	33.6	50.1
Mar	54.6	34.5	53.5
Apr	59.7	39.5	59.2
May	67.3	46.4	65.9
Jun	75.0	54.1	73.0
Jul	81.3	62.6	80.5
Aug	79.6	61.3	78.7
Sep	<u>74.3</u>	<u>57.0</u>	<u>73.8</u>
Mean	63.0	45.6	62.2

b. Precipitation. Normal annual precipitation (NAP) in the Tule River Basin varies from about 6-inches at the lowest elevation to about 50-inches at the headwaters. The NAP for the Basin above Success Reservoir is 31.0 inches. NAP isohyets for the area are shown on plate 12. Approximately 90 percent of the precipitation occurs in the period from November through April. It generally occurs as rain below 5,000 feet and as snow above that elevation. However, warm winter storms have produced rain up to 11,000 feet, which would cover the entire basin, and snow has occurred on the valley floor below the dam. The average monthly precipitation for representative stations is shown below:

TABLE 4-04

AVERAGE MONTHLY PRECIPITATION

Month	: Success Dam		: Eagle Creek		: Rogers Camp		: Mtn Home		: Hossack	
	in.	% Ann	in.	% Ann	in.	% Ann	in.	% Ann	in.	% Ann
Oct	0.65	5.8	1.89	5.0	1.00	2.9	1.33	3.2	0.95	2.2
Nov	1.56	14.0	3.73	9.9	3.15	9.1	3.64	8.7	4.28	10.1
Dec	1.55	14.0	7.49	19.9	6.94	20.0	7.13	17.1	7.71	18.3
Jan	1.99	17.8	8.05	21.4	7.86	22.6	8.71	20.9	8.92	21.2
Feb	1.84	16.5	5.61	14.9	5.42	15.6	6.97	16.7	6.14	14.6
Mar	1.58	14.2	5.06	13.4	5.31	15.3	6.29	15.1	6.40	15.2
Apr	1.15	10.3	2.94	7.8	2.69	7.8	4.69	11.2	4.12	9.8
May	0.45	4.0	1.19	3.2	0.95	2.7	1.46	3.5	1.91	4.5
Jun	0.08	0.7	0.51	1.4	0.40	1.2	0.80	1.9	0.61	1.4
Jul	0.02	0.2	0.27	0.7	0.26	0.7	0.18	0.4	0.16	0.4
Aug	0.07	0.6	0.22	0.6	0.12	0.3	0.13	0.3	0.21	0.5
Sep	0.21	1.9	0.72	1.9	0.62	1.8	0.44	1.0	0.74	1.8
TOTAL	11.15	100.0	37.68	100.0	34.72	100.0	41.77	100.0	42.15	100.0

c. Snow. Snow cover below 5,000 feet is generally transient and may accumulate and melt a number of times during the winter season. Above 5,000 feet, the snow generally accumulates until March when the melt season begins. Snowpack data for 1969, 1975, and 1977 representing wet, normal, and dry years is shown below:

TABLE 4-05

1 APRIL SNOW PACK DATA FOR 1969, 1975 AND 1977

Index:	#	: Snow Course:	: Elev. in ft.:	: Record Began	: Depth in Inches			: Water Content in Inches		
					: 1969:	: 1975 :	: 1977 :	: Ave. : 1/ :	: 1969 :	: 1975 :
247	Quaking Aspen	7,000	1937	97.5	48.5	1.3	13.9	44.7	17.7	0.5
248	Old Enterprise Mill	6600	1937	95.8	52.6	1.6	16.9	44.4	20.8	0.5
244	Hockett Mdw.	8500	1930	144.2	107.4	20.3	28.8	71.6	31.6	6.5
264	Quinn Ranger Station	8350	1930	128.1	68.2	4.6	20.4	59.6	22.3	2.0

1/ Average for 1931-1981 period.

d. Evaporation. Monthly evaporation rates are shown below:

TABLE 4-06
HISTORICAL MONTHLY EVAPORATION
SUCCESS LAKE

Month	: Mean Evaporation (in.) 1/	: Standard Deviation (in.)
January	1.1	.28
February	1.5	.29
March	2.7	.51
April	4.3	.91
May	6.6	.78
June	8.2	.80
July	10.4	.76
August	10.0	1.11
September	7.9	.94
October	5.6	.91
November	2.6	.68
December	<u>1.2</u>	.37
Total	62.1	

1/ Average for 1960-1981 period.

e. Wind. The average monthly wind movement at Success Lake is shown below:

TABLE 4-07
HISTORICAL MONTHLY WIND MOVEMENT
SUCCESS LAKE

Month	: Mean Wind Movement (miles) 1/	: Standard Deviation (miles)
January	961	236
February	963	264
March	1,095	291
April	1,082	267
May	1,154	259
June	1,186	253
July	1,207	224
August	1,148	269
September	1,052	266
October	1,010	313
November	917	244
December	<u>949</u>	263
Total	12,724	

1/ Average for 1964-1981 period.

4-06. Storms and Floods. Flood flows on Tule River are of two types, winter rain floods and spring snowmelt floods. The winter-type floods are characterized by sharp high peaks and small volumes and are usually of short duration, seldom lasting more than four days. These winter floods normally occur during the period November through March and are caused by intense rains sometimes augmented by snowmelt at the lower elevations. The largest rain flood of record on Tule River at Success Dam was that of December 1966. Flows during the 6 largest rain floods of record follow:

TABLE 4-08
MAXIMUM INFLOW TO SUCCESS LAKE

Date of Peak	Peak :(Average Flow in c.f.s)	Peak : 1-Day	Peak : 3-Day	Peak : 7-Day	Peak : 15-Day	Peak : 30-Day
6 Dec 1966	76,900	40,000	18,300	8,700	4,300	2,300
19 Nov 1950	28,000*	15,500*	8,100*	3,700*	2,100*	1,100*
23 Dec 1955	27,000	13,600	6,100	3,300	1,800	1,000
25 Jan 1969	24,000	12,900	7,400	4,600	3,300	2,100
9 Mar 1943	21,000*	14,200*	8,600*	4,400*	3,700*	2,700*
3 Jan 1980	17,000	8,700	7,200	4,100	2,300	1,600

*Determined by correlation with Tule River near Porterville.

Flows during the 5 largest snowmelt floods of record follow:

TABLE 4-09
MAXIMUM INFLOW TO SUCCESS LAKE DURING SNOWMELT SEASON

Water Year	1-Day	15-Day (Average Flow in c.f.s.)	30-Day	60-Day	90-Day	120-Day
1906	3,560*	2,100*	1,920*	1,700*	1,690*	1,330*
1969	1,560	1,270	1,220	1,200	1,000	830
1938	1,650*	1,160*	1,140*	1,050*	1,040*	800*
1909	1,270*	1,180*	1,120*	1,020*	1,000*	780*
1967	1,740	1,250	1,080	980	840	690

*Determined by correlation with Tule River near Porterville.

4-07. Runoff Characteristics. Stream gage locations are shown on plate 8, a stream profile is shown on plate 10 and historical unimpaired flow below Success Dam is shown on plate 13. The flows on plate 13 from 1904 through 1953 have been estimated based on upstream gages. Runoff data at 3 of the upstream gages follows:

TABLE 4-10

RECORDED RUNOFF DATA

	Tule River near Porterville	Tule River near Springville	SF Tule River
Period of Record	1901-1960	1958-Present	1930-1954; 1956-Present
Drainage area sq. mi.	261	247	109
Instantaneous flow, c.f.s.			
Maximum	25,500 (Nov 1950)	49,600 (Dec 1966)	14,300 (Dec 1966)
Minimum	0 (More than 1 Year)	0 (More than 1 Year)	0 (More than 1 Year)
Mean daily flow, c.f.s.	138	292	42
Instantaneous flow, c.s.m.			
Maximum	97.7	202	131
Minimum	0	0	0
Mean daily flow, c.s.m.	0.53	1.18	0.39
Annual flow, acre-feet			
Maximum	340,000 (1905-06)	366,200 (1967-69)	122,000 (1968-69)
Minimum	13,900 (1930-31)	12,870 (1976-77)	2,330 (1976-77)
Mean	101,400	106,700	29,900
Annual flow, inches			
Maximum	24.4	27.80	21.0
Minimum	1.0	0.98	0.40
Mean	7.28	8.10	5.14
April-July flow, acre-feet			
Maximum	192,300 (1906)	169,100 (1969)	48,500 (1969)
Minimum	2,090 (1934)	4,060 (1977)	448 (1977)
Mean	50,000	49,000	14,000
April-July flow, inches			
Maximum	13.8	12.84	8.34
Minimum	0.15	0.31	0.08
Mean	3.59	3.72	2.41

The seasonal variation in runoff is illustrated by the following table:

TABLE 4-11

MEAN MONTHLY RUNOFF INTO SUCCESS LAKE

Month	Volume (1,000 acre-feet) ^{1/}	Percent
Oct	1.3	.01
Nov	3.5	.03
Dec	9.1	.07
Jan	15.6	.11
Feb	18.2	.13
Mar	24.4	.18
Apr	25.3	.18
May	23.4	.17
Jun	11.4	.08
Jul	3.3	.02
Aug	1.1	.01
Sep	.8	.01
Total	137.4	100.0

^{1/} Average for 1904-1980 period.

4-08. Water Quality. The quality of Success Lake water, its inflow, and its outflow are checked bi-annually in April and August. A probe is used for on-site determination of temperature (T), dissolved oxygen (D.O.), pH, and electrical conductivity (EC). Nutrient, algae, salt, heavy metal, and pesticide levels are determined from samples in a laboratory. A sample measurement follows:

TABLE 4-12
WATER QUALITY OF TULE RIVER - APRIL 16, 1974

<u>Location</u>	<u>Inflow</u>	<u>Lake</u>	<u>Outflow</u>
Flow (c.f.s.)	289		303
TC (°F)	62	59	54.4
E.C. (p.p.m.)	142	120	166
D.O. (p.p.m.)	8.5	8.7	10.1
pH	7.8	8.4	7.3

In general, the project water quality is good to excellent relative to its beneficial uses. They have been determined by the State of California to be:

TABLE 4-13

BENEFICIAL USES OF TULE RIVER WATER

<u>Success Lake</u>	<u>Downstream</u>
Recreation	Recreation
Warm freshwater habitat	Warm freshwater habitat
Wildlife habitat	Wildlife habitat
Freshwater replenishment	Groundwater recharge
	Municipal and domestic supply
	Agricultural supply
	Industrial service supply
	Industrial process supply

4-09. Channel and Floodway Characteristics. Channel capacities below Success Dam are shown on plate A-7. Immediately below the project the channel passes through relatively sparsely populated rolling hills for about 5 miles before reaching Porterville. This reach can pass about 10,000 c.f.s. to below Porterville before agricultural damages occur and about 16,000 c.f.s. before damage occurs to urban property. Porter Slough takes off from the Tule River just above Porterville and passes through the Porterville business district. Its capacity is about 180 c.f.s. and diversions to it are controlled by a concrete structure.

Below Porterville the Tule River flood plain is mainly agricultural and the channel capacity decreases in this area. About 22 miles downstream from Porterville, Elk Bayou enters the Tule River and may contribute Kaweah River water. Tule River flow essentially enters Tulare Lakebed at Turnbull Weir where any remaining flow must be diverted into Lakeland Canal or it will enter the lakebed.

Since the Tule River has no outlet to the ocean, any releases above irrigation and spreading capability may be damaging below Turnbull Weir. In the spring and summer months, irrigation and spreading demand may reach approximately 1,500 c.f.s.: 1,000 c.f.s. diverted and 500 c.f.s. spread within the channel. During the rainflood season, under optimum conditions, the diversion capability may reach 500 c.f.s. and in channel spreading capability another 500 c.f.s. for a total of 1,000 c.f.s. above Turnbull Weir. At Turnbull Weir, up to 300 c.f.s. can be diverted into the Lakeland Canal depending on canal inflow from Elk Bayou (Kaweah River distributary) and other sources and the conditions at the canal's terminus. Channel improvements are in progress to increase Lakeland Canal to 550 c.f.s. by 1984.

In the past, releases of 3,200 c.f.s. (the maximum project design release) have caused damage to agricultural areas. In December 1966 a combined spill and release of 9,050 c.f.s. caused considerable agricultural damage but very little damage to urban property.

4-10. Upstream Structures. There are two powerhouses above Success Lake: Tule Powerhouse owned by P.G.&E. on the North Fork of Middle Fork Tule River and Tule Powerhouse owned by S.C.E. on Middle Fork Tule River. Larson Dam with 325 acre-feet of storage is located on a tributary to the South Fork Tule River and a diversion to South Tule Ditch is located on the South Fork Tule River. None of these projects affect the operation of Success Lake.

4-11. Downstream Structures. Except during large floods, most releases from Success Lake are used for irrigation. There are numerous diversion structures downstream for this purpose. Their locations are shown on plate A-7. The structure at the head of Porter Slough just above Porterville is of particular importance since it prevents excessive flow from going into Porter Slough and flooding Porterville.

4-12. Economic Data.

a. Population. Porterville is the only major population center along the Tule River. Its population is approximately 20,000. It is located in Tulare County which has a population of approximately 230,000.

b. Agriculture. Agriculture is the major activity along the Tule River. The crops grown include citrus, grapes, cotton and cattle field crops.

c. Industry. Manufacturing does take place in the vicinity of Porterville. The classes of goods manufactured include electronics, printing, synthetic yarns, womens sportswear, marine controls, disposable diapers, helicopters and machine components.

d. Flood Damages. Rainfloods on the Tule River produce high peak flows which damage improvements within the channel and adjacent areas while the volume exceeding irrigation and spreading capabilities goes on to Tulare Lake to pond on cropland. Prior to construction of Success Lake, rainfloods frequently caused extensive soil erosion, damaged farm equipment and structures, silted in irrigation canals, washed out diversion structures and washed out reaches of highways. The December 1950 flood, which reached a peak of approximately 28,000 c.f.s. at the Success Dam site, extensively damaged agricultural and industrial areas and caused relatively shallow flooding in a small portion of Porterville. The December 1955 flood, which peaked out at approximately 25,000 c.f.s. at the damsite, caused extensive damage but did not flood Porterville or its suburbs.

Snowmelt floods have much lower peak flows than rainfloods but larger volumes. Tule River snowmelt flood flows combined with runoff from adjacent basins flood large areas in Tulare Lakebed for long periods of time, more than a year in some cases.

A number of large floods have occurred since the project was built, the December 1966 flood with a peak inflow to Success Lake of 76,900 c.f.s. being the largest of record. Its combined spill and release reached 9,050 c.f.s. This flow damaged agricultural areas along the Tule River and in Tulare Lakebed but did relatively little damage to urban areas. The estimated damages prevented by Success Lake during 4 major floods follow:

TABLE 4-14
ESTIMATED DAMAGES PREVENTED BY SUCCESS LAKE

Water Year	Damages Prevented (\$1,000)	
	During Rainfloods	During Snowmelt Floods
1967	10,400	1,280
1969	5,300	2,100
1978	5,490	380
1980	7,600	1,500

V - DATA COLLECTION AND COMMUNICATIONS NETWORKS

5-01. Hydrometeorological Stations. Hydrometeorological information at Success Lake and elsewhere within the Tule River basin is monitored through the Hydrologic Automatic Data Acquisition (HADA) system. The Success Lake project office subcentral station automatically stores precipitation reports from 4 gages, Hossack (Hossack also transmits temperature data), Eagle Creek, Rogers Camp and Mountain Home by radio. It also automatically stores project release data and reservoir stages. Temperature, wind, evaporation and precipitation data at the project is entered into the subcentral station memory manually with thumb wheels. This data is transmitted to the central station (HADA central) in the Sacramento District Reservoir Control Section office. Normally, the precipitation gages automatically report every 6 hours, however, the system is set to make interim reports when .3 inches or more of precipitation falls since the last report.

The facilities at the project include the following:

- a. A float operated digital recording pool gage in the dam capable of recording pool levels up to the spillway design pool level, supplemented by a permanent staff gage in the reservoir.
- b. Two float operated digital recording outflow stream gages with selsyn operated data transmission just below the dam. One of these gages is on Tule River and the other is on Pioneer Ditch. Both are supplemented with visual staff gages.
- c. Recording inflow stations on Tule River near Springville and on South Fork Tule River near Success above the reservoir.
- d. A weather station at the dam.

The weather station at the dam consists of:

- a. Recording and non-recording precipitation gages.
- b. A wind station recording both direction and velocity.
- c. A weather bureau Class-A evaporation pan with anemometer.
- d. A recording hygrothermograph with maximum and minimum thermometers.

Climatological station locations and descriptions are shown on plate 12 and stream gage locations and descriptions are shown on plate 8.

5-02. Water Quality Stations. Project water quality and the techniques used to monitor it are discussed in paragraph 4-08. The locations and descriptions of water quality stations are shown on plate 8.

5-03. Sediment Stations. The sedimentation range locations are shown on plate 11. Reservoir sedimentation is discussed in paragraph 4-04.

5-04. Recording Hydrologic Data. Records of storage, inflow, outflow and evaporation at Success Lake are kept at the Corps of Engineers District Office

in Sacramento. Outflows and storages for the project are published by the U.S. Geological Survey from the Corps record. Extensive hydrologic data pertinent to irrigation is published by the Tule River Association.

5-05. Communication Network. Voice communication between the Sacramento Office and the project office is either by radio or telephone and the radios in both offices have backup power from batteries and standby generators.

The central station of the Hydrologic Automatic Data Acquisition system (HADA) in Sacramento can interrogate the subcentral stations of the projects by radio or telephone. The central and subcentral stations have backup power from batteries and standby generators.

The precipitation and stream gaging stations above the project report to the subcentral station by radio only and the reservoir stage and outflow gages are hard wired to the HADA system.

5-06. Communication with Project. Communication requirements between the project office and the Reservoir Control Section are discussed in exhibit A.

5-07. Project Reporting Instructions. Reporting instructions are discussed in exhibit A.

5-08. Warnings. Warnings are discussed in exhibit A.

VI - HYDROLOGIC FORECASTS

6-01. General. Since reliable long-term rainflood forecasts are not available, the rainflood space must be kept available throughout the rainflood season in anticipation of a large unforecasted rainflood. Short-term precipitation forecasts are available and are mainly useful for anticipating release changes due to increased inflow or a change in downstream conditions.

Most of the central valley in California is relatively unique in that general rainfloods during the late spring and summer are extremely rare. Therefore, runoff into the reservoirs can be fairly accurately predicted during the spring and summer based on the snowpack in the mountains. This allows the space required for flood control to be varied during the snowmelt season based on the forecasted runoff. These snowmelt forecasts are important in optimizing reservoir operation for flood control and conservation.

a. Role of Corps. The Corps of Engineers has no responsibility for furnishing forecasts of flow into or out of Success Lake to the public. However, the Corps does furnish release predictions to the National Weather Service to facilitate their forecasting of river flows. Plate 14 provides data which can be used to forecast inflow due to rain based on precipitation or known inflow.

b. Role of Other Agencies. The National Weather Service provides precipitation and river flow forecast data and the State provides snowmelt forecasts.

6-02. Flood Condition Forecasts. The National Weather Service provides short-term local precipitation forecasts up to 24-hours in advance. The precipitation gages incorporated in the HADA system which report every 6 hours under normal conditions will make interim reports anytime .3 inches of rain has fallen since the last report.

Since the conditional space required for flood control is determined from snowmelt forecasts, they are of primary concern in the operation of Success Lake. The Tule River Watermaster and the Corps of Engineers use snowmelt forecasts made by the California Department of Water Resources. The Department prepares forecasts of April through July runoff into Success Lake as of 1 February, 1 March, 1 April, and 1 May each year. Weekly updates are provided when conditions change appreciably from the last forecast. The forecasts are published about 10 days after the date to which they apply. A summary of forecasted runoff compared to actual runoff is shown on plate 15.

6-03. Conservation Purpose Forecasts. Operation of Success Lake for conservation is generally as requested by the Tule River Watermaster. The total demand for conservation water in Success Lake is largely a function of the forecasted runoff during the snowmelt season. Normal irrigation demand is shown on plate A-8.

6-04. Long-range Forecasts. Other than snowmelt forecasts discussed above, no long-range forecasts are used by the Corps of Engineers for the Tule River basin.

VII - WATER CONTROL PLAN

7-01. General Objectives. Success Reservoir will be operated for flood control and conservation to achieve the following objectives:

a. To restrict flows in downstream channels of Tule River and its distributaries to nondamaging rates.

b. To minimize damaging flows from Tule River into the Tulare Lakebed area.

c. To provide the maximum practicable amount of storage space for conservation of irrigation water without impairment of the flood control functions.

7-02. Major Constraints. Releases greater than irrigation and spreading demand have the potential to pond on valuable cropland in Tulare Lakebed. Tulare Lakebed also receives flood water from a number of other sources. Therefore, releases from Success Lake should be coordinated with flow from other sources to the extent possible giving consideration to downstream storage and diversion capabilities.

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Structures which impede the flow of water over the spillway will not be permitted.

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7-03. Overall Plan for Water Control. The overall plan for water control is to coordinate releases for flood control with conservation demand to the greatest extent possible. During the rainflood season, when reliable inflow forecasts are not available, the required rainflood space is set for a given date, with minor variations based on downstream irrigation and spreading capability, and antecedent precipitation. During the snowmelt season, the required flood control space is varied based on forecasted inflow and irrigation and spreading demand to satisfy both flood control and conservation objectives. The snowmelt portion of the flood control diagram (plate A-8) is designed to fill the reservoir, if runoff and irrigation demand permit, but not to spill.

Downstream spreading and irrigation capability is essential to allow non-damaging releases to be made. The design of Success Lake flood control operation is based on maintaining a 500 c.f.s. irrigation and spreading capability along the Tule River below the project.

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7-04. Standing Instructions to Dam Operator. The standing instructions to the dam operator are contained in exhibit A.

7-05. Flood Control. In 1986, the Tule River Association agreed on the following to describe the distribution of water released from flood control space: "Water stored in schedule 1, 2, or 3 flood control space will be released in accordance with the schedule that applies to that space. These criteria are established to ensure the timely release of water from flood control space in the reservoir and, therefore, such releases shall not be restricted by the storage and diversion rights under the Tule River Association agreements. It is understood that, under the Tule River Association agreements, each TRA unit has the right to supplement any required flood control releases by additional releases of such unit's Tule

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River Water entitlement and/or water held in Success Lake storage for the account of such unit, as may be desired from time to time for beneficial use by such unit."* A detailed explanation of flood control operation, including emergencies, is contained in exhibit A and on plate A-8. An explanation of the allocation of reservoir space is contained in paragraph 3-05, "Modification to Regulations". Specific information concerning forecasts and channel and floodway characteristics is found under those headings. *

7.06. Recreation. On 2 November 1965, the Tule River Association entered into an agreement with the County of Tulare (Tulare County Agreement No. 1915) for the purpose of providing a minimum pool for recreational use. This agreement was terminated on 16 October 1987 and the parties are presently negotiating a new agreement. *

7.07. Water Quality. Success Lake is not operated for water quality. Water quality measurements and the quality of water within the Lake are discussed in paragraph 4-08, "Water Quality."

7-08. Fish and Wildlife. Success Lake supports one of the best bass fisheries in the San Joaquin Basin. In addition, approximately 1,400 acres on the northeast side of Success Lake have been set aside as a wildlife management area. About half of the acreage is above gross pool elevation. The area is characterized by alternating rows of bush, cereal grains, and fallow strips. The area is managed to increase the variety and numbers of upland game species as well as non-game animals. The area was developed with the assistance and cooperation of the California Department of Fish and Game, Southern Tulare Sportsmen's Association, Tulare County Audubon Society, California Department of Forestry, Tulare County Fine Commission, and Tulare County Parks and Recreation Department.

7.09. Water Supply. Space not required for flood control or retention of a minimum pool is operated for conservation. In 1986, the Tule River Association agreed on the following to describe the distribution of water stored in conservation space: "Water stored in conservation space may be released by Tule River water users in accordance with their respective entitlements under the agreements among such water users." *

User contract No. 14-06-200-2110A between the United States and the downstream water users provides for the operation and maintenance of irrigation space.

7-10. Hydroelectric Power. There are no facilities for hydroelectric power generation at this time, however, the Lower Tule River Irrigation District representing the Tule River Association has an approved application from F.E.R.C. for generating power at the project.

7-11. Navigation. No portion of the Tule River is considered navigable.

7-12. Drought Contingency Plan. During droughts, flood control is not expected to be a principle factor in the operation of Success Lake. Conservation water and conservation space is managed by local interests in accordance with contacts between the various irrigation interests. As part of the drought contingency plan, Schedule 1 releases may be deferred temporarily in anticipation of a dry water year during the period 11 November through 27 March. The amount of encroachment at anytime is dependent on the basin

wetness parameter as discussed in paragraph 3f in exhibit A. During droughts, the Tule River Watermaster and the various groups he represents can be expected to conserve water to the best of their ability. Any information that the Corps of Engineers may have that would be beneficial to drought operation will be passed on to the Tule River Watermaster. In extreme cases, it may be desirable to pump water from the sediment pool below the outlet invert. It should be noted that project toilets, showers, and sink fixtures are low flow or microflow types.

7-13. Deviation from Normal Operation. Deviations from normal operation are discussed in exhibit A.

7-14. Rate of Release Change. Release changes should not be made without notifying the Tule River Watermaster or his representative. There are numerous irrigation structures downstream from the dam which may require adjustments prior to any release change. In addition, during periods of high releases, the Tule River channel must be patrolled for debris removal and to assure the proper functioning of flood control works. These downstream activities are coordinated through the Tule River Watermaster.

Generally, the rate at which flows will be changed will be based on prevailing downstream conditions. In the absence of any downstream constraints, releases from Success Lake should not be increased or decreased by more than 1,000 c.f.s. per hour.

VIII - EFFECT OF WATER CONTROL PLAN

8-01. General. Success Lake has decreased the frequency of flooding, increased the water available for irrigation during the irrigation season and increased the recreation opportunities within the Tule River basin. The historical operation of Success Lake is shown graphically on plate 16.

8-02. Flood Control.

a. Spillway Design Flood. The spillway design flood for Success Lake is based on a storm averaging 23.2 inches of precipitation and the equivalent of 4.7 inches of snowmelt over the entire basin resulting in a total runoff of 16.6 inches. The total volume of runoff in 4 days is 347,000 acre-feet. The peak inflow is 200,000 c.f.s. A routing of the spillway design flood is shown on plate 17.

b. Standard Project Rainflood. The standard project rainflood shown in this manual was developed in 1970. The total average precipitation over the basin (20.14 inches) is about the same as that in December 1966 but the freezing level, snowmelt, time distribution and infiltration rates are more severe. The excess (6.12 inches) combined with base flow gives a total main wave volume of 157,000 acre-feet, about 140 percent of the 5-day runoff from 4 through 8 December 1966. A routing of the standard project rainflood is shown on plate 17.

c. Reservoir Design Flood. The reservoir design flood shown in Design Memorandum No. 5 Reservoir Regulation, dated December 1956, was considered to be a 100-year flood and was controlled to 3,200 c.f.s. below Success Dam. It was concluded that the project provided 100-year protection to agricultural areas since at that time 3,200 c.f.s. was considered non-damaging. Its 4-day volume is about 95,000 acre-feet which is about a 50-year event on the current frequency curves for unregulated rainflows below Success Dam shown on plate 19. In addition, the design flood is a 4-day flood series whereas routings show that, due to limited release schedules at low pool elevations, a longer duration series is critical at Success Lake. Success Lake was considered to provide standard project flood protection to Porterville. However, the SPF shown in D.M. No. 5 was exceeded in December 1966 and a new one was developed in 1970. Routings using 30-day rainflood series based on the frequency curves for unregulated rainflows below Success Dam indicate that Success Lake will fill to the spillway or above an average of once every 30 years, spill 3,200 c.f.s. or more once every 40 years and exceed the channel capacity through Porterville about once every 100 years. These routings were made assuming that on the average 80 percent of the scheduled releases shown on plate A-8 would be achieved. Routings of the reservoir design flood and 100-year flood are shown on plate 17.

d. Snowmelt floods. Releases required to control snowmelt floods are not expected to exceed 3,200 c.f.s. except during exceptionally rare events. Releases exceeding 1,500 c.f.s. (total downstream diversion and spreading capability above Turnbull Weir) can be expected about once every 40 years. Tule River flows below Turnbull Weir may damage Tulare Lakebed depending on their diversion capability. Hypothetical routings of the 1906 and 1969 snowmelt floods using the criteria on plate A-8 are shown on plate 18.

8-03. Recreation. Success Lake supports a fishery and provides opportunities for many other types of recreation. A description of the recreation development is in paragraph 2-06.

8-04. Water Quality. Although the agricultural and recreational activities at the lake and the warming of the ponded water may have some detrimental affect on quality, Success Lake provides water for recreation and irrigation at times when there would otherwise be none and the quality of the water is good to excellent relative to its beneficial uses. The beneficial uses are listed in table 4-12.

8-05. Fish and Wildlife. Success Lake supports an excellent warmwater fishery within the lake. This is a considerable enhancement since natural flow in the Tule River often falls to zero.

8-06. Water Supply. Success Lake provides approximately 25,000 acre-feet of new and redistributed water.

8-07. Hydroelectric Power. There is presently no generation of hydroelectric power at the project. However, there is some potential and the feasibility for power generation is presently being investigated by the Tule River Association.

8-08. Navigation. Success Lake augments Tule River flows, however, very little if any navigation occurs below the dam.

8-09. Frequencies.

a. Peak Flow Probability. The potential for rainfloods below the dam comes from project spills. There is little local flow between the dam and Porterville. Rainflow frequency curves for unregulated and regulated flows at the dam are shown on plate 19. Snowmelt flow frequency curves for unregulated and regulated conditions are shown on plate 20.

The unregulated rainflow frequency curves were based on a two station comparison between the Tule River gage below Success Dam and the Tule River near Porterville gage. The curves were then adjusted on the assumption that the 1 through 15 day flows during the December 1966 flood were the largest in the last 100 years. The curves were also adjusted for expected probability. The plotting positions for the flows below Success Dam were determined by correlation with the flows near Porterville. The period of record for the Tule River near Porterville gage is from 1901 through 1960.

The regulated rainflow frequency curve was drawn graphically. The project releases were plotted based on a period of nineteen years except for the December 1966 peak release which was plotted at the frequency of the 30-day flow for that flood. Hypothetical routings assuming 80 percent channel capacity were used to locate the uncontrolled portion of the curve. A 30-day flood series was used, the frequency of which was determined from the unregulated 30-day frequency curve.

The snowmelt flow means at the Tule River below Success Dam and the Tule River near Porterville gages were close and the correlation coefficients for the flows of various durations at these stations were .99+. So, it was felt that little error would result from estimating the snowmelt flows at Success

1

through a correlation with the near Porterville gage flows. The snowmelt flow frequency curves were developed by treating the estimated and actual flows below Success Dam as a continuous record. The actual flows below Success Dam were plotted as indicated by the correlation with the gage near Porterville.

The regulated snowmelt flow frequency curve was drawn graphically. The project releases were plotted based on a period of nineteen years except for the 1969 flood which was plotted as the second largest in 78 years. Hypothetical routings were used to locate the upper portion of the curve. The routings were based on the April through July 1969 flow pattern with the volume determined by the 120-day unregulated snowmelt curve. The flood control diagram and irrigation demands shown on plate A-8 were used for the routings.

b. Stage-Duration and Frequency. Stage-duration curves, a stage-frequency curve and seasonal variation of reservoir storage frequency curves are shown on plates 21, 22 and 23.

8-10. Other Studies. The Tule River association is presently investigating the feasibility of generating power with Success Lake releases.

IX - WATER CONTROL MANAGEMENT

9-01. Responsibilities and Organization.

a. Corps of Engineers. The District Engineer, Sacramento is responsible for:

- (1) Prescribing the use of flood control space in Success Lake.
- (2) Operation and Maintenance of Success Lake.
- (3) Advising local interests and the Division Engineer of any substantial deviation from the flood control regulations.
- (4) Preparing monthly operation and other reports required by the Division Engineer.
- (5) Estimating the water users share of maintenance and operation costs.

Corps personnel under supervision of Construction-Operations Division, Sacramento District, operate Success Lake with instructions on all matters pertaining to flood control operation received directly from the Reservoir Control Section. The duties of the reservoir operators and the Reservoir Control Section are discussed in detail in Exhibit A.

b. Bureau of Reclamation. The Bureau acts as the agent for the United States in the execution of the repayment contract (14-06-200-2110A).

c. California Department of Fish and Game. They enforce fish and game laws on the lake and within the wildlife areas. They also plant fish in the lake.

d. California Division of Forestry. They are responsible for fire fighting on project lands.

e. County of Tulare. They provide normal law enforcement at the project and, through an agreement with the State, patrol the lake by boat. During periods of peak visitation, they provide additional law enforcement under contract with the Corps. They also supervise and maintain Bartlett Park which is on project land below the dam.

f. Tule River Watermaster. He is appointed by the Tule River Association to act on behalf of downstream water users. He directs the use of space not required for flood control in Success Lake.

9-02. Interagency Coordination.

a. Local Press. Either the Corps of Engineers Public Affairs Office or the Tule River Association are responsible for making local press releases concerning the operation of Success Lake. The Federal-State River Forecast Center furnishes the press with downstream river flow forecasts.

b. National Weather Service. The California Department of Water Resources cooperates with the National Weather Service to develop streamflow forecasts. The Corps of Engineers provides them with forecasts of Success Lake operation.

c. U.S. Geological Survey. The Corps of Engineers makes payments to the U.S.G.S. to maintain 5 gages on the Tule River: Tule River near Springville; South Fork Tule River near Success, California; Success Lake near Success, California; Tule River below Success Dam and Pioneer Ditch below Success Dam. The U.S.G.S. publishes the flows and water quality data (when applicable) at these gages.

d. California Department of Water Resources. The Corps of Engineers furnishes the DWR with precipitation and temperature data from climatological stations it maintains on the Tule River: Hossack, Eagle Creek, Mountain Home, Rogers Camp and Success Dam. The DWR publishes most of this data.

e. Bureau of Reclamation. The Friant Kern Canal which is operated by the Bureau of Reclamation carries diverted water from Millerton Lake on the San Joaquin River to Tulare Lake Basin. The canal diverts San Joaquin River water to the Tule River irrigation network. The operation of the Friant Kern Canal and Success Lake must be coordinated. The coordination of conservation releases is normally the responsibility of the Tule River Watermaster. However, during floods, Corps personnel and Bureau personnel should be aware of how the operation of Success Lake and the Friant Kern Canal will impact the Tule River.

f. Tule River. All releases from Success Lake must be coordinated with Tule River Watermaster since he has first hand knowledge of downstream conditions and may have to operate various structures to accommodate a release change.

g. Other Local Agencies. Releases from Success Lake, which are not used for irrigation or spreading may flow to Tulare Lakebed and flood cropland. Therefore, whenever such releases are anticipated, Tulare Lake interests should be notified.

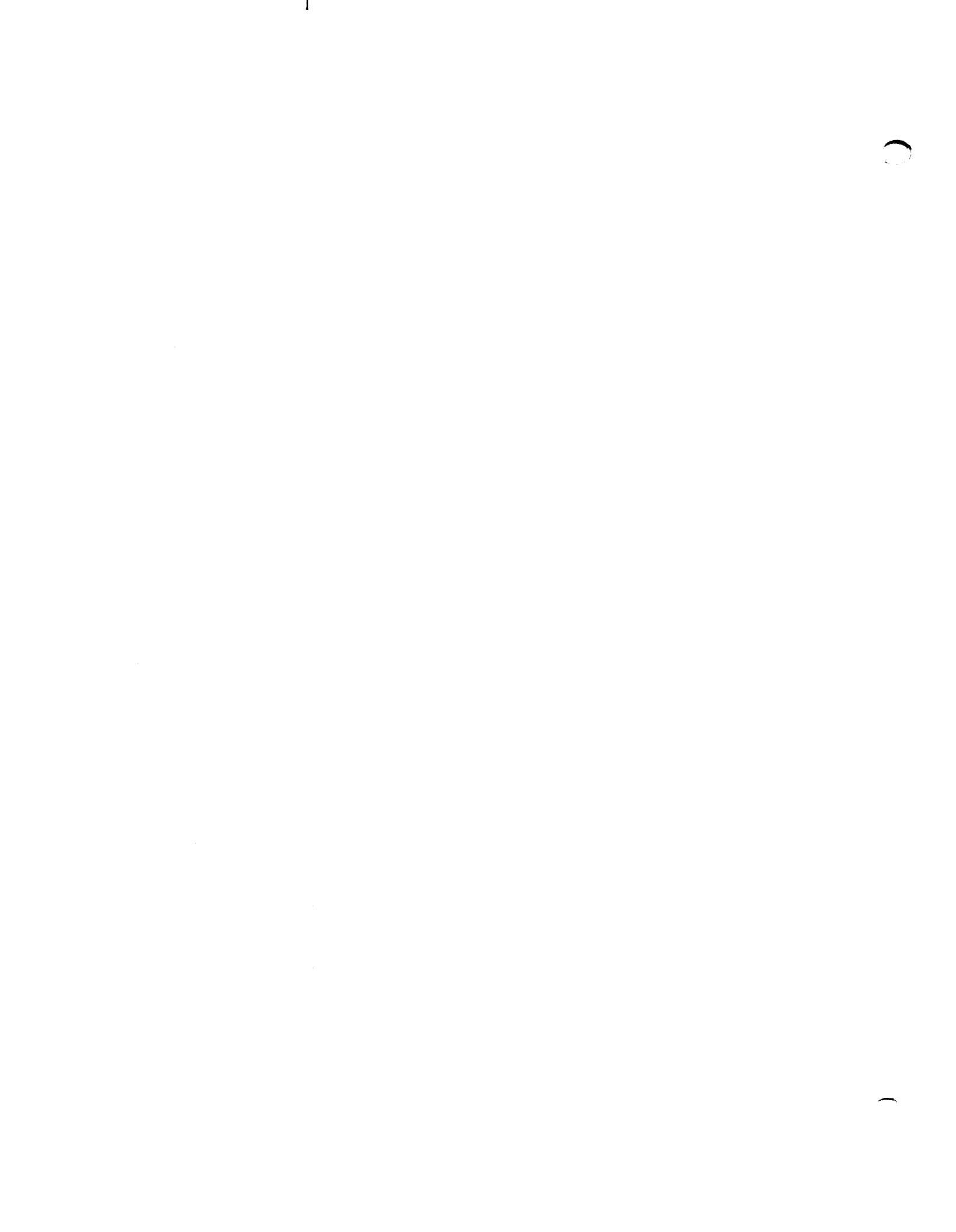
9-03. Coordination with Other Projects Operated by the Corps of Engineers. Pine Flat Lake, Lake Kaweah, and Isabella Lake are all operated by the Corps of Engineers and have the potential to release floodwater to Tulare Lakebed. The flood control operation of these projects must be coordinated with that of Success Lake to take advantage of any opportunity to minimize flood damages.

9-04. Interagency Agreements. The division of responsibilities in the Central Valley Basin of California between the Corps of Engineers and the Bureau of Reclamation in respect to water resource project planning, construction and operation activities is spelled out in the Memorandum of Agreement between the Department of The Army and The Department of the Interior on division of responsibilities in the Central Valley Basin, California dated 29 December 1958.

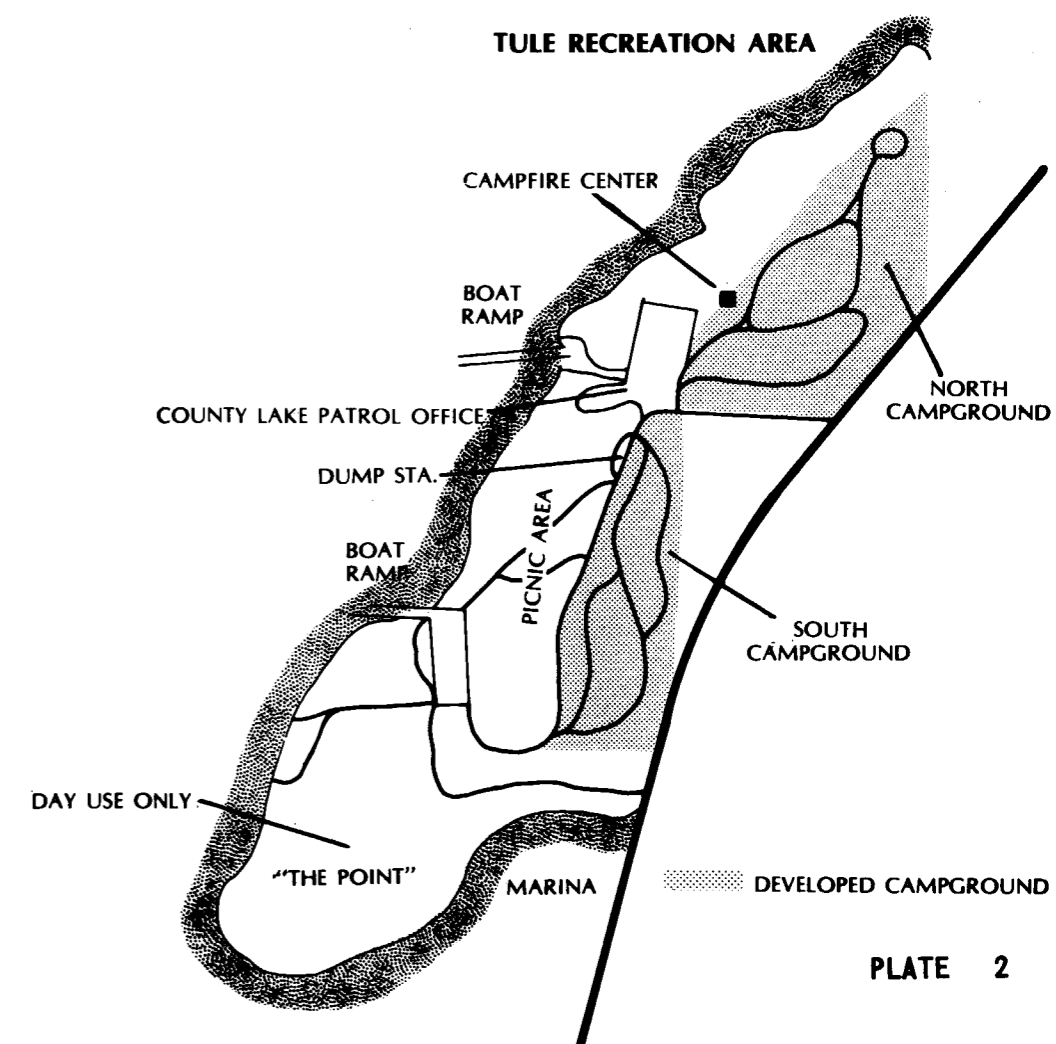
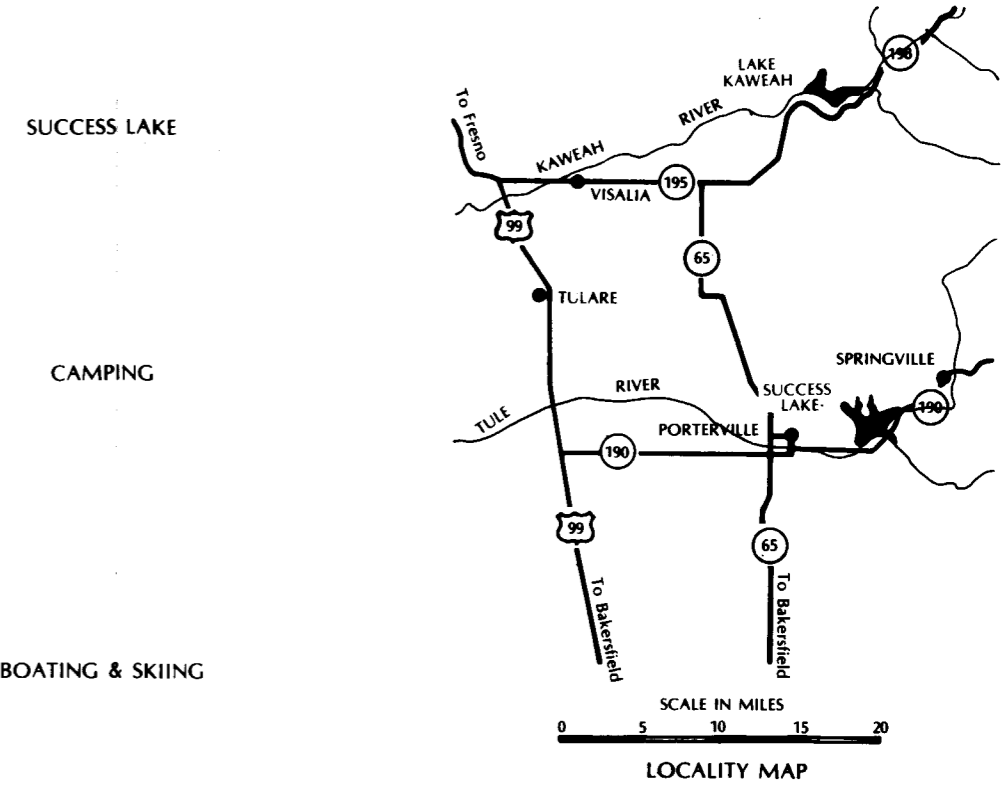
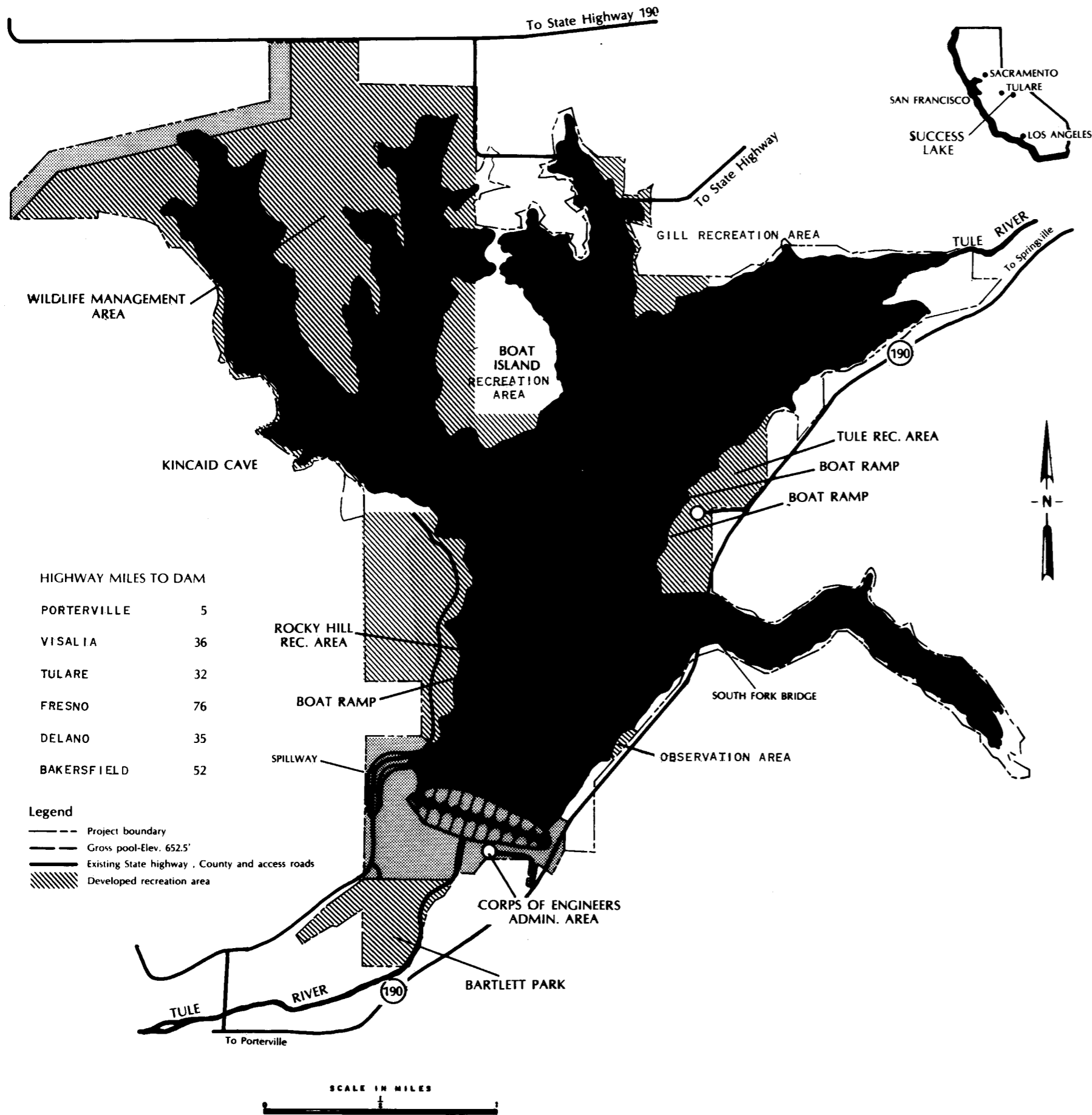
The provisions for payment of project first costs and O&M costs by local interests are set forth in Bureau of Reclamation contract number 14-06-200-2110A.

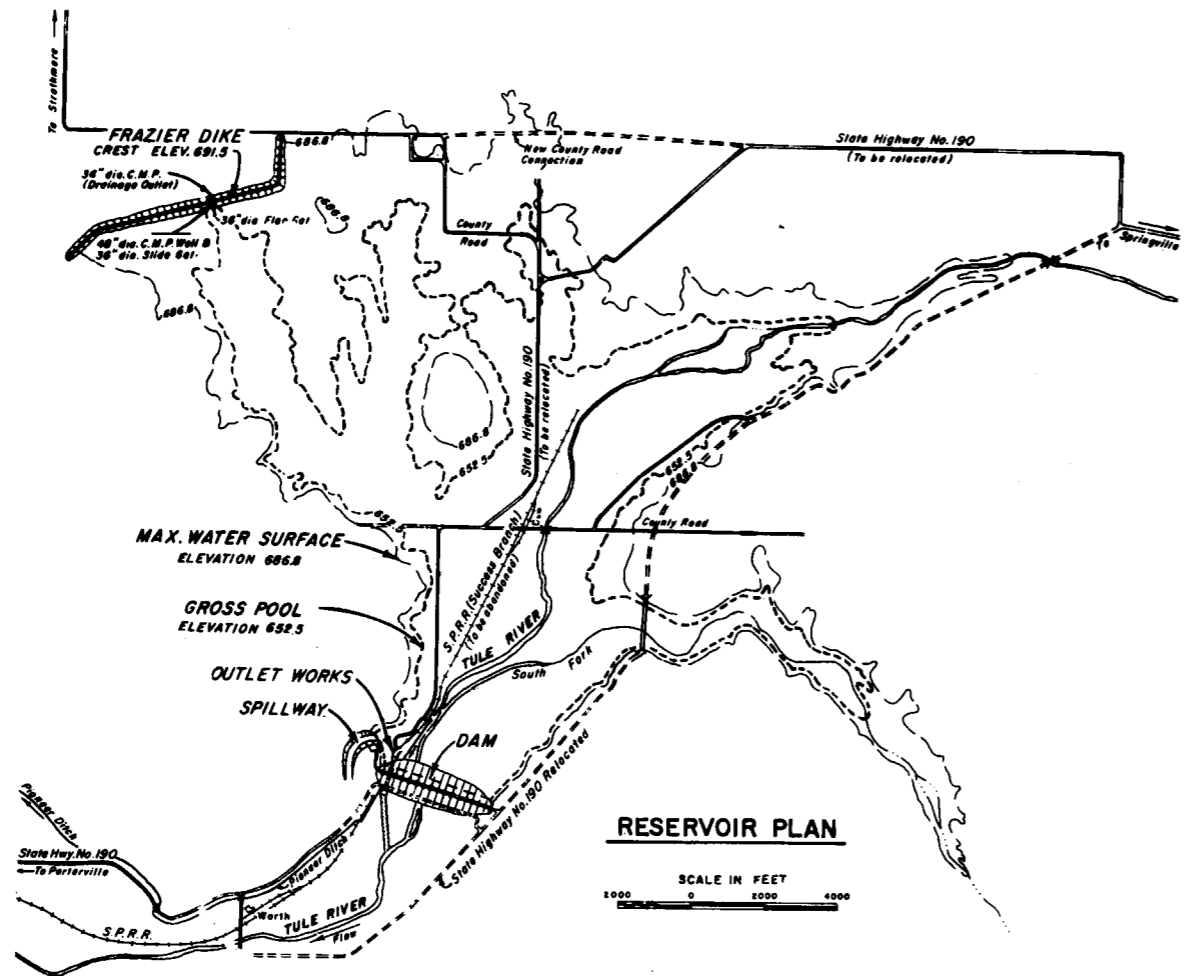
9-05. Commissions, River Authorities, Compacts and Committees. None.

9-06. Reports. The Tule River Association publishes an annual report listing precipitation, discharge, unit entitlement, storage, and diversion. Other reports required for the operation of Success Lake are discussed in exhibit A.



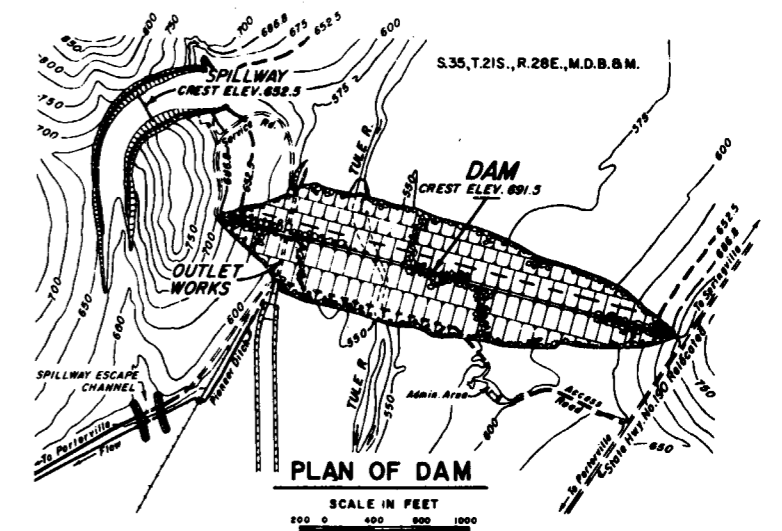
GENERAL SITE PLAN AND RECREATIONAL DEVELOPMENT NEAR PORTERVILLE IN TULARE COUNTY, CALIFORNIA





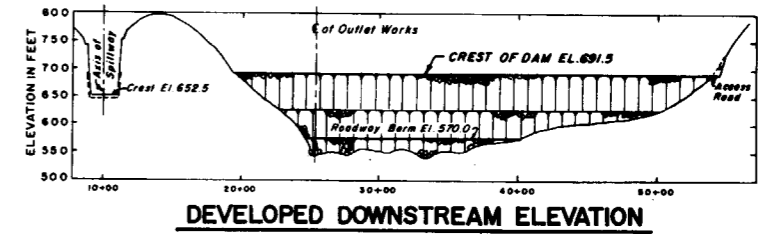
RESERVOIR PLAN

SCALE IN FEET
0 1000 2000 4000

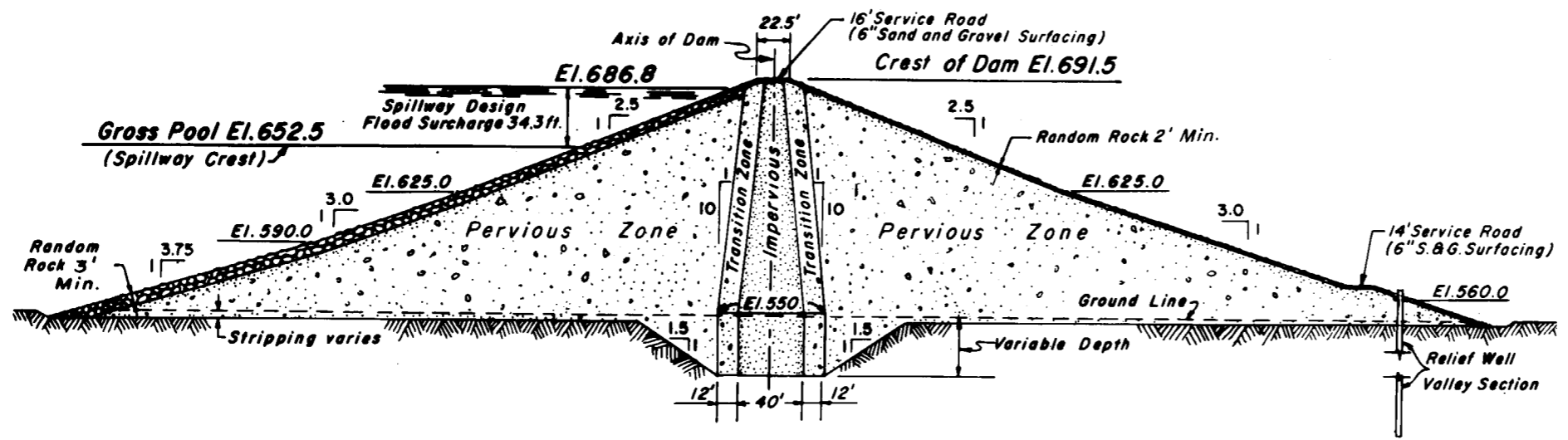


PLAN OF DAM

SCALE IN FEET
0 200 400 600 800 1000



DEVELOPED DOWNSTREAM ELEVATION



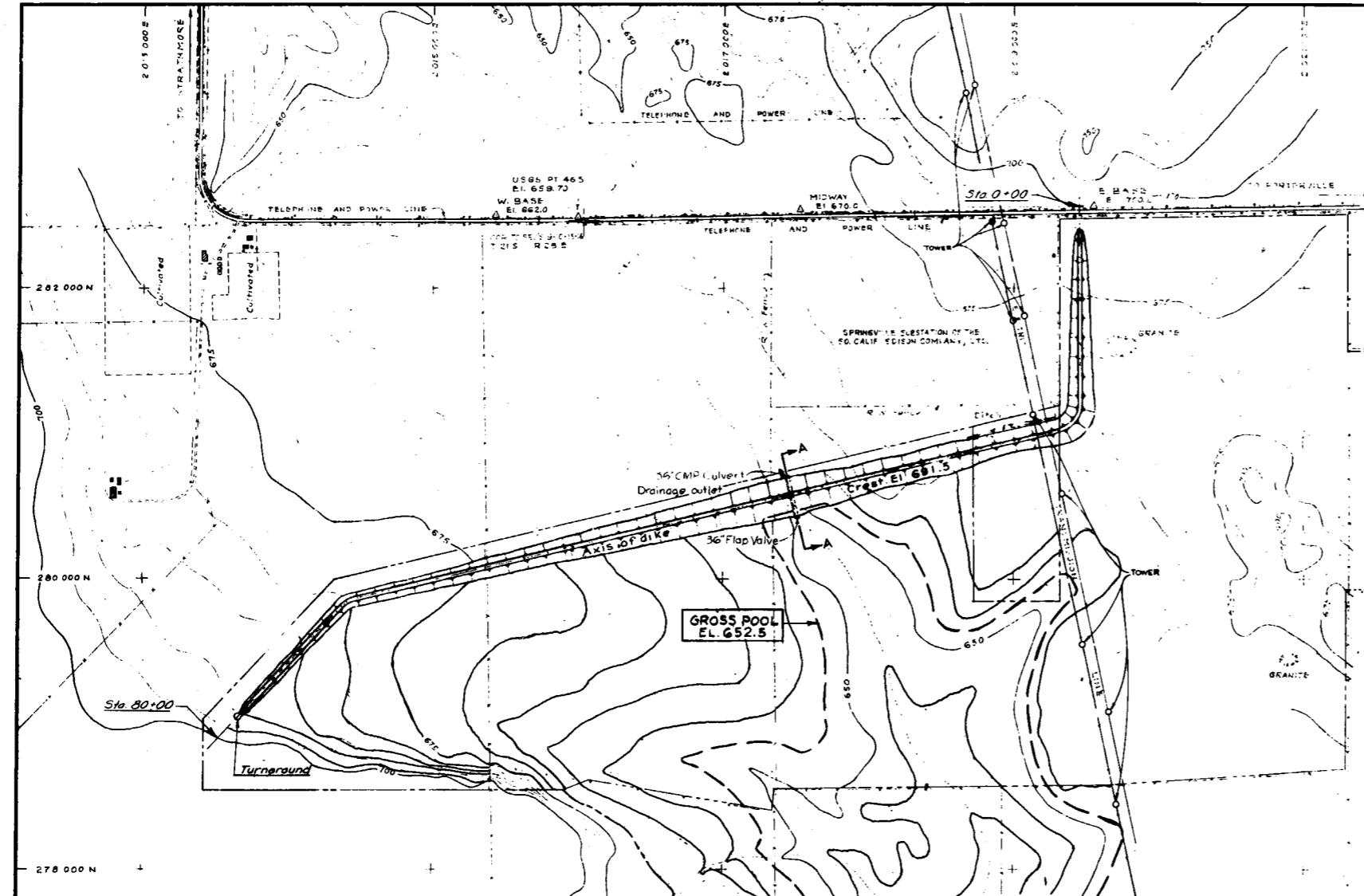
TYPICAL EMBANKMENT SECTION OF DAM

SCALE IN FEET
0 30 60 120

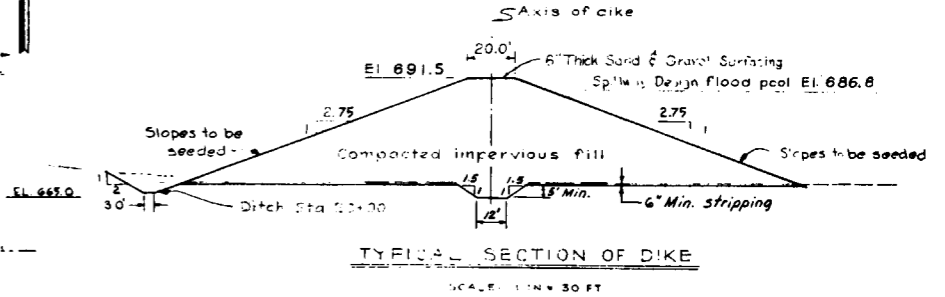
SUCCESS LAKE
TULE RIVER, CALIFORNIA

SUCCESS DAM
GENERAL PLAN AND PROFILE

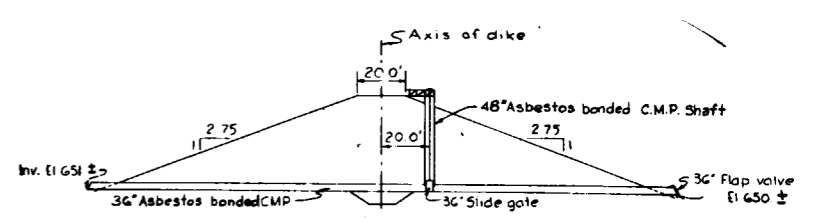
U. S. Army Engineer District Sacramento, California
R.P.L. August 1966



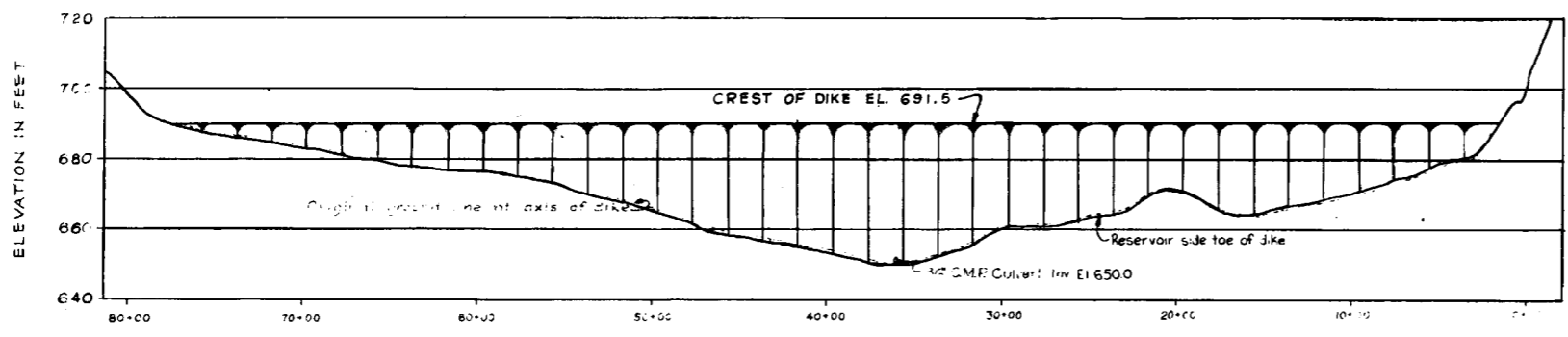
PLAN
SCALE: 1 IN = 400 FT



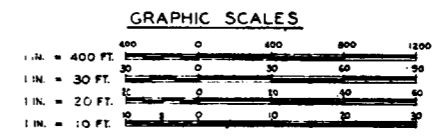
TYPICAL SECTION OF DIKE
SCALE: 1 IN = 30 FT



SECTION A-A
SCALE: 1 IN = 30 FT



DEVELOPED RESERVOIR SIDE ELEVATION
SCALE: VERT. 1 IN = 20 FT
HORIZ. 1 IN = 400 FT



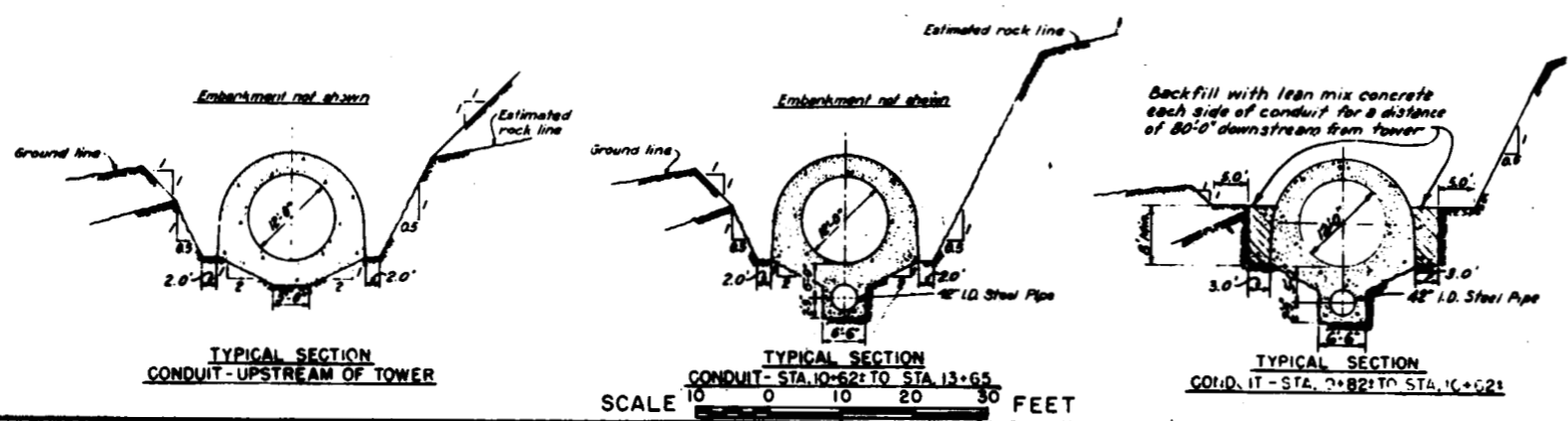
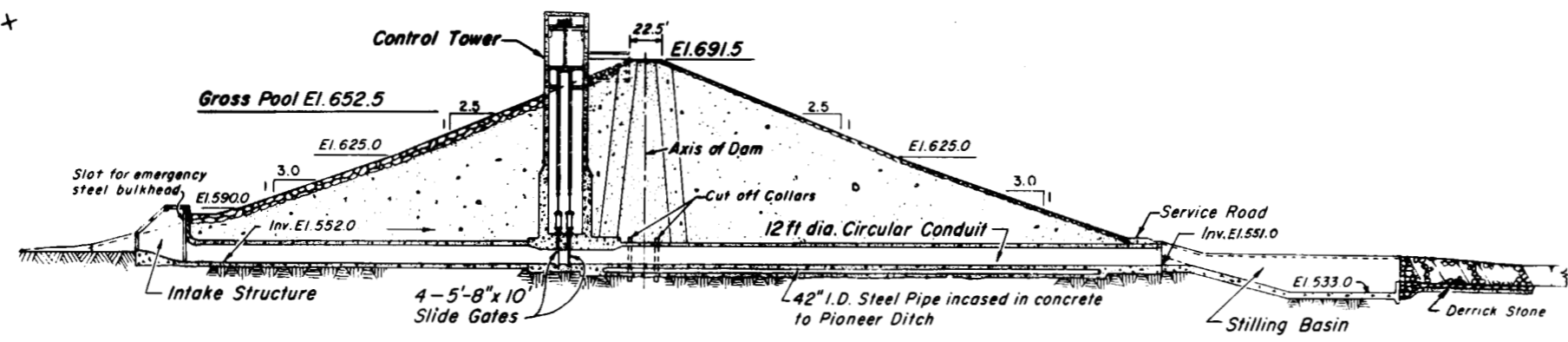
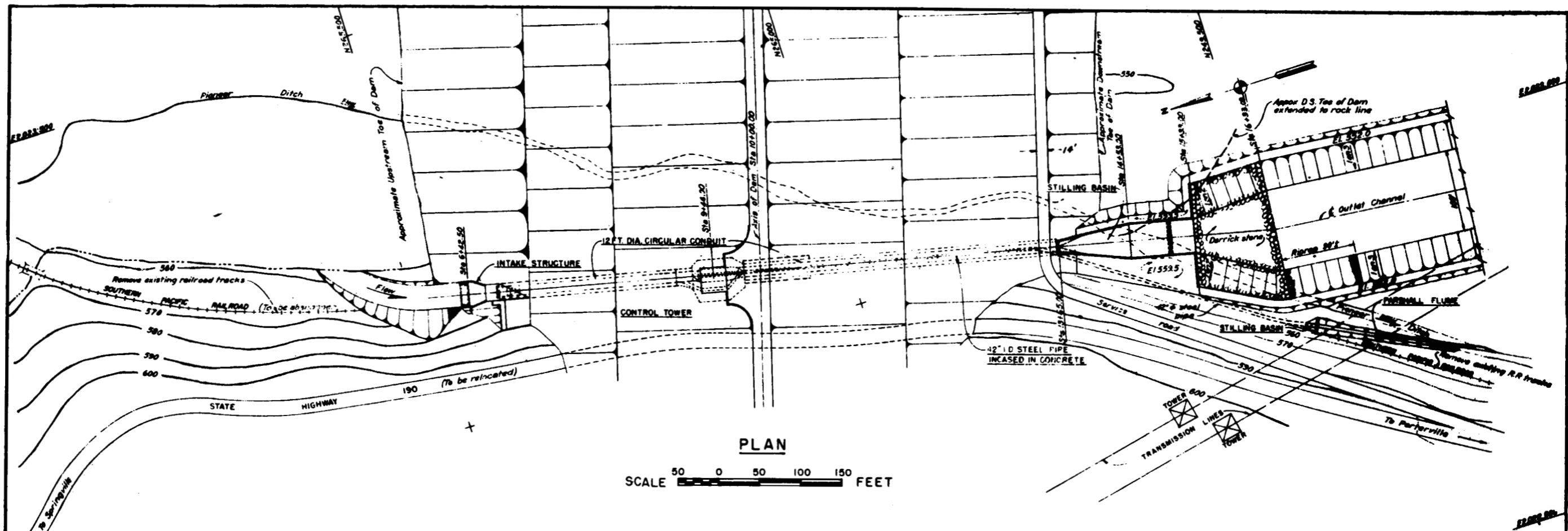
NOTES:
Datum is mean sea level (1929 adj)
Contour interval 5 ft.
California State Coordinate System, Zone 4

LEGEND
--- Real Estate Acquisition Line
--- Property Line

SUCCESS LAKE
TULE RIVER, CALIFORNIA

FRAZIER DIKE
GENERAL PLAN, PROFILE AND SECTION

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA
Prepared: _____ Date: JULY 1956



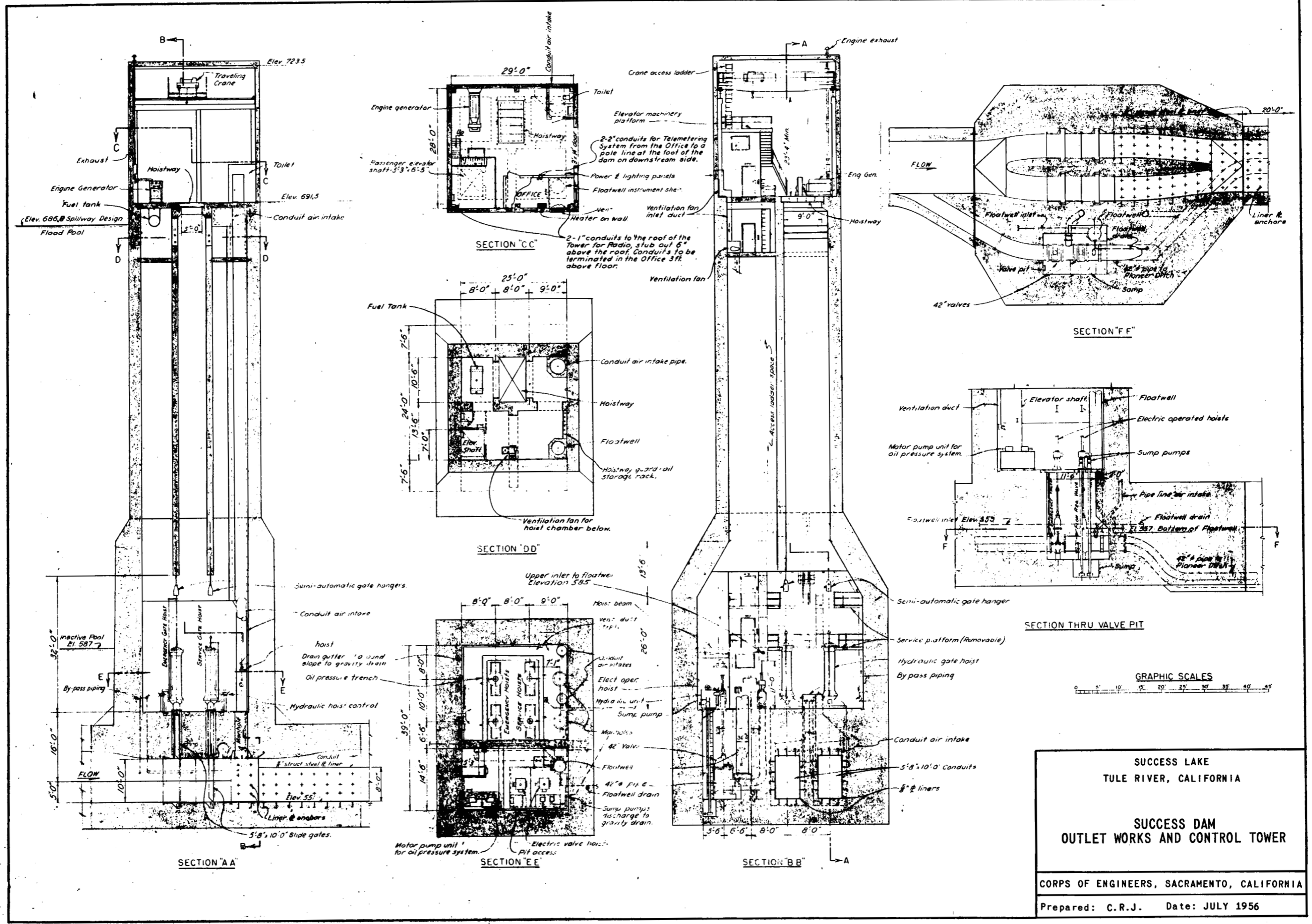
GENERAL NOTES
 1. Datum is Mean Sea Level, 1929 Adjustment.
 California State Coordinate System, Zone 4.

**SUCCESS LAKE
 TULE RIVER, CALIFORNIA**

**SUCCESS DAM
 OUTLET WORKS
 PLAN, PROFILE AND SECTIONS**

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

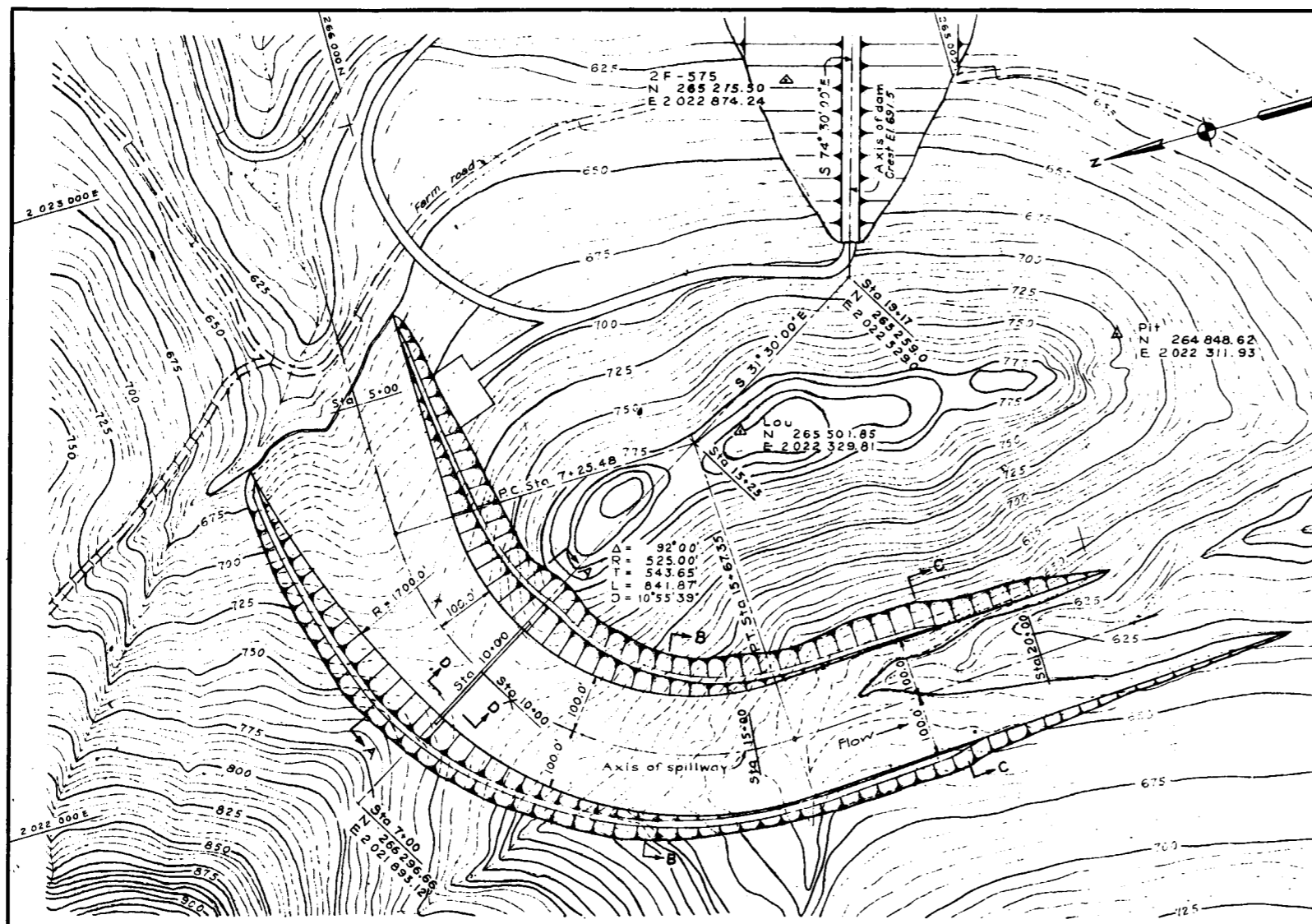
R.P.L. May 1961



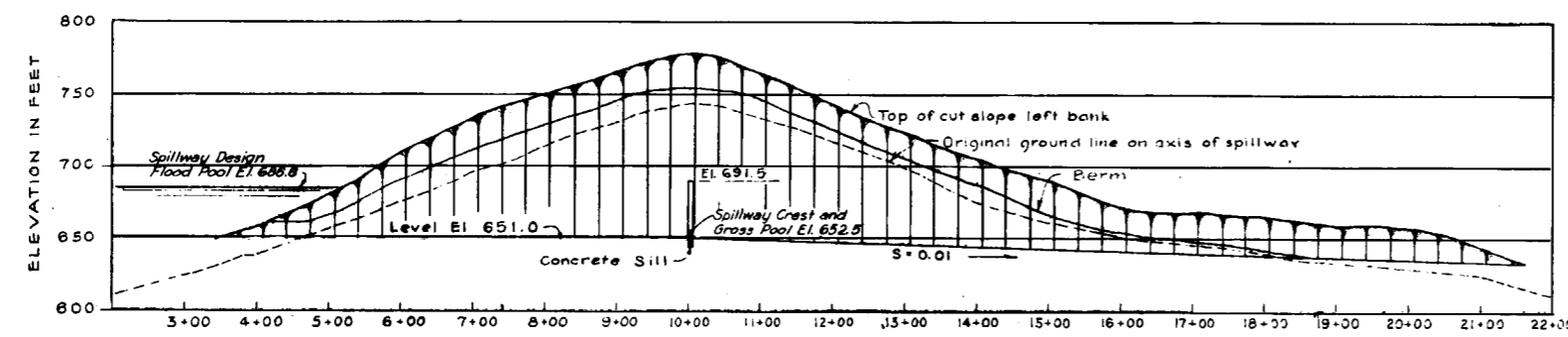
SUCCESS LAKE
 TULE RIVER, CALIFORNIA

SUCCESS DAM
 OUTLET WORKS AND CONTROL TOWER

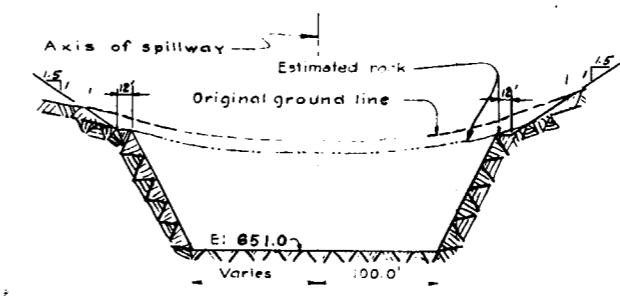
CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA
 Prepared: C.R.J. Date: JULY 1956



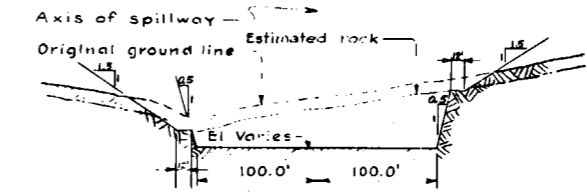
PLAN
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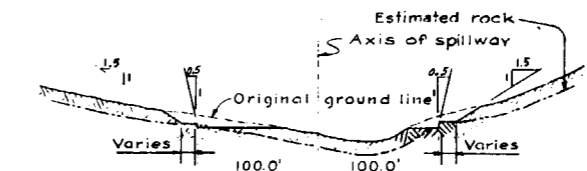
**DEVELOPED SECTION
ALONG AXIS OF SPILLWAY**
SCALE: VERT 1 IN = 20 FT
SCALE: HORIZ 1 IN = 100 FT



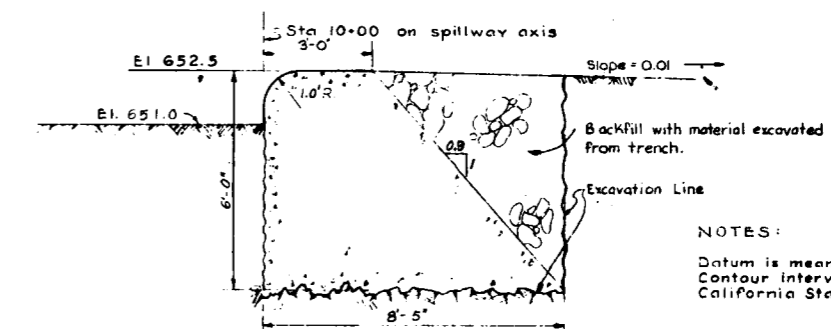
SECTION A-A
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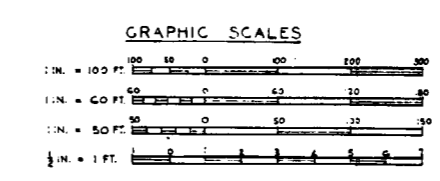
SECTION B-B
SCALE: 1 IN = 60 FT



SECTION C-C
SCALE: 1 IN = 60 FT



SECTION D-D
SCALE: 1/2 IN = 1 FT



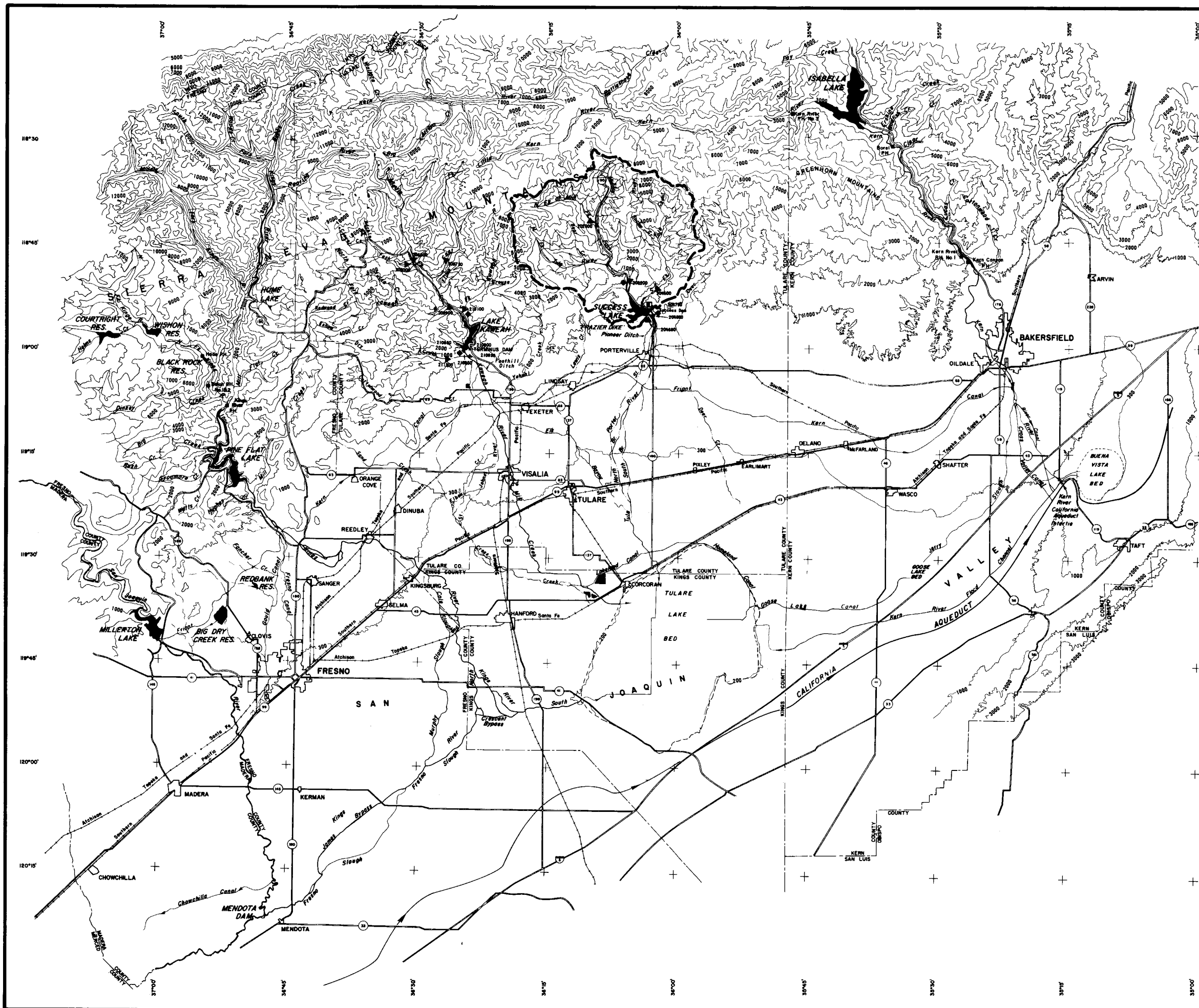
NOTES:
Datum is mean sea level (1929 adj)
Contour interval 5 ft.
California State Coordinate System, Zone 4

**SUCCESS LAKE
TULE RIVER, CALIFORNIA**

**SUCCESS DAM
SPILLWAY PLAN, PROFILE AND SECTIONS**

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

Prepared: _____ Date: _____



CALIF INDEX NUMBER	GAGING STATION	TYPE OF GAGE	LOCATION				ELEVATION		DRAINAGE AREA (SQ MI)	RECORDS		MAXIMUM FLOW	
			LATITUDE		LONGITUDE		FEET	DATUM		YEAR IN	AGENCY IN CHARGE	DATE	CFS
			DEG	MIN	DEG	MIN							
202800	NORTH FORK OF MIDDLE FORK TULE RIVER NEAR SPRINGVILLE, CA.	▲	36	10	118	52	2920	TOPO	29.3	1969	PRAC	6 DEC 66	16,000
202800	TULE RIVER NEAR SPRINGVILLE, CA.	▲	36	06	118	52	640	TOPO	247	1967	USGS	6 DEC 66	49,000
204600	SOUTH FORK TULE RIVER NEAR SUCCES, CA.	▲	36	08	118	51	770	TOPO	100	1930	USGS	6 DEC 66	14,000
204600	PIONEER DITCH BELOW SUCES DAM	▲	36	04	118	55	540	NEL	--	1960	C OF E	--	--
204700	SUCCESS LAKE NEAR SUCCES, CA.	▲	36	04	118	55	NSL	391	1961	C OF E	--	--	
204900	TULE RIVER BELOW SUCES DAM	▲	36	08	118	55	520	NEL	930	1968	C OF E	28 DEC 66	27,000
204900	MIDDLE FORK KANEAN RIVER NEAR PERDUE CAMP, CA.	▲	36	21	118	47	2100	TOPO	102	1949	USGS, SCE	28 DEC 65	46,000
204900	MIDDLE FORK KANEAN RIVER AT POTWISKEY CAMP, CA.	▲	36	21	118	43	2150	TOPO	61.4	1950	USGS, SCE	28 DEC 65	12,500
204780	EAST FORK KANEAN RIVER NEAR THREE RIVERS, CA.	▲	36	27	118	47	2500	TOPO	86.6	1957	SCE	6 DEC 66	19,000
204900	KANEAN RIVER AT THREE RIVERS, CA.	▲	36	27	118	54	810	NS	418	1958	USGS	5 DEC 66	78,000
210100	SOUTH FORK KANEAN RIVER AT THREE RIVERS, CA.	▲	36	25	118	55	907	NS	88.7	1959	USGS	6 DEC 66	11,000
210650	LEHMOGVE DITCH BELOW TERNHUS DAM, CA.	▲	36	25	118	00	546.0	NS	--	1962	C OF E	--	--
210900	LAKE KANEAN NEAR LEHMOGVE, CA.	▲	36	25	118	00	894	NEL	640	1962	C OF E	--	--
210930	FOOTRILL DITCH BELOW TERNHUS DAM, CA.	▲	36	25	118	01	492.0	NS	--	1961	C OF E	--	--
210950	KANEAN RIVER BELOW TERNHUS DAM, CA.	▲	36	25	118	01	495.0	NS	561	1961	C OF E	2 JUN 68	6,610
211300	DRY CREEK NEAR LEHMOGVE, CA.	▲	36	27	118	02	870	TOPO	75.6	1969	USGS	6 DEC 66	14,000

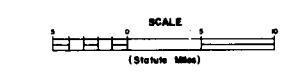
- TYPE OF GAGE
- ▲ WATER STAKE RECORDER
 - ▲ WATER STAKE RECORDER WITH RADIO TELEGRAMS
 - ▲ WATER STAKE RECORDER WITH TELEPHONE TELEMARK
 - RECORDING RESERVOIR GAGE, STAKE ONLY
 - ◆ WATER QUALITY STATION

- 1/ RECORDS SINCE 20 MAR 1968 INCLUDE FLOW DIVERTED TO TULE RIVER DIVERSION DITCH. PRIOR TO 20 MAR 1968 AT SITE 1.0 MI. (2.4 KM) UPSTREAM AT DIFFERENT DATUM.
- 2/ PRIOR TO 24 JUNE 1961 AT SITE 0.4 MI. (0.6 KM) DOWNSTREAM AT DIFFERENT DATUM.
- 3/ PRIOR TO 1 FEB 1961 AT SITE 0.5 MI. (0.8 KM) DOWNSTREAM AT DIFFERENT DATUM.
- 4/ PRIOR TO OCTOBER 1960 PUBLISHED AS " AT NORTH BRIDGE," NEAR PORTERVILLE.
- 5/ PRIOR TO OCTOBER 1960 RECORDS FOR RIVER AND CONDUIT PUBLISHED SEPARATELY; COMBINED FLOW ONLY, OCTOBER 1960 TO SEPTEMBER 1960.
- 6/ PRIOR TO OCTOBER 1962 COMBINED ONLY.
- 7/ FLOOD OF 25 DEC 1958 REACHED A STAGE OF 17.9 FT. (5.46 M) FROM FLOODMARKS.
- 8/ FLOOD OF 25 DEC 1958 REACHED A STAGE OF 9.5 FT. (2.90 M) FROM FLOODMARKS, DISCHARGE, 16,000 CFS/SEC (450 M³/SEC).
- 9/ PRIOR TO 6 MARCH 1969 1.6 MI. (2.6 KM) DOWNSTREAM AT DIFFERENT DATUM.

INDEX	STATION NAME	TYPE OF STATION	LOCATION				AGENCY
			LATITUDE	LONGITUDE	YEAR	MONTH	
202800	TULE RIVER NEAR SPRINGVILLE	▲	36 06	118 52	1967	USGS	
204600	TULE RIVER BELOW SUCES DAM	▲	36 04	118 55	1960	USGS	
204900	KANEAN RIVER AT THREE RIVERS	▲	36 27	118 54	1958	USGS	
210950	KANEAN RIVER BELOW TERNHUS DAM	▲	36 25	118 01	1961	USGS	

USGS - U.S. GEOLOGICAL SURVEY
 NSR - STATE OF CALIFORNIA, DEPARTMENT OF WATER RESOURCES

- LEGEND
- Drainage Boundary
 - U.S. Highway
 - Interstate Highway
 - Railroad
 - Levee
 - Intermittent Stream
 - Perennial Stream
 - Canal
 - Reservoir or Lake
 - Authorized Reservoir
 - Contour

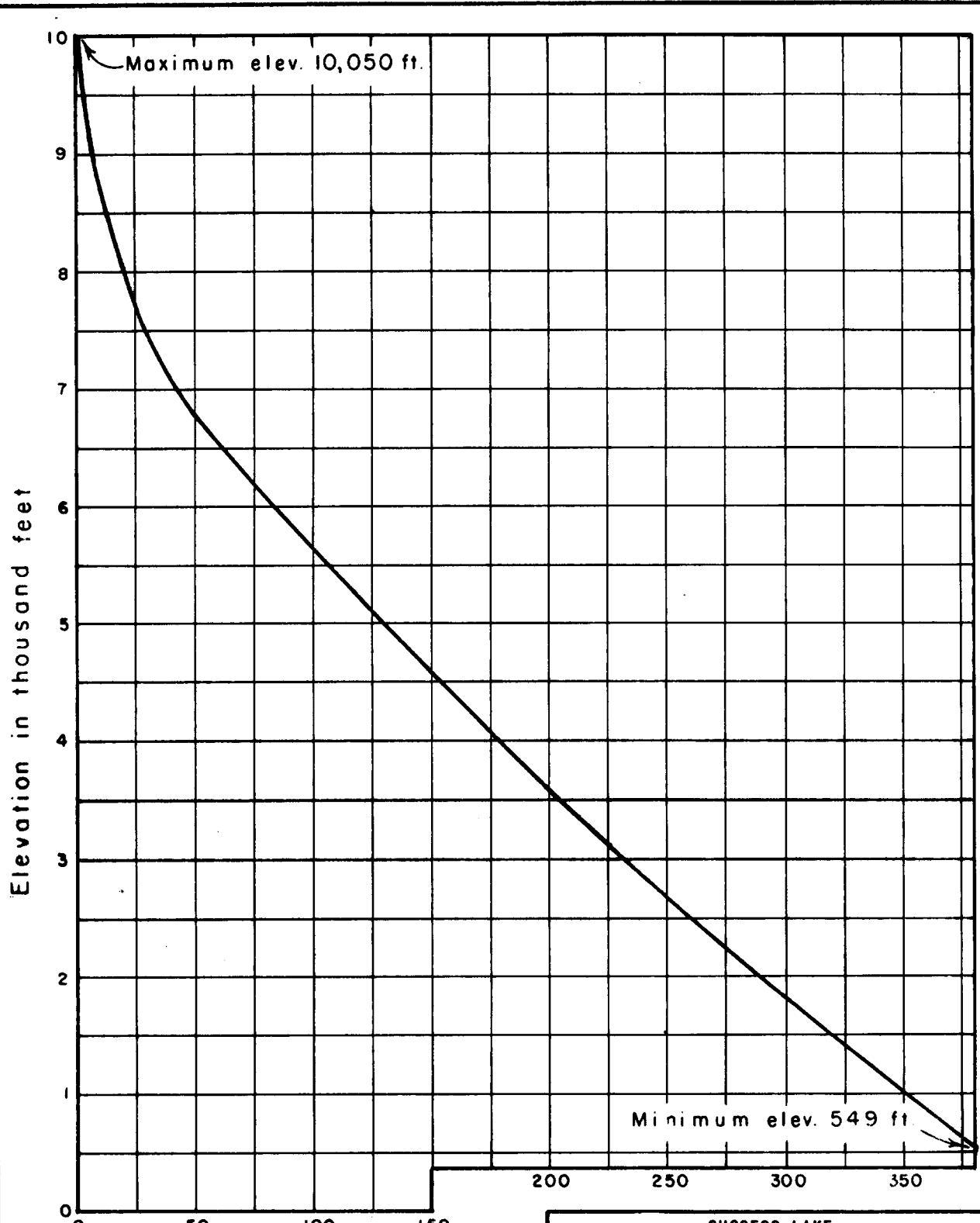


**SUCCESS LAKE
TULE RIVER, CALIFORNIA**

**TOPOGRAPHY AND
STREAM GAGING STATIONS**

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

Prepared: L.H.C. Date: SEPTEMBER 1981
 Drawn: L.H.C.

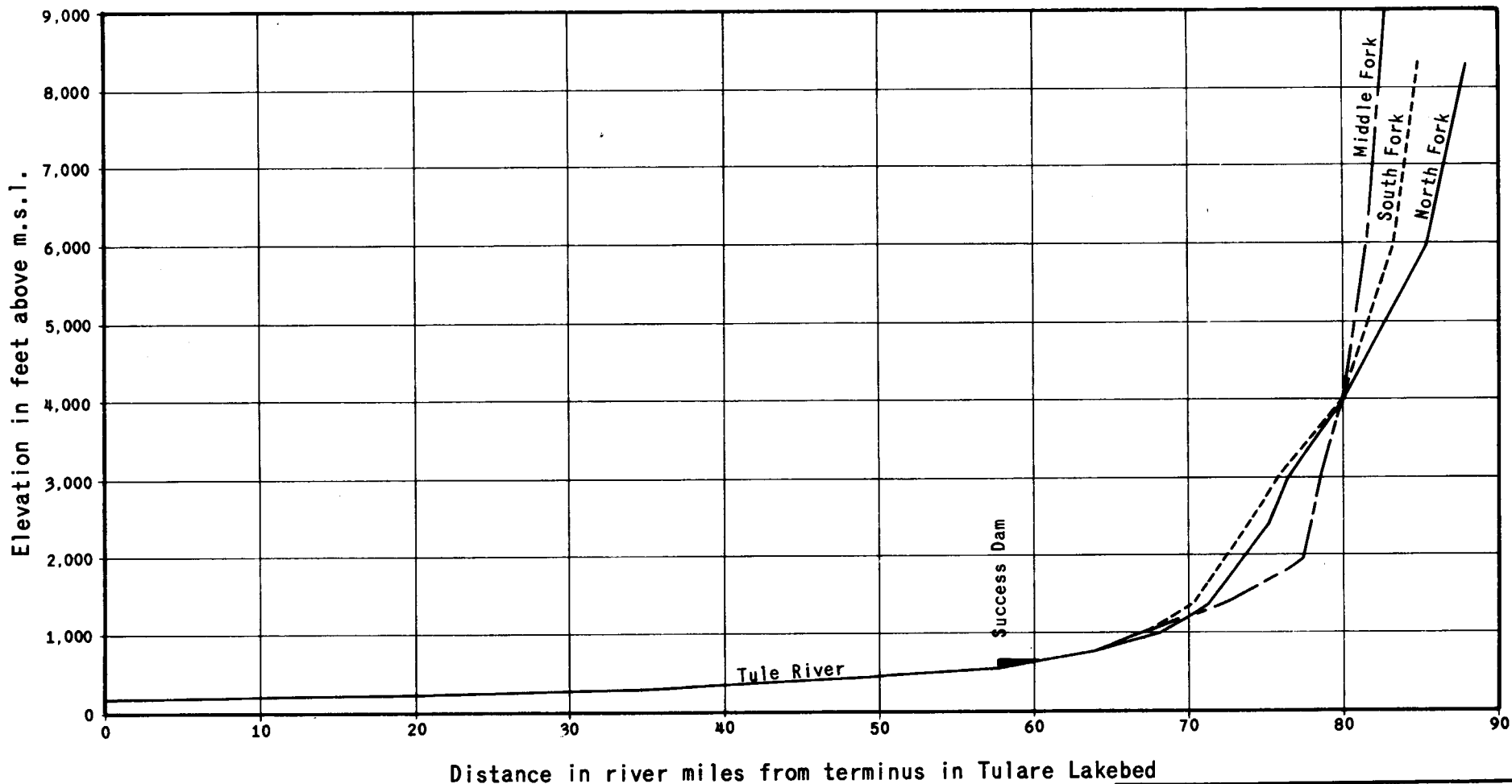


SUCCESS LAKE
TULE RIVER, CALIFORNIA

**AREA - ELEVATION CURVE
TULE RIVER BASIN**

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

Prepared: D.T.C. Date: August 1966



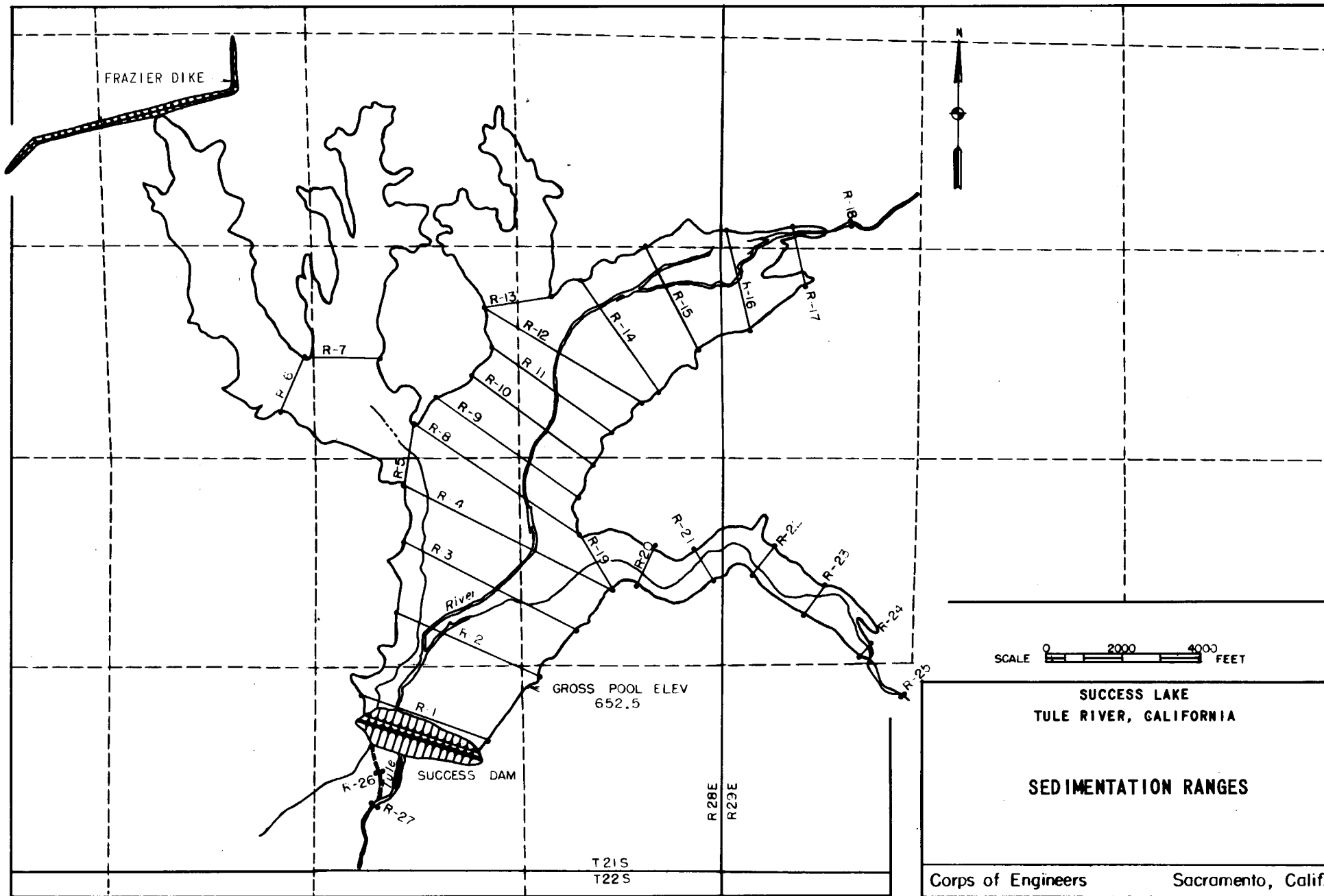
SUCCESS LAKE
TULE RIVER, CALIFORNIA

TULE RIVER
STREAM PROFILE

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

Prepared: L.H.C. Date: APRIL 1981
Drawn: L.H.C.

PLATE 10



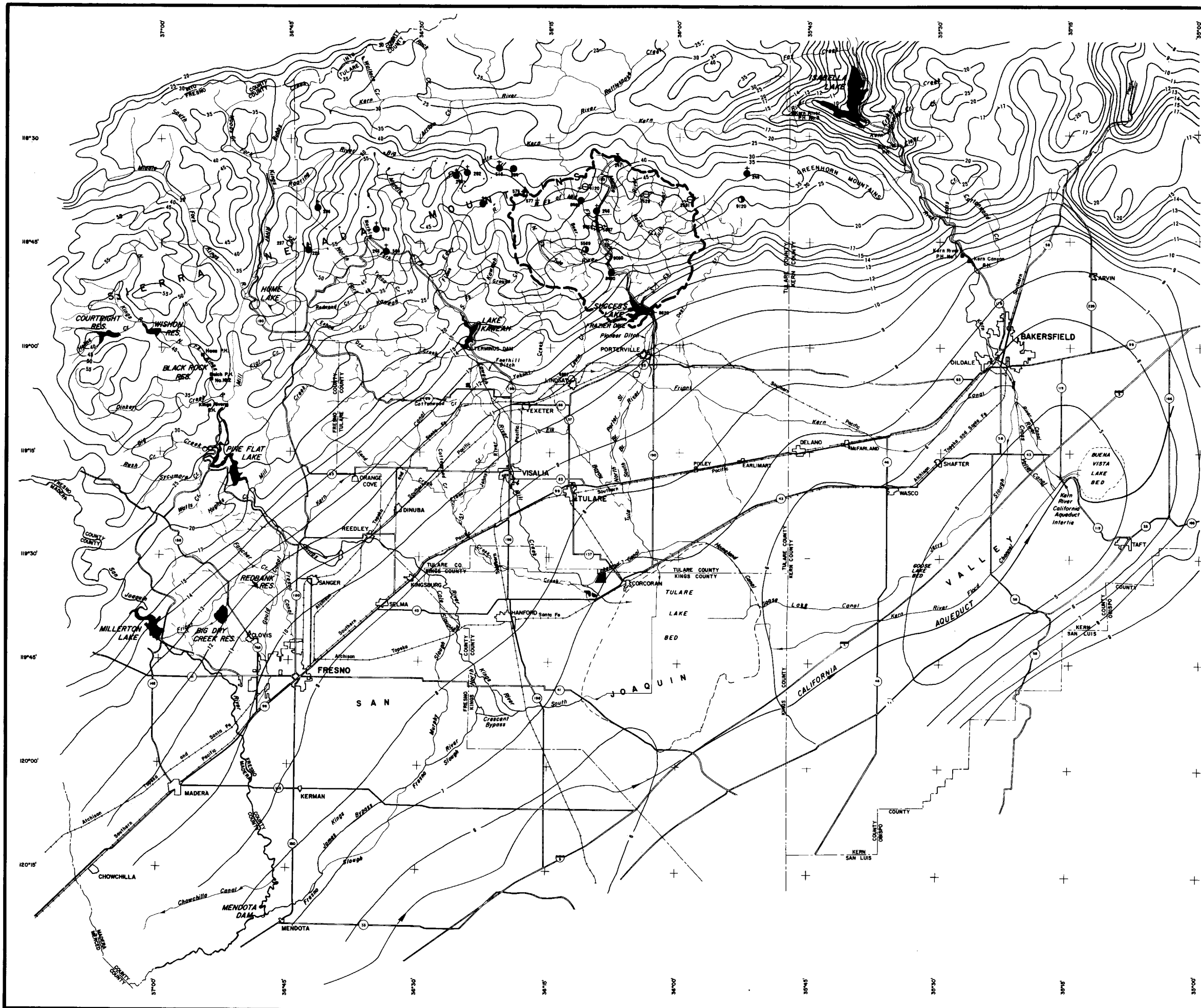
SCALE 0 2000 4000 FEET

SUCCESS LAKE
TULE RIVER, CALIFORNIA

SEDIMENTATION RANGES

Corps of Engineers Sacramento, Calif.
G.H.C. 13 AUG 1956 File: KT-I-26-176

PLATE 11



SNOW COURSE AND AERIAL SNOW DEPTH READINGS

GALT INDEX NUMBER	STATION	TYPE OF GAGE	ELEV. (FEET)	LOCATION				RECORD YEAR	MEASUREMENT DATES ^{1/}	MEASURED BY	APRIL WATER QUANTITY (CUBIC FEET)
				LONGITUDE	LATITUDE	SEASIDE	WIND				
517	BENTON POND	T	18,000	98	24	110	30	1900	2, 3, 4, 5	C. W. E.	27.4
518	CHAMBERS PLAZA	T	18,000	30	30	110	27	1905	2, 3, 4, 5	C. W. E.	21.8
511	NICHOLS HEADQUARTERS	T	8,000	36	36	110	42	1906	2, 3, 4, 5	C. W. E.	26.6
207	SCIENCE HEADQUARTERS	T	8,000	36	41	110	34	1924	2, 3	C. W. E. ^{2/}	26.4
202	FAREWELL GAP	T	9,500	35	25	110	35	1902	2, 3, 4, 5	S. B. C. E. P. ^{3/}	26.2
200	SHAWNEY LAKE	T	9,000	36	40	110	30	1924	2, 3, 4, 5	S. B. C. E. P. ^{3/}	26.0
201	WET HEADQUARTERS	T	8,000	36	21	110	34	1907	2, 3, 4, 5	S. B. C. E. P. ^{3/}	25.9
226	RODNEY HEADQUARTERS	T	8,000	36	40	110	42	1900	2, 3, 4, 5	S. B. C. E. P. ^{3/}	27.2
243	PARTNER HEADQUARTERS	T	8,000	36	10	110	42	1923	2, 3, 4, 5	S. B. C. E. P. ^{3/}	27.0
248	ROCKY HEADQUARTERS	T	8,000	36	23	110	30	1900	2, 3, 4, 5	S. B. C. E. P. ^{3/}	26.8
246	OLIVE HANDED STATION	T	8,000	36	18	110	30	1900	2, 3, 4, 5	S. B. C. E. P. ^{3/}	26.4
240	WINDMILL KING	T	8,000	36	20	110	35	1906	2, 3, 4, 5	S. B. C. E. P. ^{3/}	26.1
234	BIG HEADQUARTERS	T	7,000	36	40	110	51	1900	2, 3, 4, 5	S. B. C. E. P. ^{3/}	25.9
227	SHORE CANYON HEADQUARTERS	T	7,000	36	40	110	46	1900	2, 3, 4, 5	S. B. C. E. P. ^{3/}	27.2
279	1900 HEADQUARTERS	T	7,000	36	17	110	30	1924	2, 3, 4, 5	S. B. C. E. P. ^{3/}	27.0
180	DEAN HEADQUARTERS	T	7,000	36	42	110	30	1907	2, 3, 4, 5	S. B. C. E. P. ^{3/}	18.0
207	WINDMILL RIDGE	T	7,000	36	27	110	33	1907	2, 3, 4, 5	S. B. C. E. P. ^{3/}	18.0
246	OLD ENTERPRISE HILL	T	6,000	36	15	110	31	1907	2, 3, 4, 5	S. B. C. E. P. ^{3/}	18.0
248	SHAWNEY FOREST	T	6,000	36	29	110	46	1900	2, 3, 4, 5	S. B. C. E. P. ^{3/}	17.2

^{1/} RECORDS INDICATE DATE OF OBSERVATION; 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16, 17, 18, 19, 20, 21, 22, 23, 24, 25, 26, 27, 28, 29, 30, 31, 32, 33, 34, 35, 36, 37, 38, 39, 40, 41, 42, 43, 44, 45, 46, 47, 48, 49, 50, 51, 52, 53, 54, 55, 56, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 71, 72, 73, 74, 75, 76, 77, 78, 79, 80, 81, 82, 83, 84, 85, 86, 87, 88, 89, 90, 91, 92, 93, 94, 95, 96, 97, 98, 99, 100, 101, 102, 103, 104, 105, 106, 107, 108, 109, 110, 111, 112, 113, 114, 115, 116, 117, 118, 119, 120, 121, 122, 123, 124, 125, 126, 127, 128, 129, 130, 131, 132, 133, 134, 135, 136, 137, 138, 139, 140, 141, 142, 143, 144, 145, 146, 147, 148, 149, 150, 151, 152, 153, 154, 155, 156, 157, 158, 159, 160, 161, 162, 163, 164, 165, 166, 167, 168, 169, 170, 171, 172, 173, 174, 175, 176, 177, 178, 179, 180, 181, 182, 183, 184, 185, 186, 187, 188, 189, 190, 191, 192, 193, 194, 195, 196, 197, 198, 199, 200, 201, 202, 203, 204, 205, 206, 207, 208, 209, 210, 211, 212, 213, 214, 215, 216, 217, 218, 219, 220, 221, 222, 223, 224, 225, 226, 227, 228, 229, 230, 231, 232, 233, 234, 235, 236, 237, 238, 239, 240, 241, 242, 243, 244, 245, 246, 247, 248, 249, 250, 251, 252, 253, 254, 255, 256, 257, 258, 259, 260, 261, 262, 263, 264, 265, 266, 267, 268, 269, 270, 271, 272, 273, 274, 275, 276, 277, 278, 279, 280, 281, 282, 283, 284, 285, 286, 287, 288, 289, 290, 291, 292, 293, 294, 295, 296, 297, 298, 299, 300, 301, 302, 303, 304, 305, 306, 307, 308, 309, 310, 311, 312, 313, 314, 315, 316, 317, 318, 319, 320, 321, 322, 323, 324, 325, 326, 327, 328, 329, 330, 331, 332, 333, 334, 335, 336, 337, 338, 339, 340, 341, 342, 343, 344, 345, 346, 347, 348, 349, 350, 351, 352, 353, 354, 355, 356, 357, 358, 359, 360, 361, 362, 363, 364, 365, 366, 367, 368, 369, 370, 371, 372, 373, 374, 375, 376, 377, 378, 379, 380, 381, 382, 383, 384, 385, 386, 387, 388, 389, 390, 391, 392, 393, 394, 395, 396, 397, 398, 399, 400, 401, 402, 403, 404, 405, 406, 407, 408, 409, 410, 411, 412, 413, 414, 415, 416, 417, 418, 419, 420, 421, 422, 423, 424, 425, 426, 427, 428, 429, 430, 431, 432, 433, 434, 435, 436, 437, 438, 439, 440, 441, 442, 443, 444, 445, 446, 447, 448, 449, 450, 451, 452, 453, 454, 455, 456, 457, 458, 459, 460, 461, 462, 463, 464, 465, 466, 467, 468, 469, 470, 471, 472, 473, 474, 475, 476, 477, 478, 479, 480, 481, 482, 483, 484, 485, 486, 487, 488, 489, 490, 491, 492, 493, 494, 495, 496, 497, 498, 499, 500, 501, 502, 503, 504, 505, 506, 507, 508, 509, 510, 511, 512, 513, 514, 515, 516, 517, 518, 519, 520, 521, 522, 523, 524, 525, 526, 527, 528, 529, 530, 531, 532, 533, 534, 535, 536, 537, 538, 539, 540, 541, 542, 543, 544, 545, 546, 547, 548, 549, 550, 551, 552, 553, 554, 555, 556, 557, 558, 559, 560, 561, 562, 563, 564, 565, 566, 567, 568, 569, 570, 571, 572, 573, 574, 575, 576, 577, 578, 579, 580, 581, 582, 583, 584, 585, 586, 587, 588, 589, 590, 591, 592, 593, 594, 595, 596, 597, 598, 599, 600, 601, 602, 603, 604, 605, 606, 607, 608, 609, 610, 611, 612, 613, 614, 615, 616, 617, 618, 619, 620, 621, 622, 623, 624, 625, 626, 627, 628, 629, 630, 631, 632, 633, 634, 635, 636, 637, 638, 639, 640, 641, 642, 643, 644, 645, 646, 647, 648, 649, 650, 651, 652, 653, 654, 655, 656, 657, 658, 659, 660, 661, 662, 663, 664, 665, 666, 667, 668, 669, 670, 671, 672, 673, 674, 675, 676, 677, 678, 679, 680, 681, 682, 683, 684, 685, 686, 687, 688, 689, 690, 691, 692, 693, 694, 695, 696, 697, 698, 699, 700, 701, 702, 703, 704, 705, 706, 707, 708, 709, 710, 711, 712, 713, 714, 715, 716, 717, 718, 719, 720, 721, 722, 723, 724, 725, 726, 727, 728, 729, 730, 731, 732, 733, 734, 735, 736, 737, 738, 739, 740, 741, 742, 743, 744, 745, 746, 747, 748, 749, 750, 751, 752, 753, 754, 755, 756, 757, 758, 759, 760, 761, 762, 763, 764, 765, 766, 767, 768, 769, 770, 771, 772, 773, 774, 775, 776, 777, 778, 779, 780, 781, 782, 783, 784, 785, 786, 787, 788, 789, 790, 791, 792, 793, 794, 795, 796, 797, 798, 799, 800, 801, 802, 803, 804, 805, 806, 807, 808, 809, 810, 811, 812, 813, 814, 815, 816, 817, 818, 819, 820, 821, 822, 823, 824, 825, 826, 827, 828, 829, 830, 831, 832, 833, 834, 835, 836, 837, 838, 839, 840, 841, 842, 843, 844, 845, 846, 847, 848, 849, 850, 851, 852, 853, 854, 855, 856, 857, 858, 859, 860, 861, 862, 863, 864, 865, 866, 867, 868, 869, 870, 871, 872, 873, 874, 875, 876, 877, 878, 879, 880, 881, 882, 883, 884, 885, 886, 887, 888, 889, 890, 891, 892, 893, 894, 895, 896, 897, 898, 899, 900, 901, 902, 903, 904, 905, 906, 907, 908, 909, 910, 911, 912, 913, 914, 915, 916, 917, 918, 919, 920, 921, 922, 923, 924, 925, 926, 927, 928, 929, 930, 931, 932, 933, 934, 935, 936, 937, 938, 939, 940, 941, 942, 943, 944, 945, 946, 947, 948, 949, 950, 951, 952, 953, 954, 955, 956, 957, 958, 959, 960, 961, 962, 963, 964, 965, 966, 967, 968, 969, 970, 971, 972, 973, 974, 975, 976, 977, 978, 979, 980, 981, 982, 983, 984, 985, 986, 987, 988, 989, 990, 991, 992, 993, 994, 995, 996, 997, 998, 999, 1000.

LEGEND

- SNOW COURSE
- AERIAL SNOW DEPTH GAGE
- SNOW COURSE WITH AERIAL SNOW DEPTH GAGE
- RADIO REPORTING SNOW FILLING
- RADIO REPORTING SNOW FILLING WITH AERIAL SNOW DEPTH GAGE

CLIMATOLOGICAL STATIONS

INDEX NUMBER	STATION	ELEV. (FEET)	TYPE OF GAGE	LOCATION		RECORD YEAR	PUBLISHED BY		
				LATITUDE	LONGITUDE				
0000	SUCCESS LAKE	100	○	36	08	110	55	1900	COE
7077	WINTERVILLE	200	○	36	08	110	01	1900	ORNL
0007	LIMBURY	300	○	36	11	110	04	1913	ORNL
7079	WINTERVILLE S.W.	110	○	36	08	110	04	1900	ORNL
5205-10	DEAN HEADQUARTERS	900	○	36	37	110	51	1900	ORNL
0000	SPRINGVILLE 83	1000	○	36	06	110	48	1901	ORNL
0000	TRIA RIVER PD	1200	○	36	04	110	47	1910	COE
0000	TRIA RIVER INTAKE	2000	○	36	10	110	42	1910	COE
0000	HILA S.W.	2000	○	36	17	110	46	1907	ORNL
0000	HILA S.E.	2000	○	36	23	110	26	1905	ORNL
0000	SPRINGVILLE TULE RD.	4000	○	36	12	110	29	1907	ORNL
1125	CAMP WELAND	1600	○	36	06	110	26	1900	ORNL
5407	WINDMILL RIDGE	2000	○	36	15	110	40	1902	COE
7020	SHORE CANYON	4200	○	36	04	110	26	1904	COE
2001	FAIR CREEK	6000	○	36	50	110	20	1900	ORNL
4120	ORANGE (DAP)	7100	○	36	11	110	27	1900	ORNL

^{1/} RECORDS NOT PUBLISHED
 COE - CORPS OF ENGINEERS, DEPARTMENT OF THE ARMY
 ORNL - DEPARTMENT OF WATER RESOURCES, STATE OF CALIFORNIA
 ORNL - NATIONAL GEODESIC AND ATMOSPHERIC ADMINISTRATION

LEGEND

- Drainage Boundary
- U.S. Highway
- Interstate Highway
- Railroad
- Levee
- Intermittent Stream
- Perennial Stream
- Canal
- Reservoir or Lake
- Authorized Reservoir
- Isohyets

LEGEND FOR CLIMATOLOGICAL STATIONS

- RECORDING AND NON-RECORDING
- PRECIPITATION STATION
- PRECIPITATION STORM
- PRECIPITATION AND TEMPERATURE
- PRECIPITATION, TEMPERATURE AND EVAPORATION
- COMPLETE METEOROLOGICAL STATION
- STATION WITH COMPLETE RECORDS

SCALE
 (Statute Miles)

**SUCCESS LAKE
 TULE RIVER, CALIFORNIA**

**NORMAL ANNUAL PRECIPITATION,
 CLIMATOLOGICAL STATIONS
 AND SNOW COURSES**

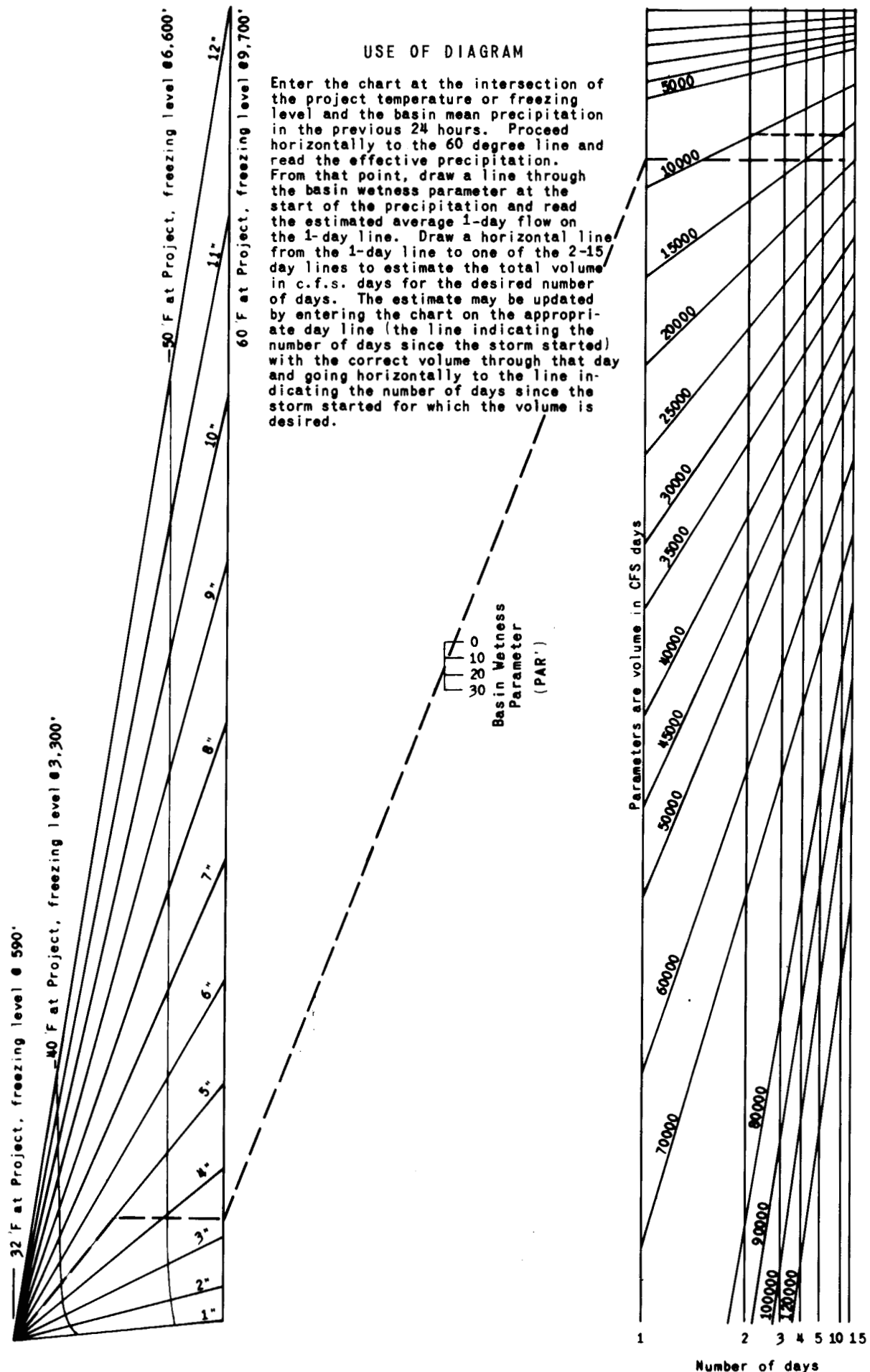
CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

Prepared: L.H.C. Date: SEPTEMBER 1981
 Drawn: L.H.C.

HISTORICAL UNIMPAIRED FLOW BELOW SUCCESS DAM

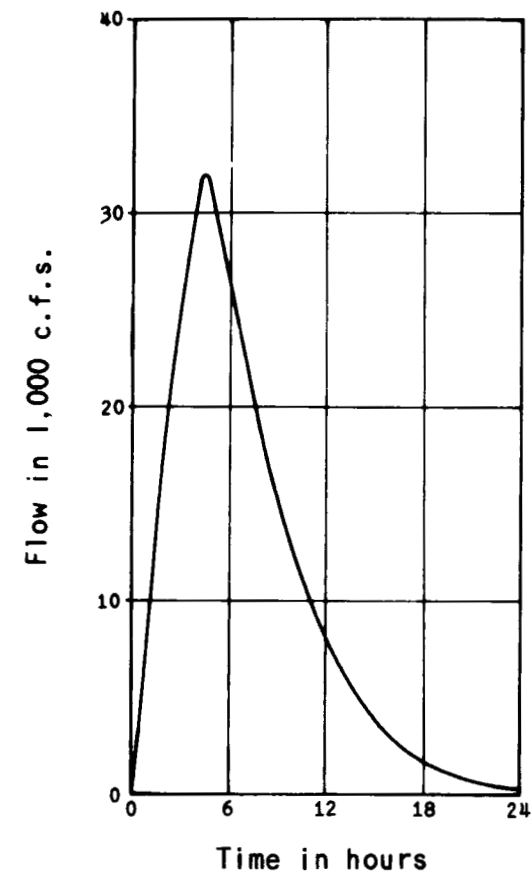
(Runoff in 1,000 acre-feet)

WATER YEAR	OCT	NOV	DEC	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	ANNUAL TOTAL
1904	1.2	1.8	2.3	2.7	9.7	24.5	22.1	20.8	6.0	1.5	0.9	1.7	95.2
1905	4.5	2.3	3.0	5.1	7.2	21.0	17.7	26.7	12.7	3.1	0.8	0.7	104.8
1906	1.0	3.9	9.3	44.6	16.5	122.2	64.7	90.4	75.5	29.2	7.6	4.4	469.3
1907	3.8	4.5	8.9	19.7	21.7	29.5	60.1	26.9	20.3	6.9	3.0	2.3	207.6
1908	3.7	4.4	9.3	10.2	20.6	24.2	14.3	13.4	6.4	1.5	0.8	1.4	110.2
1909	2.5	2.7	3.7	77.5	70.2	45.4	61.6	59.2	45.3	13.3	4.3	3.0	388.7
1910	3.5	7.0	49.3	28.2	13.2	17.3	17.4	12.1	4.1	1.4	0.5	0.8	154.8
1911	1.6	2.6	4.0	22.2	19.0	35.2	26.2	20.2	12.1	3.7	1.3	1.0	149.1
1912	1.9	3.2	3.8	4.9	4.2	7.4	14.3	16.1	8.4	1.2	0.2	0.3	65.9
1913	0.6	1.4	2.0	2.8	2.7	7.1	10.2	7.2	3.5	0.6	0.1	0.3	38.5
1914	0.2	2.8	5.5	62.7	19.8	19.0	21.5	20.5	11.0	2.9	0.6	0.4	166.9
1915	1.1	1.6	3.5	6.2	13.2	14.5	20.1	52.8	20.2	4.7	1.0	0.7	139.6
1916	0.7	2.4	6.1	85.0	48.7	74.2	52.8	43.1	23.0	7.9	2.9	1.5	348.3
1917	7.5	5.1	17.9	12.8	26.4	22.2	30.5	31.6	21.0	4.8	1.6	0.7	182.1
1918	1.2	2.3	2.9	3.2	4.6	16.7	11.1	7.6	2.6	0.2	0.1	0.2	52.7
1919	0.9	2.2	4.0	3.4	8.7	18.8	20.7	15.1	3.5	0.3	0.0	0.0	77.6
1920	0.7	1.3	5.6	2.6	3.2	25.7	36.3	24.7	11.1	2.0	0.3	0.5	114.6
1921	1.2	2.6	4.8	7.1	11.9	19.9	13.3	18.7	10.9	1.5	0.2	0.1	92.2
1922	0.5	1.1	7.7	10.8	19.6	19.7	24.8	38.6	16.6	3.0	0.5	0.2	143.1
1923	0.8	2.9	10.9	7.1	8.1	8.0	37.9	18.7	7.3	1.7	0.4	0.5	104.3
1924	1.1	1.6	2.2	2.6	2.7	3.7	8.2	2.5	0.1	0.0	0.0	0.0	24.7
1925	0.2	4.1	8.0	6.7	13.0	13.2	20.0	15.6	5.9	1.1	0.1	0.1	88.0
1926	1.2	2.1	2.8	2.3	6.2	7.5	18.0	8.7	1.2	0.1	0.0	0.0	50.1
1927	0.0	9.2	5.2	5.2	35.9	23.7	23.6	21.7	9.2	1.3	0.1	0.2	135.3
1928	0.7	5.9	3.5	3.9	4.3	15.6	10.2	4.3	0.5	0.0	0.0	0.0	48.9
1929	0.0	1.2	3.4	3.0	4.8	10.8	14.3	13.0	4.8	0.3	0.0	0.0	55.6
1930	0.0	0.2	0.7	2.3	4.9	12.0	9.7	12.8	4.1	0.2	0.0	0.0	46.9
1931	0.1	1.5	2.0	3.8	3.5	3.4	3.0	2.4	0.3	0.0	0.0	0.0	20.0
1932	0.0	0.2	12.9	9.3	26.5	19.7	20.2	29.3	13.6	2.3	0.3	0.0	134.3
1933	0.3	0.7	2.1	9.0	6.9	14.4	14.6	16.9	14.4	2.0	0.1	0.0	81.4
1934	0.1	0.8	4.2	5.3	3.8	5.1	2.0	0.4	0.3	0.0	0.0	0.0	22.0
1935	0.0	1.6	2.9	4.5	6.9	11.9	32.4	20.7	8.6	1.1	0.1	0.0	90.7
1936	0.4	1.1	2.1	4.1	46.6	23.5	43.9	27.7	11.0	2.4	0.4	0.2	163.4
1937	0.9	1.9	5.7	8.8	73.9	56.1	59.5	51.6	20.4	5.6	1.3	0.7	286.4
1938	1.1	2.1	24.5	10.7	29.9	92.0	63.1	68.0	31.5	8.9	3.0	1.8	336.6
1939	3.0	4.3	5.4	6.9	10.3	19.4	21.2	9.3	2.5	0.4	0.0	0.1	82.8
1940	1.1	1.1	2.1	37.2	49.6	35.0	37.0	24.2	7.4	1.3	0.3	0.3	196.6
1941	1.4	2.7	13.4	16.5	40.5	34.3	41.5	45.4	22.5	6.1	1.9	1.2	227.4
1942	2.1	3.3	9.8	17.1	13.0	19.1	27.4	25.2	14.6	2.9	0.7	0.4	135.6
1943	0.8	3.1	7.1	40.3	25.5	144.4	56.0	36.2	15.3	5.2	1.9	1.1	336.9
1944	1.9	3.3	5.0	7.8	11.5	19.2	16.1	24.5	11.0	2.6	0.9	0.7	104.5
1945	0.6	7.7	5.8	4.8	50.2	38.3	43.2	36.1	19.5	4.6	1.3	0.7	212.8
1946	2.2	4.7	13.0	13.4	9.5	15.3	20.1	14.2	5.1	0.6	0.0	0.0	98.1
1947	0.9	7.4	10.4	6.0	5.9	9.0	7.5	5.5	1.4	0.0	0.0	0.0	54.0
1948	0.1	1.3	2.0	1.7	2.6	6.1	24.3	20.9	7.4	0.8	0.0	0.0	67.2
1949	0.0	0.9	1.7	3.5	4.0	9.5	15.7	11.0	2.5	0.3	0.0	0.0	49.1
1950	0.0	1.4	2.2	6.6	18.2	8.9	15.5	8.9	2.9	0.1	0.0	0.0	64.7
1951	1.5	42.3	29.4	13.8	11.4	16.9	11.4	12.7	3.6	0.5	0.0	0.0	143.5
1952	2.0	13.2	18.8	40.4	26.0	60.7	58.9	58.5	28.2	8.4	3.1	1.7	319.9
1953	1.5	4.0	6.3	24.1	8.7	9.6	15.8	15.6	10.3	2.3	0.5	0.0	98.7
1954	0.5	2.1	3.5	7.5	9.9	16.3	24.9	15.3	4.0	0.3	0.0	0.0	84.3
1955	0.2	1.6	3.8	8.0	12.7	9.3	7.2	11.7	3.5	0.2	0.0	0.0	58.2
1956	0.0	1.1	56.4	45.3	21.0	15.4	22.1	30.9	10.7	1.2	0.3	0.2	204.6
1957	1.4	1.2	1.6	3.6	6.0	8.5	6.8	22.8	7.1	0.4	0.0	0.0	59.4
1958	1.0	2.4	5.6	8.3	17.0	45.5	62.9	46.5	21.8	5.6	1.1	0.7	218.4
1959	0.6	1.9	2.0	3.4	6.7	6.8	3.7	1.9	0.2	0.0	0.0	0.0	27.2
1960	0.0	0.2	0.5	1.5	10.8	10.1	8.5	9.1	1.1	0.1	0.0	0.0	41.9
1961	0.0	1.7	2.7	2.1	2.2	3.7	4.1	2.5	0.6	0.0	0.0	0.0	19.6
1962	0.0	0.3	1.6	2.7	23.5	13.6	23.8	13.3	6.3	0.9	0.2	0.2	86.4
1963	0.8	1.1	1.2	10.0	29.0	10.1	26.3	25.3	9.7	3.8	1.9	1.3	120.5
1964	2.1	5.2	3.9	3.9	3.4	7.5	14.6	13.3	5.2	0.7	0.2	0.4	60.4
1965	0.7	4.6	17.2	23.6	12.0	10.9	29.2	20.7	12.3	3.4	2.0	1.2	137.8
1966	0.8	4.3	6.0	6.9	6.5	8.5	8.1	4.3	1.2	0.5	0.0	0.1	47.2
1967	0.3	2.1	138.5	16.9	16.8	24.9	50.7	65.6	34.2	14.7	5.3	4.0	374.0
1968	2.7	4.5	6.9	7.5	10.7	12.5	10.8	7.6	2.9	0.9	0.0	0.2	67.2
1969	1.6	4.1	5.5	99.5	86.5	71.0	83.1	73.7	46.9	20.0	7.9	4.1	503.9
1970	4.5	4.8	7.5	34.1	13.3	24.1	12.0	2.9	5.9	2.0	0.8	0.3	112.2
1971	0.8	5.1	7.9	11.7	9.5	10.6	11.2	15.1	8.3	2.8	0.8	0.2	84.0
1972	1.0	2.6	6.3	5.3	5.8	5.8	3.9	2.8	0.8	0.1	0.0	0.3	34.7
1973	0.9	3.7	6.4	27.2	26.7	40.7	36.4	47.4	21.0	7.3	4.4	3.1	225.2
1974	2.8	5.3	9.1	23.9	9.6	26.9	35.6	22.2	11.2	5.4	3.6	1.1	156.7
1975	2.2	3.6	5.1	5.5	12.5	19.8	17.2	31.2	15.5	4.9	2.8	2.1	122.4
1976	3.6	3.6	4.6	3.3	4.6	8.2	6.5	4.4	1.2	0.5	0.1	0.9	41.6
1977	1.4	1.3	1.6	2.5	2.0	2.2	1.6	2.5	0.5	0.0	0.1	0.0	15.8
1978	0.1	0.5	8.1	16.3	48.4	62.7	46.6	41.5	29.6	10.3	3.7	4.8	272.6
1979	2.6	3.4	5.7	7.1	12.5	22.7	20.6	22.8	8.3	4.0	2.7	1.7	114.1
1980	2.1	3.2	3.5	73.0	73.1	53.2	37.0	35.9	26.6	12.2	6.3	2.8	328.9
MEAN	1.3	3.5	9.1	15.6	18.2	24.4	25.3	23.4	11.4	3.3	1.1	0.8	137.4



USE OF DIAGRAM

Enter the chart at the intersection of the project temperature or freezing level and the basin mean precipitation in the previous 24 hours. Proceed horizontally to the 60 degree line and read the effective precipitation. From that point, draw a line through the basin wetness parameter at the start of the precipitation and read the estimated average 1-day flow on the 1-day line. Draw a horizontal line from the 1-day line to one of the 2-15 day lines to estimate the total volume in c.f.s. days for the desired number of days. The estimate may be updated by entering the chart on the appropriate day line (the line indicating the number of days since the storm started) with the correct volume through that day and going horizontally to the line indicating the number of days since the storm started for which the volume is desired.



UNIT HYDROGRAPH	
TIME IN HOURS	FLOW IN CFS
2	10,195
4	25,752
6	30,586
8	21,208
10	14,775
12	9,952
14	5,835
16	3,744
18	2,119
20	1,217
22	690
24	461
2	178

Drainage Area - 393 sq. mi.

2-Hour Unit Hydrograph

EXAMPLE 1

FIND:
 Estimated average flow on 15 January.
 Estimated 10-day volume from 15 January through 24 January.

GIVEN:
 Basin mean precipitation (BMP) on 14 January = 5 inches.
 Average temperature at Lake Success on 14 January = 45°F.
 Basin wetness parameter (PAR') for 13 January = 15 inches.

FROM CHART:
 15 January flow estimate = 8,100 c.f.s.
 10-day volume (15-24 Jan) = 18,100 c.f.s. days.

EXAMPLE 2

FIND:
 Update 15 January through 24 January volume estimate on 17 January.

GIVEN:
 Average daily flows on 15 and 16 January are 7,000 c.f.s. and 2,800 c.f.s.
 BMP on 15 and 16 January equals zero.

FROM CHART:
 Use 2-day volume = 9,800 c.f.s.; therefore, the updated 15-24 January volume (10 days) estimate is 15,500 c.f.s. day.

NOTE:
 Computations of PAR' and BMP are found in paragraph A-3f.

LOSS IN INCHES DURING 2-HOUR PERIOD AS A FUNCTION OF PRECIPITATION AND ACCUMULATED LOSS

Precipitation in Inches During 2-Hour Period

	1	2	3	4	5
0	1.0	2.0	3.0	4.0	5.0
2	.9	1.5	2.2	2.8	3.4
4	.8	1.5	2.1	2.6	3.2
6	.8	1.4	2.0	2.5	3.0
8	.7	1.3	1.9	2.4	2.9
10	.7	1.2	1.8	2.2	2.7
12	.7	1.2	1.7	2.1	2.6
14	.6	1.1	1.6	2.0	2.4
16	.6	1.1	1.5	1.9	2.3
18	.6	1.0	1.4	1.8	2.2
20	.5	1.0	1.4	1.7	2.1

SUCCESS LAKE
 TULE RIVER, CALIFORNIA

RAINFLOOD FORECAST CRITERIA

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

Prepared: H.T.M. Date: MAY 1981
 Drawn: L.H.C.

SUMMARY OF FORECASTED AND ACTUAL SNOWMELT RUNOFF INTO SUCCESS LAKE

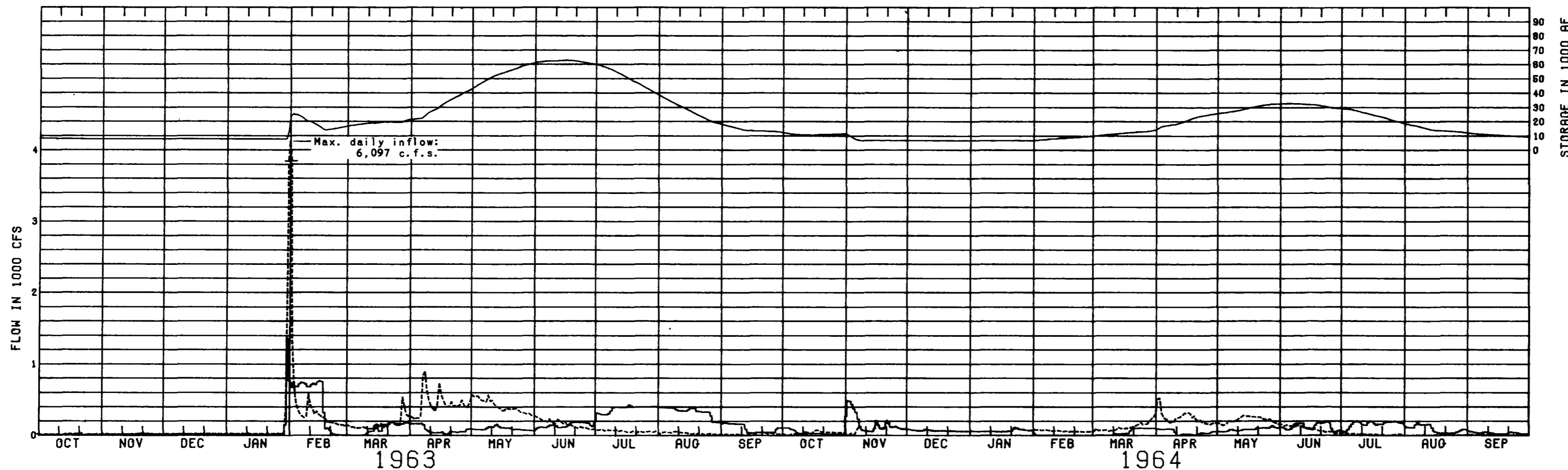
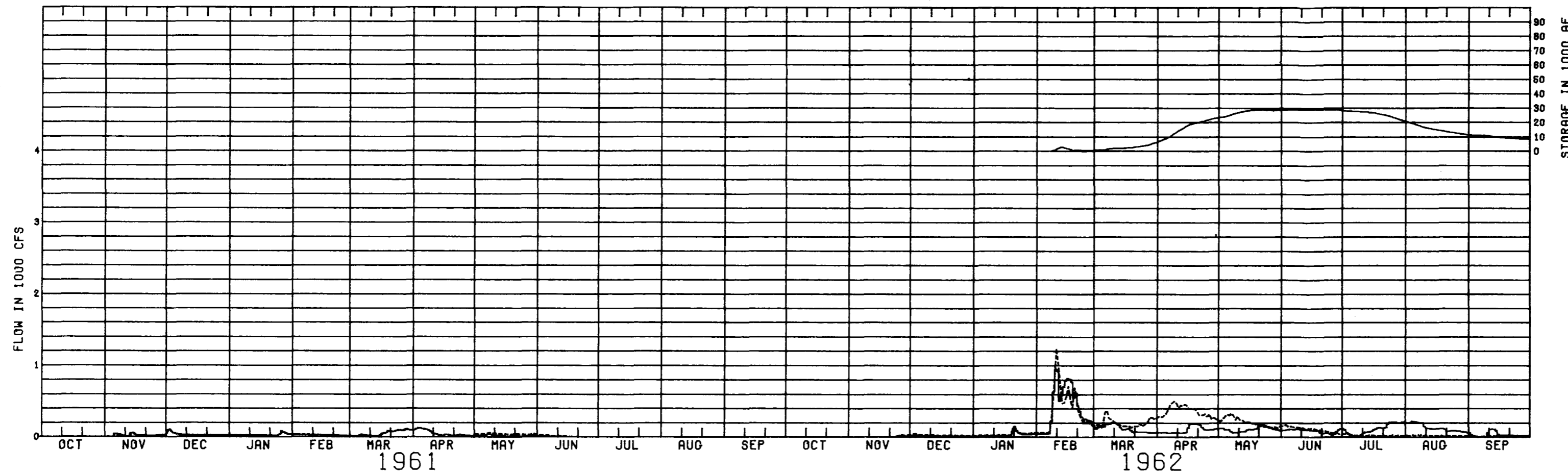
(Flow in 1,000 acre-feet)

WATER YEAR	ACTUAL	I APRIL THROUGH 3I JULY								
		I FEBRUARY			I MARCH			I APRIL		
		FORECAST	ERROR	% ERROR	FORECAST	ERROR	% ERROR	FORECAST	ERROR	% ERROR
1953	44	NR	NR	NR	NR	NR	NR	27	- 17	- 63
1954	45	NR	NR	NR	35	- 10	- 29	35	- 10	- 29
1955	23	NR	NR	NR	43	+ 20	+ 47	25	+ 2	+ 8
1956	65	55	- 10	- 18	55	- 10	- 18	30	- 35	- 117
1957	37	NR	NR	NR	NR	NR	NR	16	- 21	- 131
1958	137	NR	NR	NR	47	- 90	- 191	110	- 27	- 25
1959	6	22	+ 16	+ 73	28	+ 22	+ 79	11	+ 5	+ 45
1960	19	20	+ 1	+ 5	30	+ 11	+ 37	12	- 7	- 58
1961	7	22	+ 15	+ 68	7	0	0	10	+ 3	+ 30
1962	44	23	- 21	- 91	65	+ 21	+ 32	22	- 22	- 100
1963	65	20	- 45	- 225	15	- 50	- 333	58	- 7	- 12
1964	34	33	- 1	- 3	22	- 12	- 55	28	- 6	- 21
1965	66	75	+ 9	+ 12	45	- 21	- 47	56	- 10	- 18
1966	14	50	+ 36	+ 72	30	- 36	- 120	25	- 41	- 164
1967	165	75	- 90	- 120	60	- 105	- 175	80	- 85	- 106
1968	22	45	+ 23	+ 51	30	+ 8	+ 27	32	+ 10	+ 31
1969	224	95	- 129	- 136	200	- 24	- 12	220	- 4	- 2
1970	23	45	+ 22	+ 49	40	+ 17	+ 43	40	+ 17	+ 43
1971	37	50	+ 13	+ 26	35	- 2	- 6	30	- 7	- 23
1972	8	30	+ 22	+ 73	20	+ 12	+ 60	12	+ 4	+ 33
1973	112	80	- 32	- 40	90	- 22	- 24	150	+ 38	+ 25
1974	74	60	- 14	- 23	45	- 29	- 64	55	- 19	- 35
1975	69	23	- 46	- 200	32	- 37	- 116	55	- 14	- 25
1976	13	16	+ 3	+ 19	12	- 1	- 8	12	- 1	- 8
1977	5	14	+ 9	+ 64	5	0	0	4	- 1	- 25
1978	128	75	- 53	- 71	95	- 33	- 35	120	- 8	- 7
1979	56	40	- 16	- 40	50	- 6	- 12	65	+ 9	+ 14
1980	112	70	- 42	- 60	115	+ 3	+ 3	125	+ 13	+ 10
Mean (+)	59	45	+ 15	+ 47	48	+ 14	+ 41	53	+ 11	+ 27
Mean (-)	--	--	- 42	- 86	--	- 31	- 78	--	- 18	- 51
Extreme (+)	224	95	+ 36	+ 73	200	+ 22	+ 79	220	+ 38	+ 45
Extreme (-)	--	--	- 129	- 225	--	- 105	- 333	--	- 85	- 164

GIVEN DATE THROUGH 3I JULY									
I MAY				I JUNE					
ACTUAL	FORECAST	ERROR	% ERROR	ACTUAL	FORECAST	ERROR	% ERROR		
28	9	- 19	- 211	13	NR	NR	NR		
20	25	+ 5	+ 20	4	NR	NR	NR		
15	19	+ 4	+ 21	4	NR	NR	NR		
43	20	- 23	- 115	12	NR	NR	NR		
30	10	- 20	- 200	7	8	+ 1	+ 13		
74	NR	NR	NR	27	20	- 7	- 35		
2	NR	NR	NR	0	NR	NR	NR		
10	5	- 5	- 100	1	NR	NR	NR		
3	NR	NR	NR	1	NR	NR	NR		
20	39	+ 19	+ 49	7	NR	NR	NR		
39	19	- 20	- 105	14	NR	NR	NR		
19	13	- 6	- 46	6	NR	NR	NR		
35	26	- 9	- 35	16	NR	NR	NR		
6	5	- 1	- 20	2	NR	NR	NR		
115	100	- 15	- 15	49	NR	NR	NR		
11	16	+ 5	+ 31	4	NR	NR	NR		
141	137	- 4	- 3	67	60	- 7	- 12		
11	20	+ 9	+ 45	8	NR	NR	NR		
26	14	- 12	- 86	11	NR	NR	NR		
4	3	- 1	- 33	1	NR	NR	NR		
76	95	+ 19	+ 20	28	NR	NR	NR		
39	30	- 9	- 30	17	NR	NR	NR		
52	45	- 7	- 16	20	NR	NR	NR		
6	5	- 1	- 20	2	NR	NR	NR		
3	1	- 2	- 200	1	NR	NR	NR		
81	90	- 9	- 10	40	NR	NR	NR		
35	30	- 5	- 17	12	NR	NR	NR		
75	75	0	0	39	NR	NR	NR		
36	34	+ 12	+ 31	15	NR	NR	NR		
--	--	- 9	- 70	--	NR	NR	NR		
141	137	+ 20	+ 49	67	NR	NR	NR		
--	--	- 23	- 211	--	NR	NR	NR		

NOTES:

1. NR=No Record.
2. Forecasts prepared and published by State of California.
3. Forecasts and actual flow from 1953-1960 are from Tule River near Porterville.
4. Computed error based on past performance is not necessarily indicative of the accuracy that may be achieved in the future.

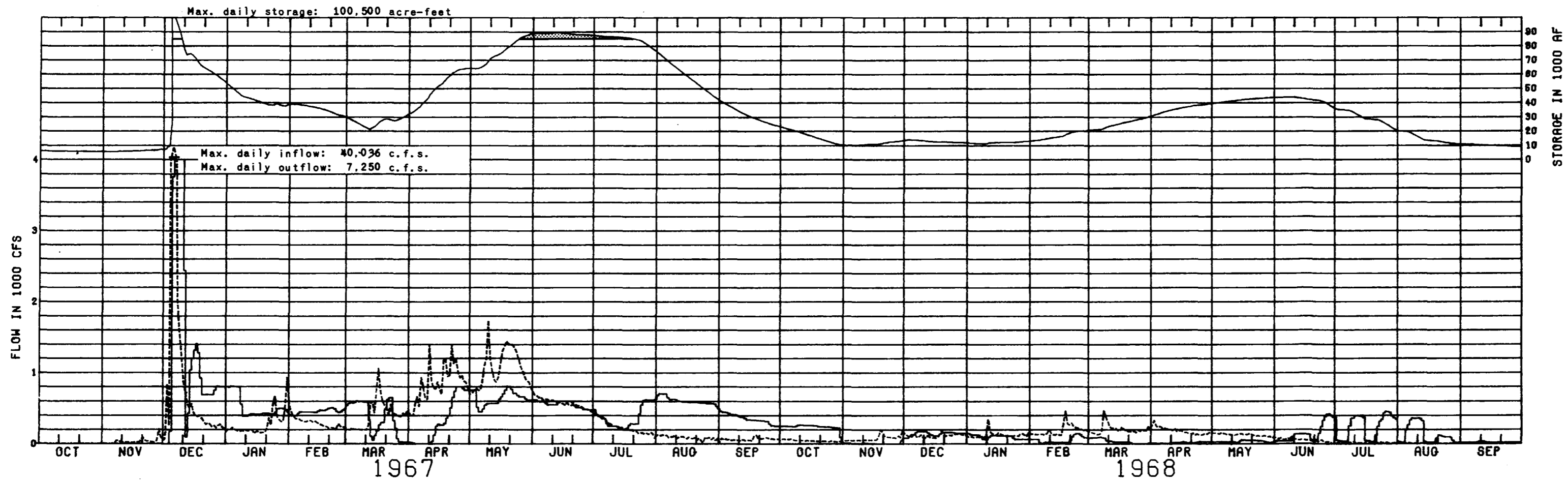
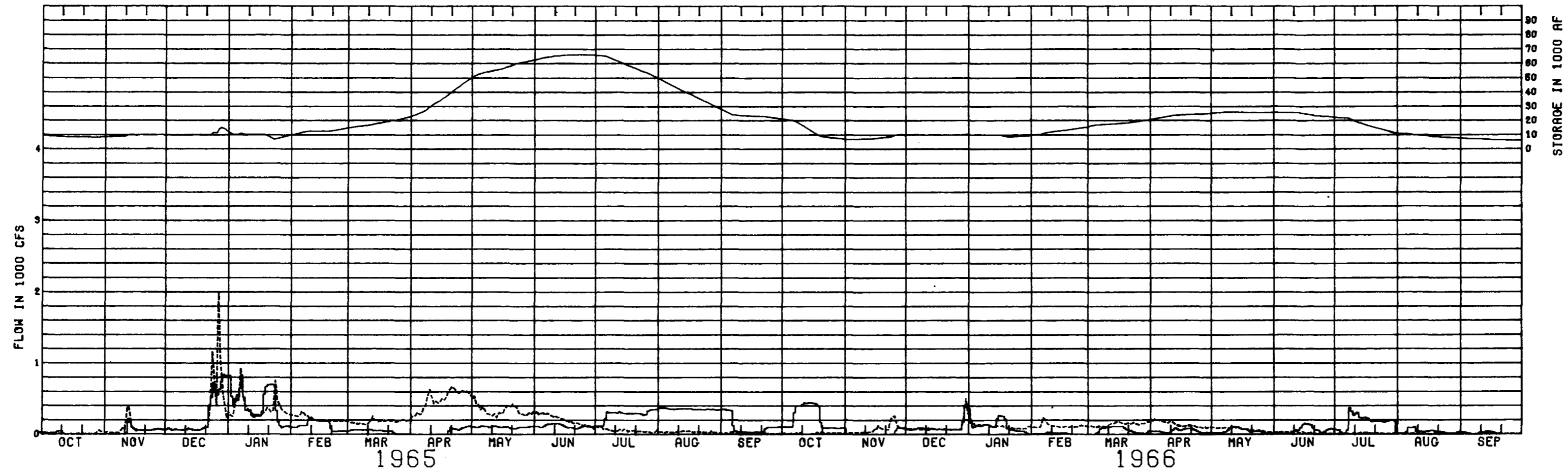


LEGEND:
 — Outflow
 - - - Inflow
 — Storage

SUCCESS LAKE
 TULE RIVER, CALIFORNIA

**HISTORICAL OPERATION
 SUCCESS LAKE**

CORPS OF ENGINEERS, SACRAMENTO, CA.
 PREPARED L.H.C. DATE AUGUST 1980
 DRAWN CAL-COMP



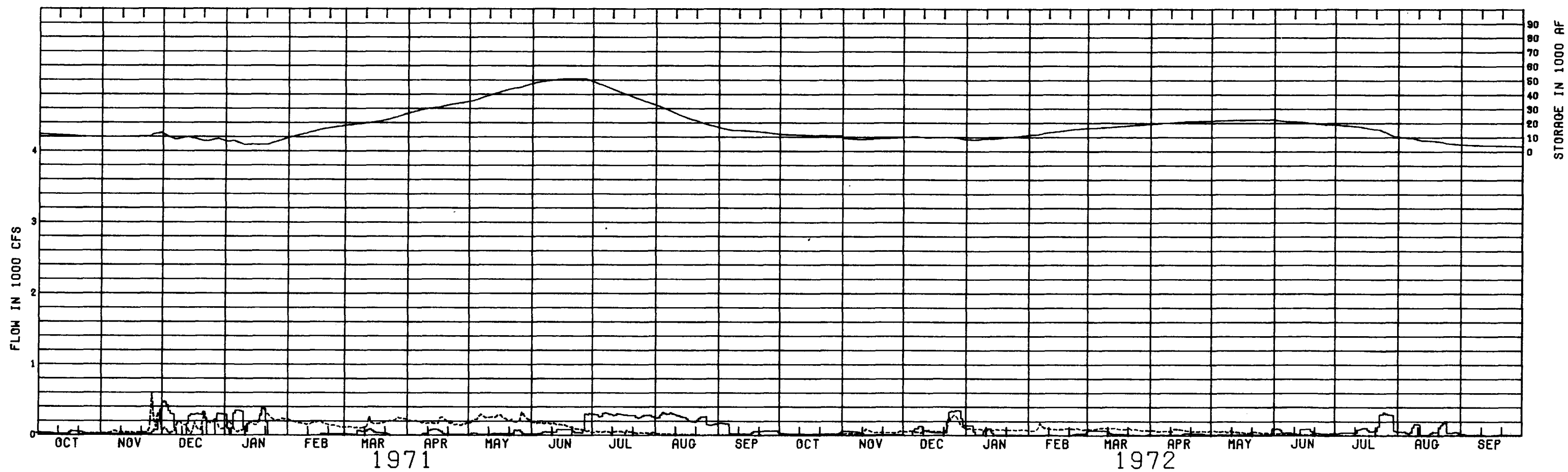
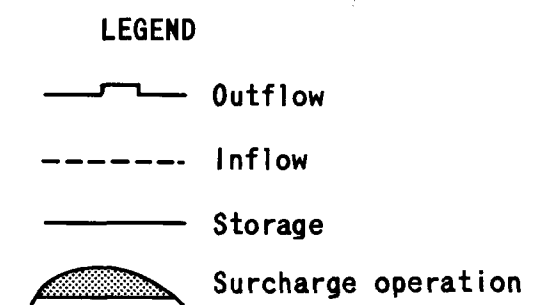
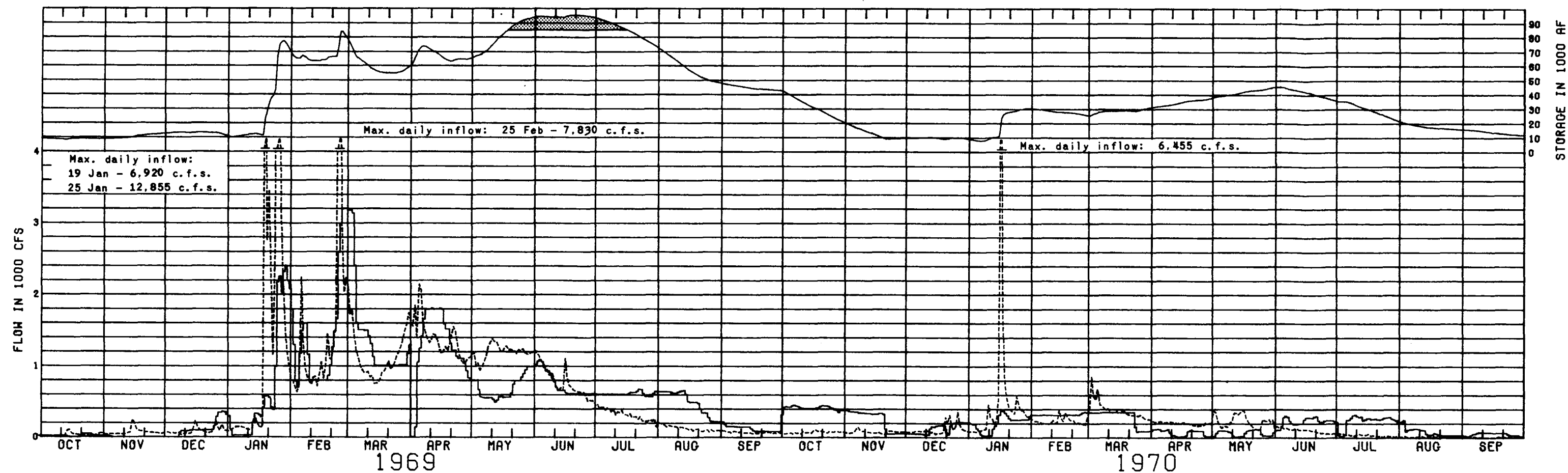
LEGEND

- Outflow
- - - Inflow
- Storage
- ▨ Surcharge operation

SUCCESS LAKE
TULE RIVER, CALIFORNIA

**HISTORICAL OPERATION
SUCCESS LAKE**

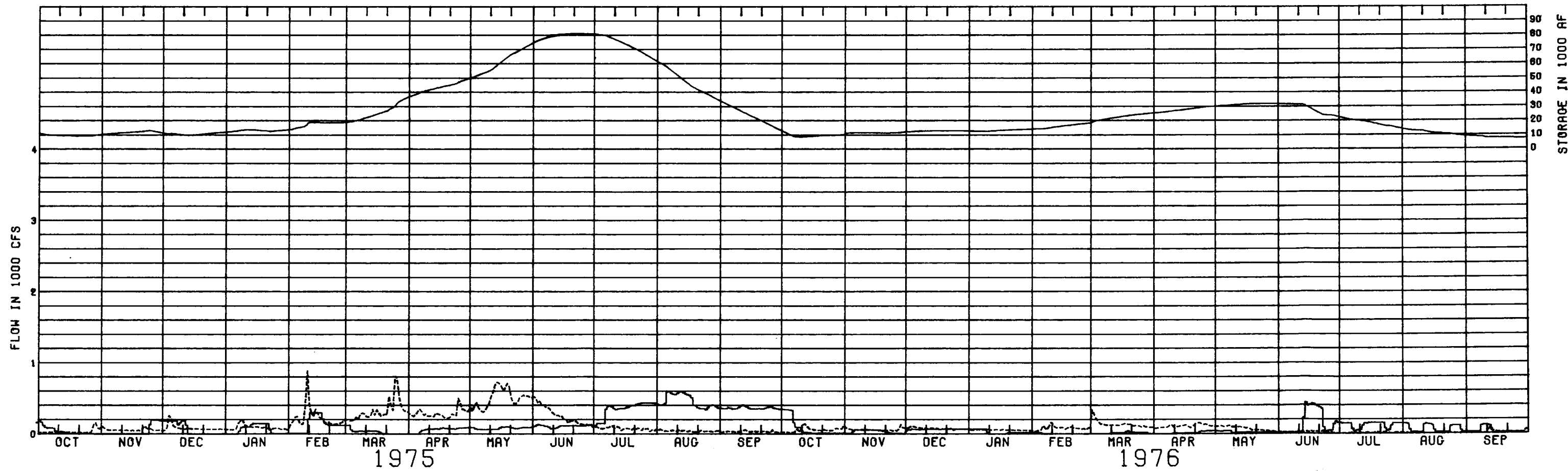
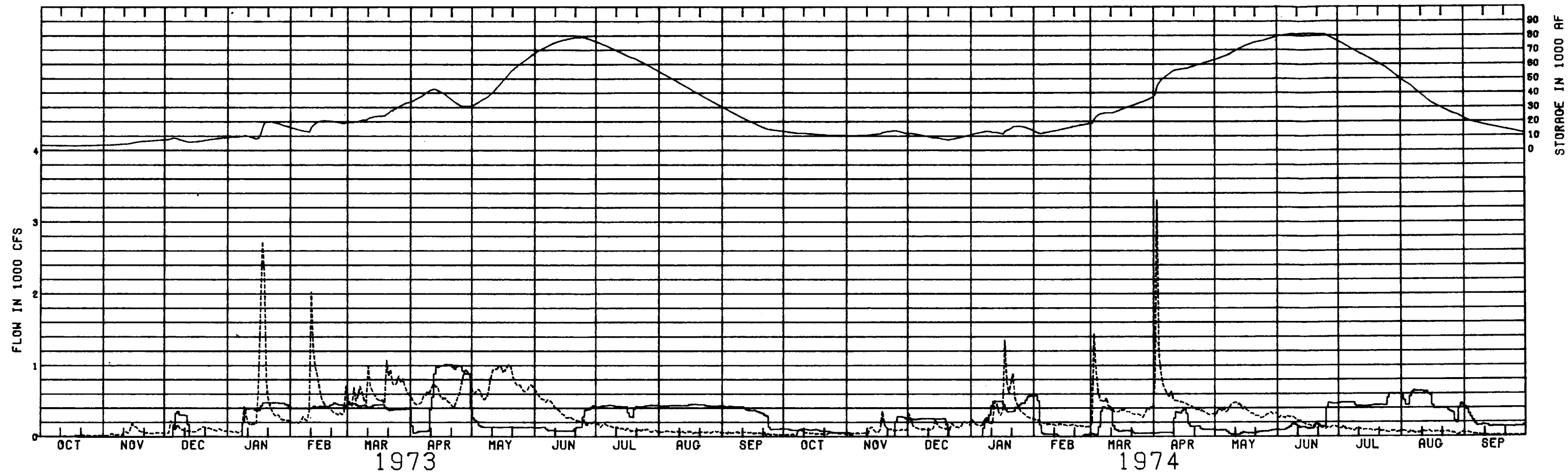
CORPS OF ENGINEERS, SACRAMENTO, CA.
PREPARED L.H.C. DATE AUGUST 1980
DRAWN CAL-COMP



SUCCESS LAKE
TULE RIVER, CALIFORNIA

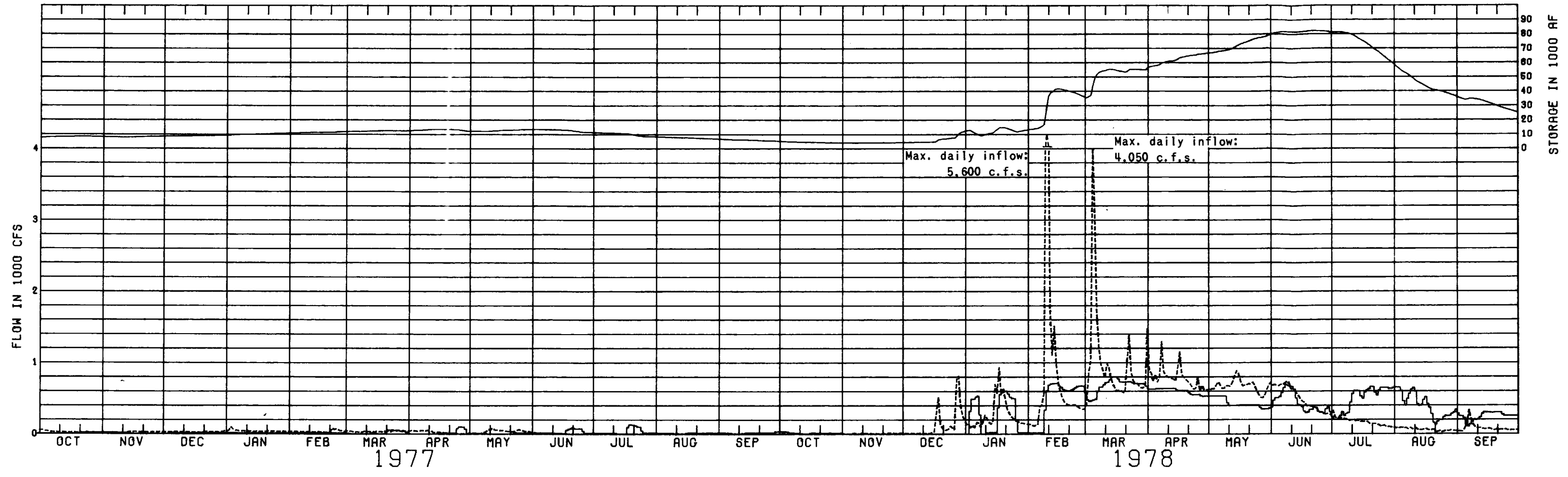
**HISTORICAL OPERATION
SUCCESS LAKE**

CORPS OF ENGINEERS, SACRAMENTO, CA.
PREPARED L.H.C. DATE AUGUST 1980
DRAWN CAL-COMP

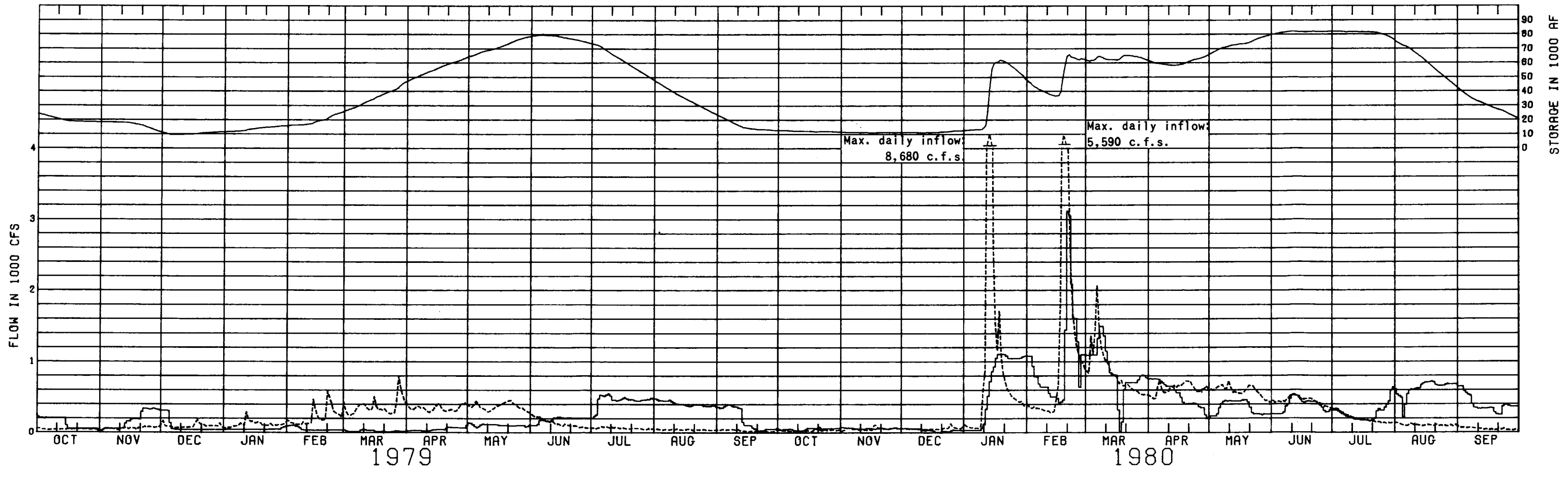


LEGEND
 — Outflow
 - - - Inflow
 — Storage

SUCCESS LAKE
 TULE RIVER, CALIFORNIA
**HISTORICAL OPERATION
 SUCCESS LAKE**
 CORPS OF ENGINEERS, SACRAMENTO, CA.
 PREPARED L.H.C. DATE AUGUST 1980
 DRAWN CAL-COMP



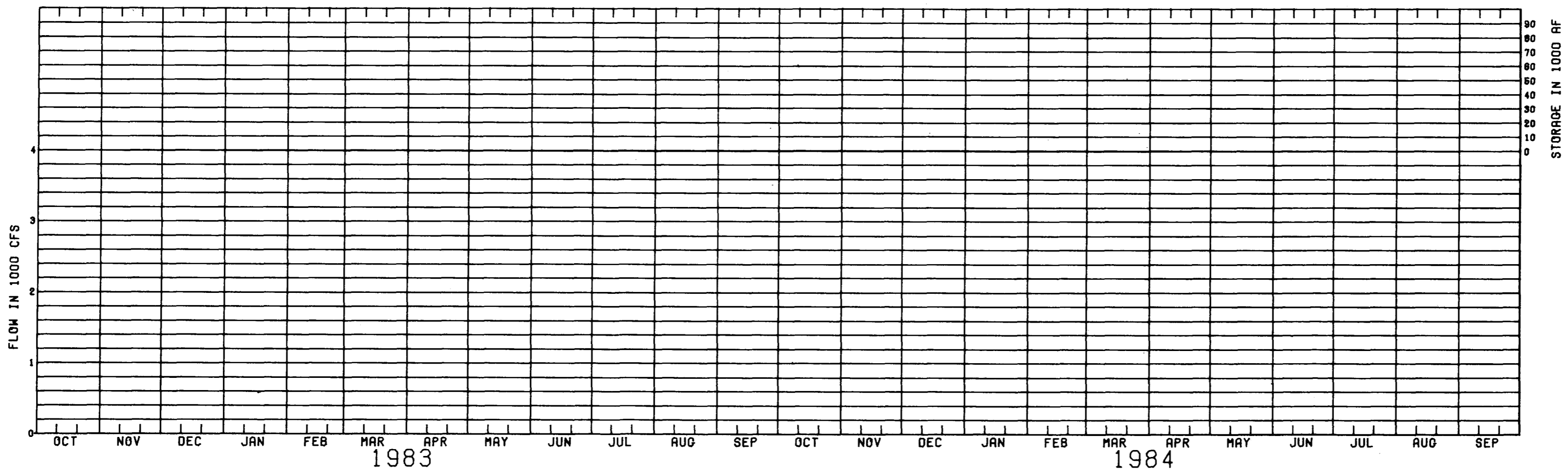
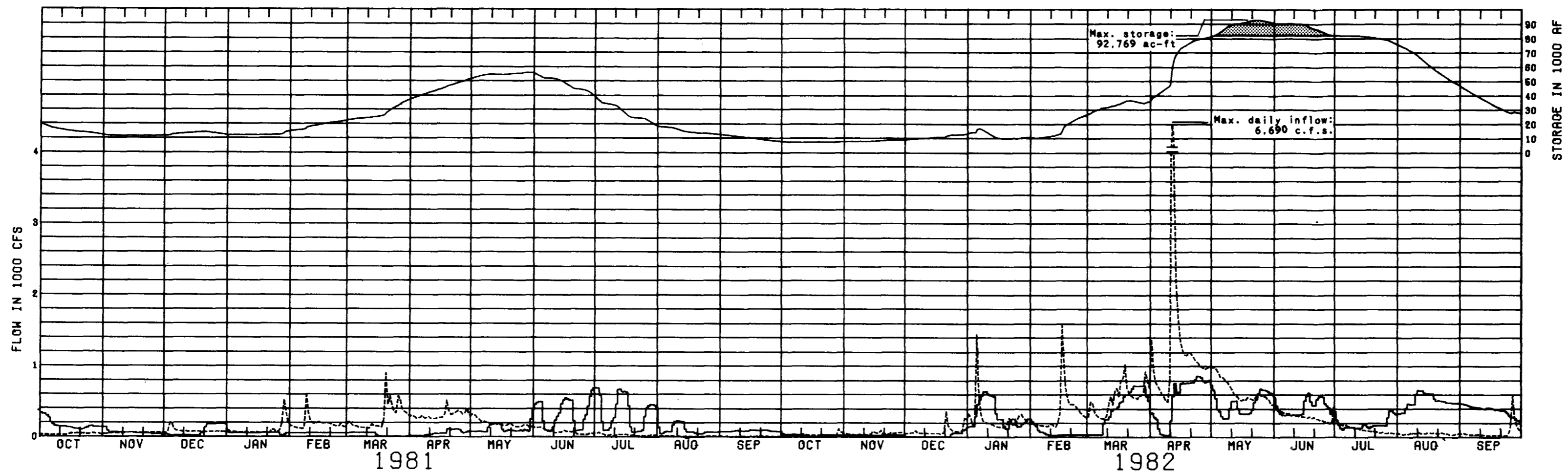
LEGEND:
 — Outflow
 - - - Inflow
 — Storage



SUCCESS LAKE
 TULE RIVER, CALIFORNIA

**HISTORICAL OPERATION
 SUCCESS LAKE**

CORPS OF ENGINEERS, SACRAMENTO, CA.
 PREPARED L.H.C. DATE OCTOBER 1980
 DRAWN CAL-COMP



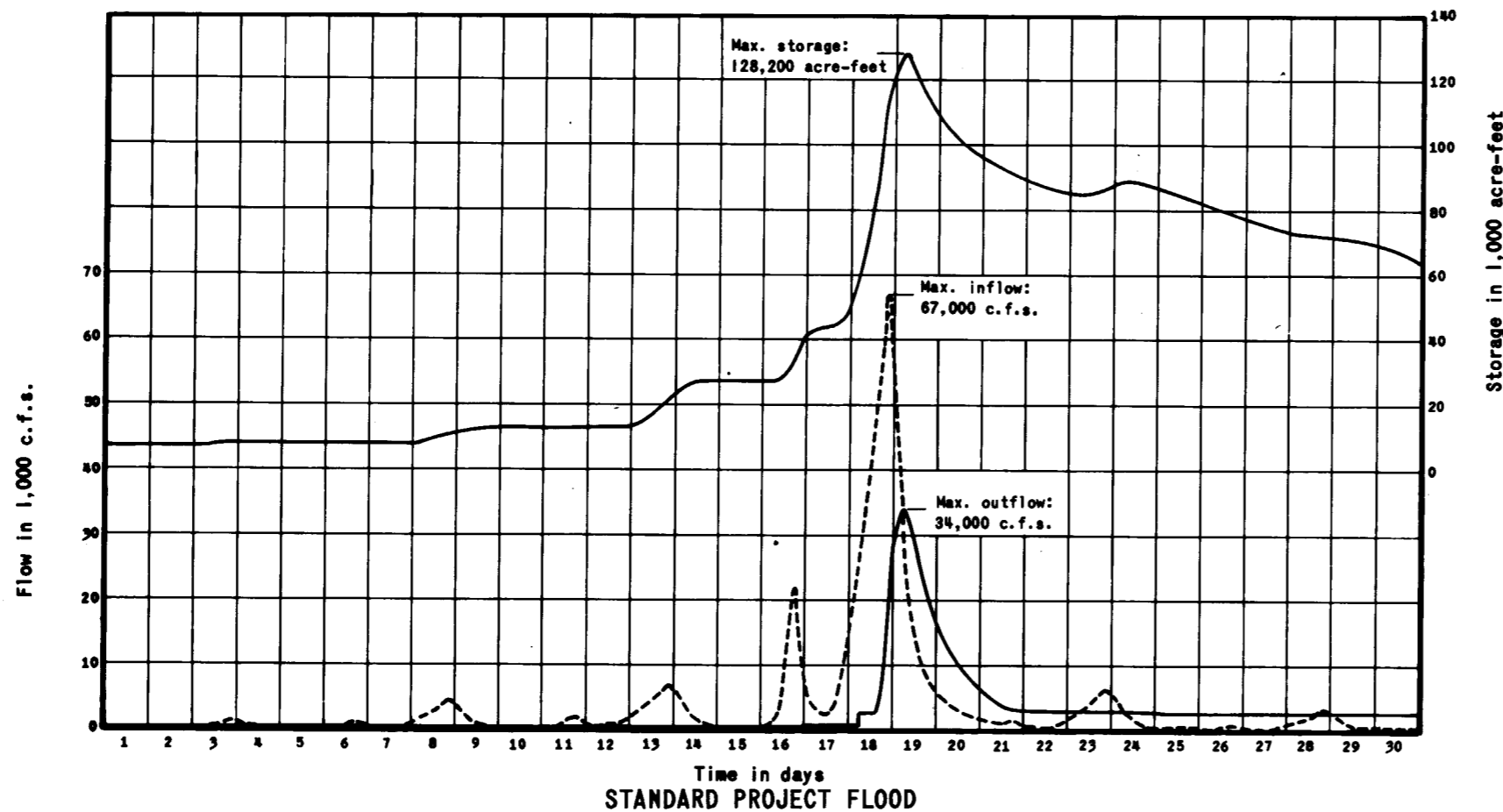
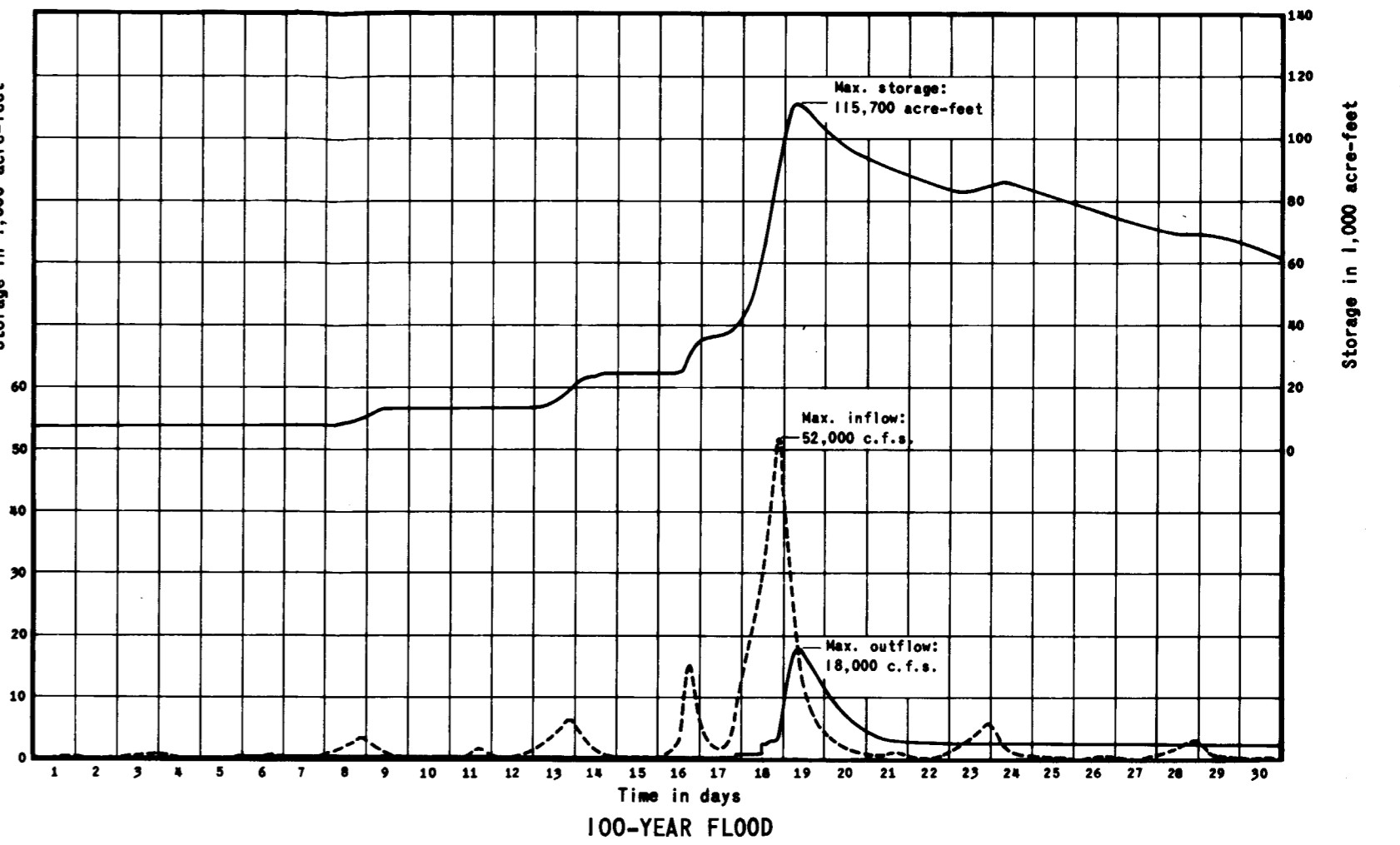
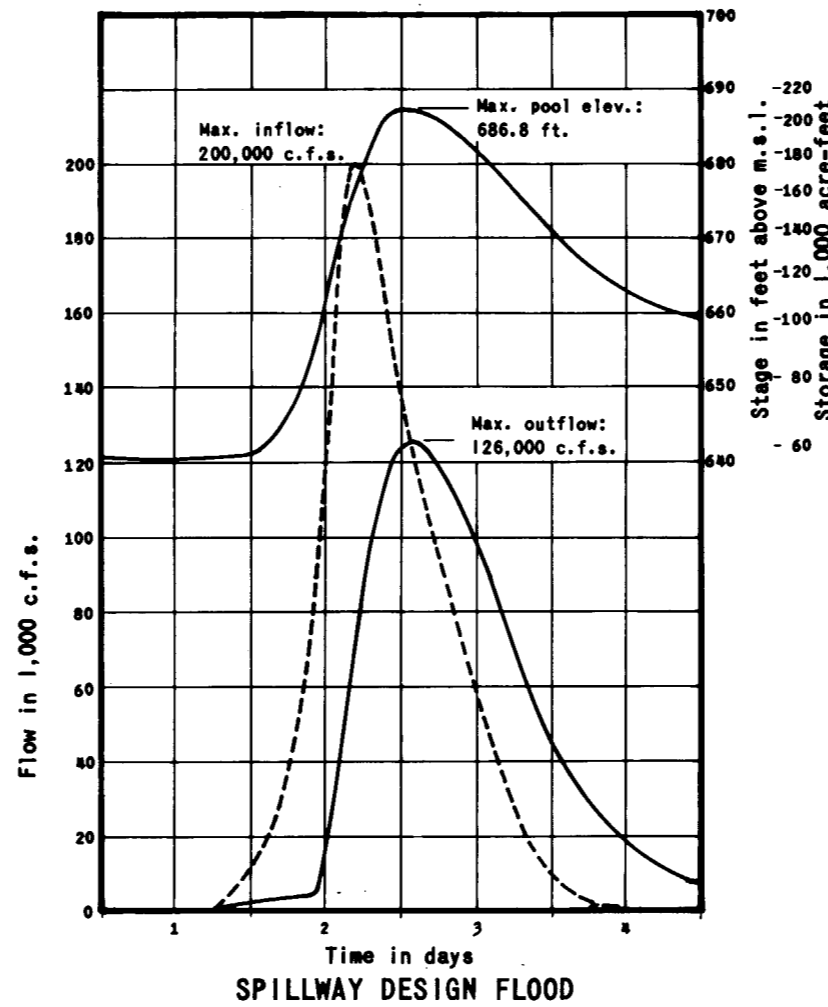
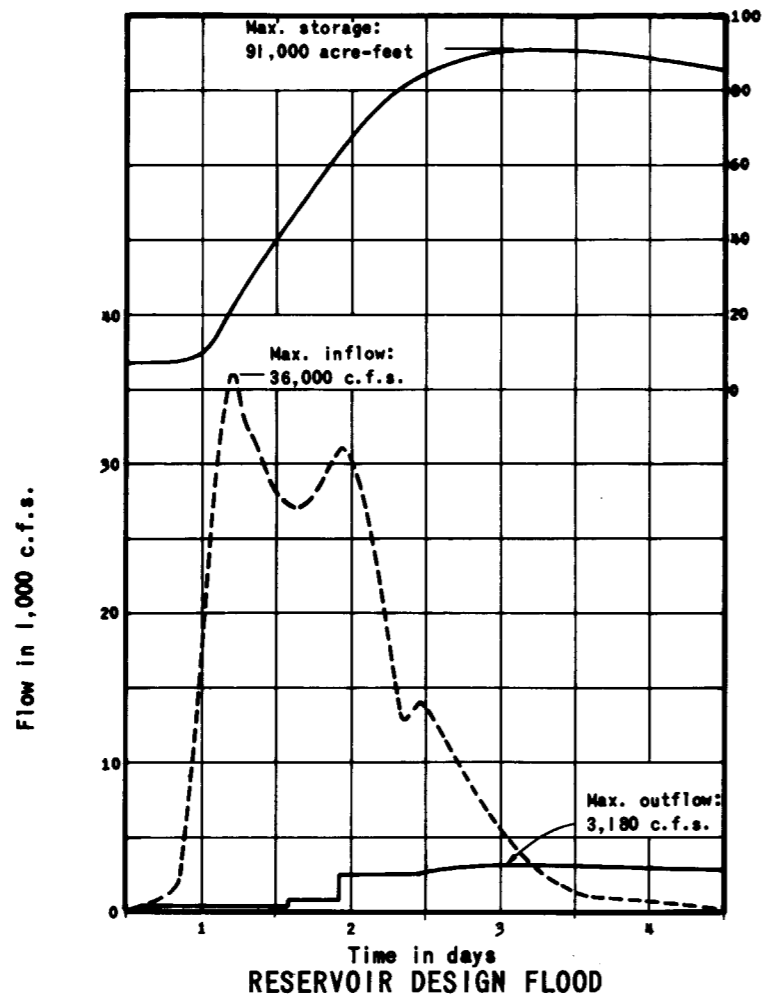
LEGEND:

- Outflow
- - - Inflow
- Storage
- ▨ Surcharge operation

SUCCESS LAKE
TULE RIVER, CALIFORNIA

**HISTORICAL OPERATION
SUCCESS LAKE**

CORPS OF ENGINEERS, SACRAMENTO, CA.
PREPARED: L.H.C. DATE: OCTOBER 1982
DRAWN: CAL-COMP



NOTE:

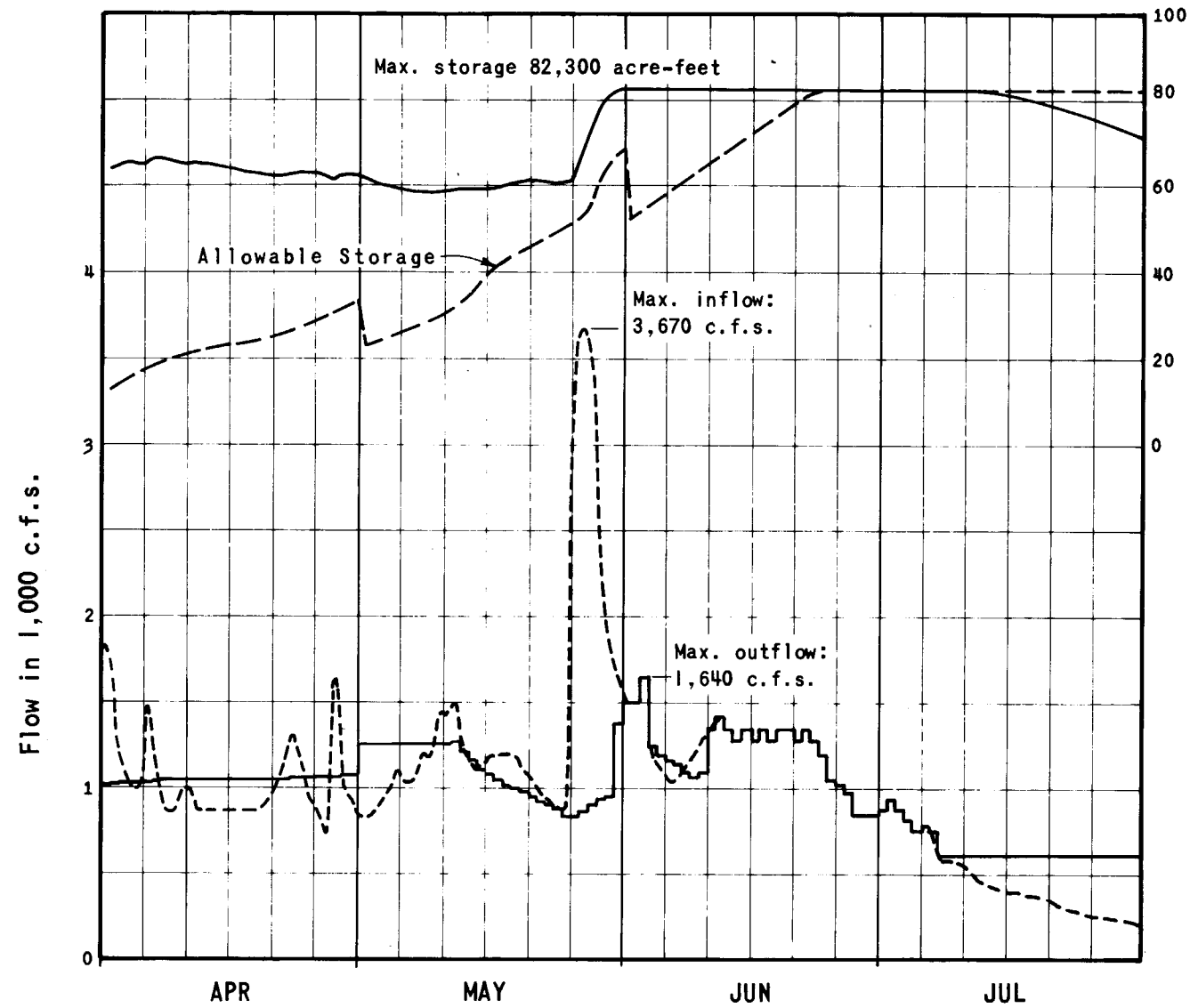
Routings were made allowing for operating contingencies by assuming 80% of the downstream channel capacities would be achieved by project releases.

SUCCESS LAKE
TULE RIVER, CALIFORNIA

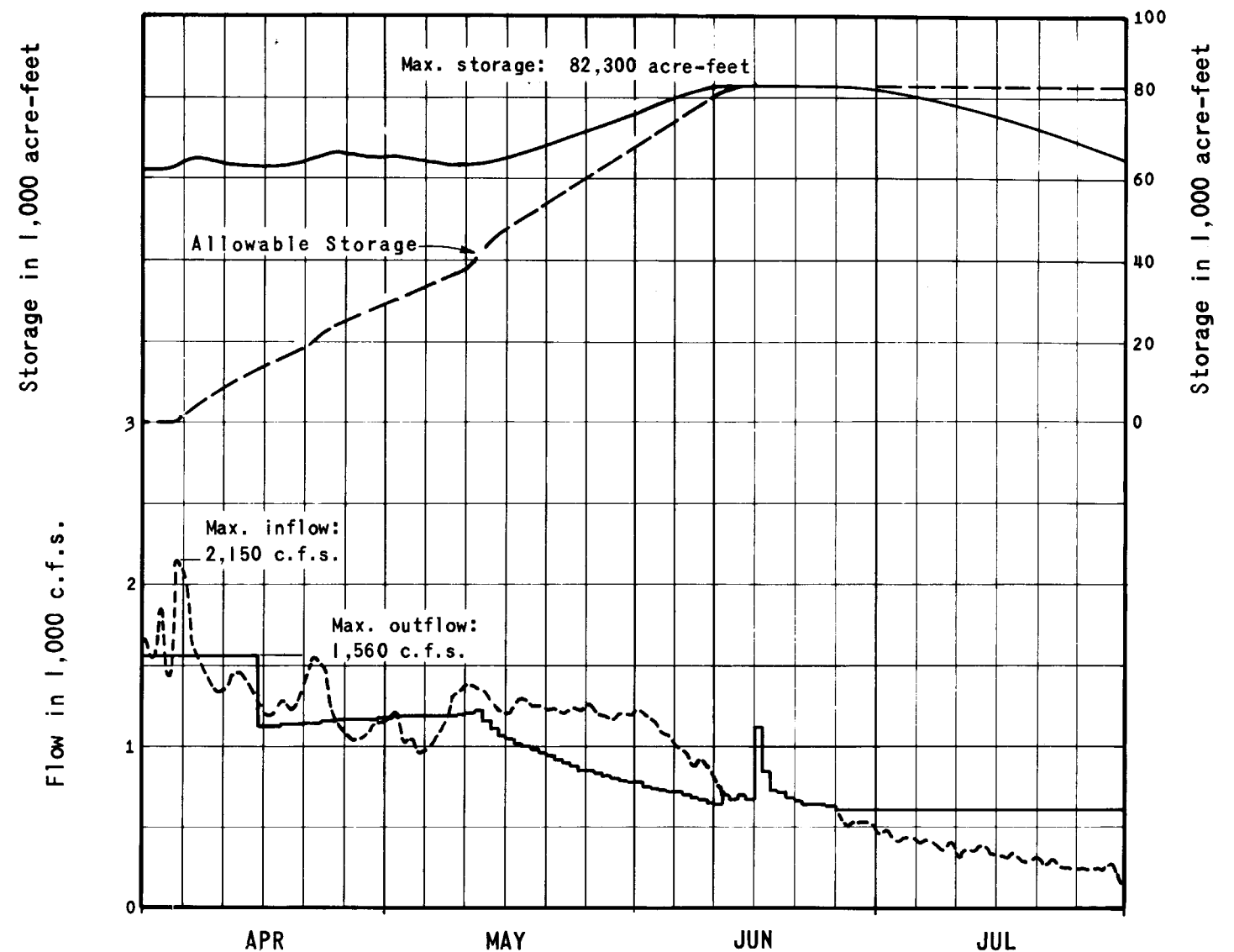
RAIN FLOOD ROUTINGS

CORPS OF ENGINEERS, SACRAMENTO, CA.

Prepared: H.T.M. Date: OCTOBER 1981
Drawn: L.H.C.



1906



1969

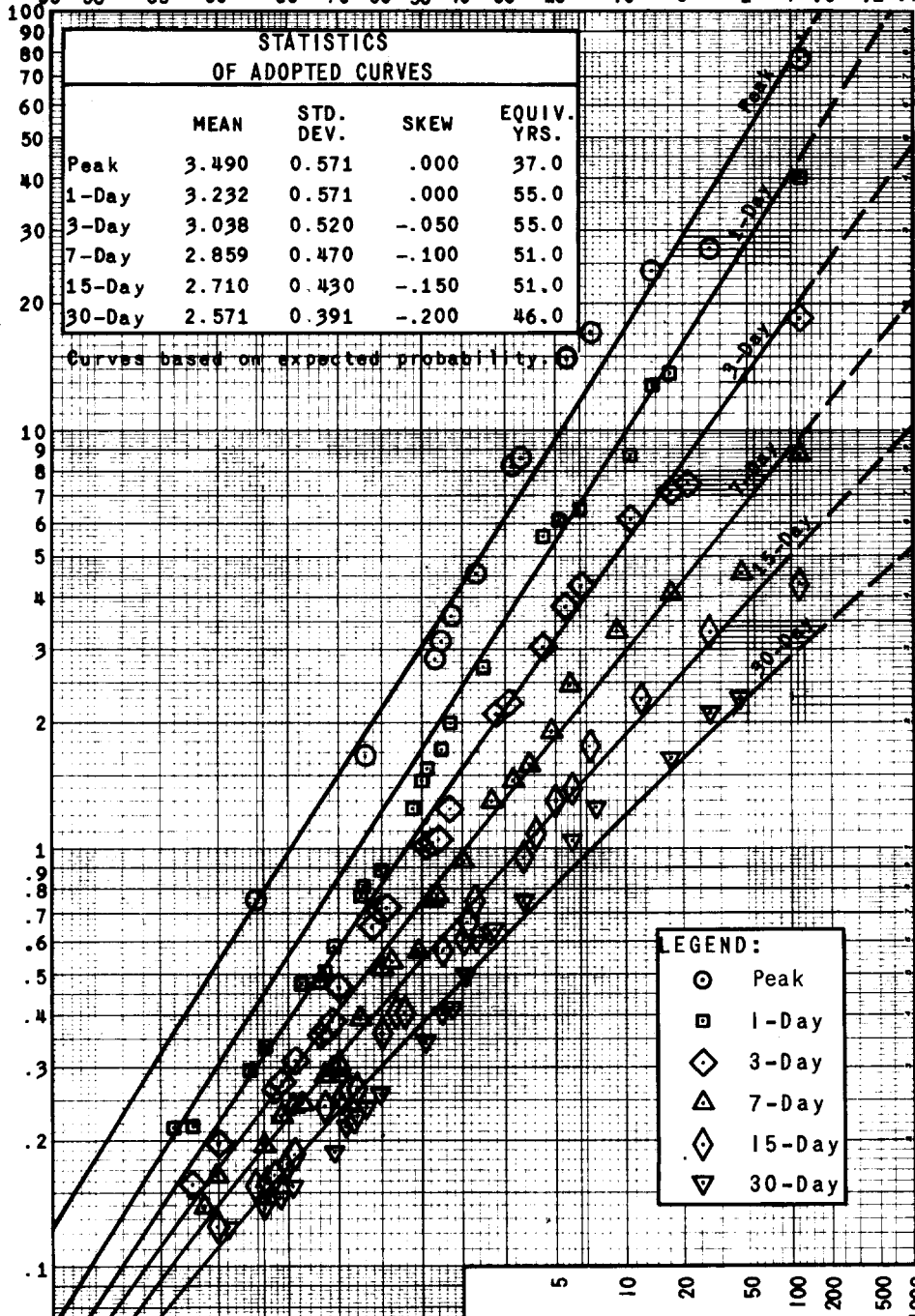
NOTE:

The routings conform to the flood control diagram (Plate A-8). Accurate forecasts were used and were updated monthly.

SUCCESS LAKE TULE RIVER, CALIFORNIA	
HYPOTHETICAL ROUTINGS OF HISTORICAL SNOWMELT FLOODS	
CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA	
Prepared: H.T.M.	Date: NOVEMBER 1981
Drawn: L.H.C.	

Exceedence frequency per hundred years

99 98 95 90 80 70 60 50 40 30 20 10 5 2 1 .5 .2 .1



STATISTICS OF ADOPTED CURVES				
	MEAN	STD. DEV.	SKEW	EQUIV. YRS.
Peak	3.490	0.571	.000	37.0
1-Day	3.232	0.571	.000	55.0
3-Day	3.038	0.520	-.050	55.0
7-Day	2.859	0.470	-.100	51.0
15-Day	2.710	0.430	-.150	51.0
30-Day	2.571	0.391	-.200	46.0

Curves based on expected probability.

LEGEND:	
○	Peak
□	1-Day
◇	3-Day
△	7-Day
◇	15-Day
▽	30-Day

Flow in 1,000 c.f.s.

Exceedence interval in years

Period of Record
1954 - 1980

Drainage Area = 393 sq. mi.

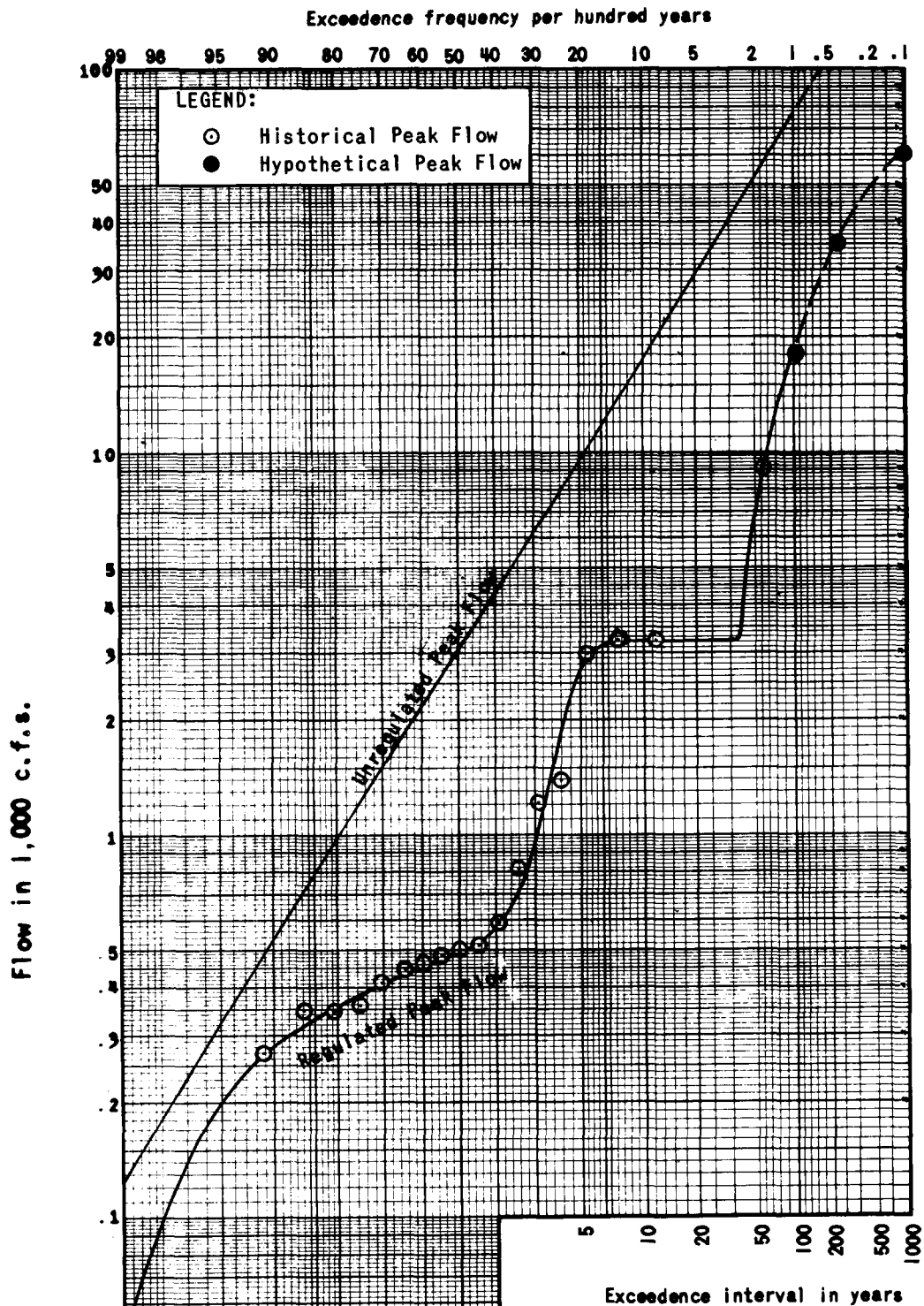
SUCCESS LAKE
TULE RIVER, CALIFORNIA

**RAIN FLOW FREQUENCY
UNREGULATED CONDITIONS**

TULE RIVER BELOW SUCCESS DAM

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

Prepared: H.T.M. Date: SEPTEMBER 1981
 Drawn: L.H.C.



SUCCESS LAKE
TULE RIVER, CALIFORNIA

**RAIN FLOW FREQUENCY
REGULATED CONDITIONS**

TULE RIVER BELOW SUCCESS DAM

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

Prepared: M.E.V., N.T.M. Date: DECEMBER 1981
Drawn: L.N.C.

Exceedence frequency per hundred years

99 98 95 90 80 70 60 50 40 30 20 10 5 2 1 .5 .2 .1

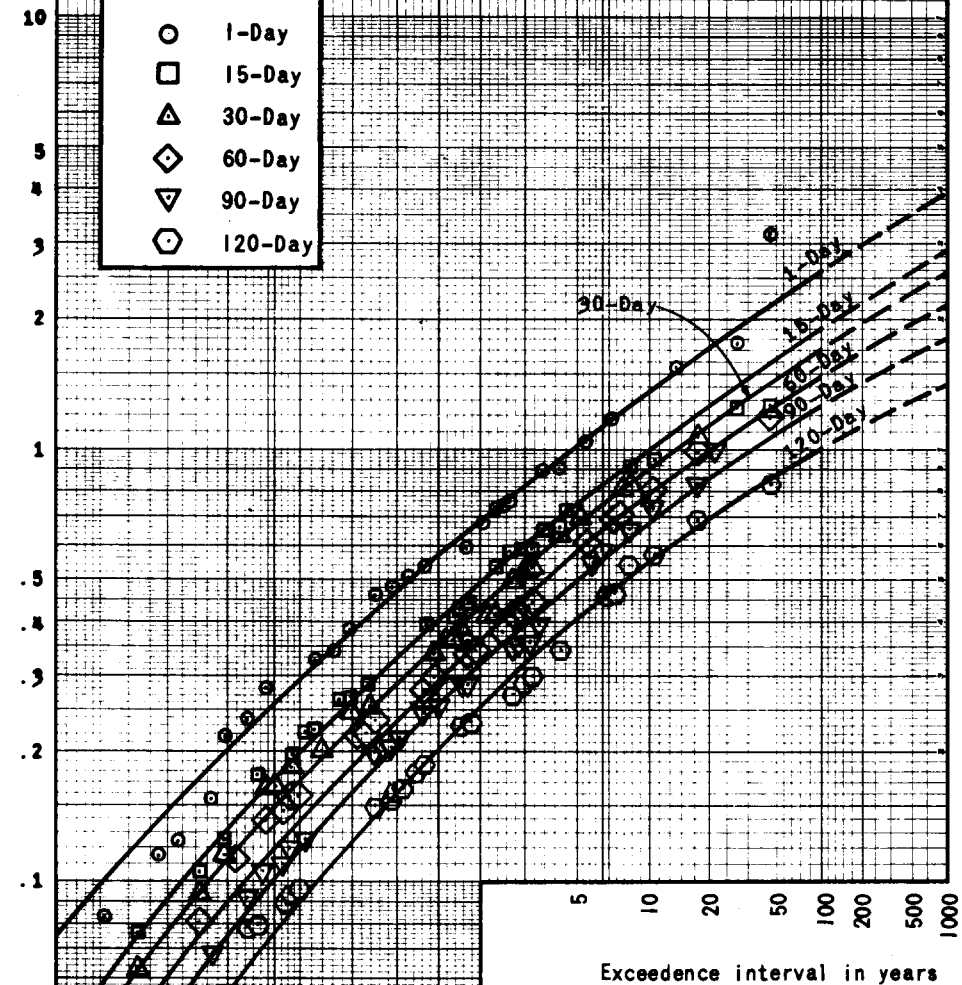
STATISTICS OF ADOPTED CURVES						
	1-DAY	15-DAY	30-DAY	60-DAY	90-DAY	120-DAY
Mean	2.734	2.579	2.530	2.456	2.374	2.267
Std. Dev.	.320	.345	.354	.366	.380	.398
Skew	-.361	-.471	-.507	-.560	-.619	-.695
Eq. Yrs.	78.1	78.3	78.7	78.9	78.9	78.8

Curves based on expected probability.

LEGEND:

- 1-Day
- 15-Day
- △ 30-Day
- ◇ 60-Day
- ▽ 90-Day
- ⊕ 120-Day

Flow in 1,000 c.f.s.



Period of Record
1954 - 1980

Drainage Area = 393 sq. mi.

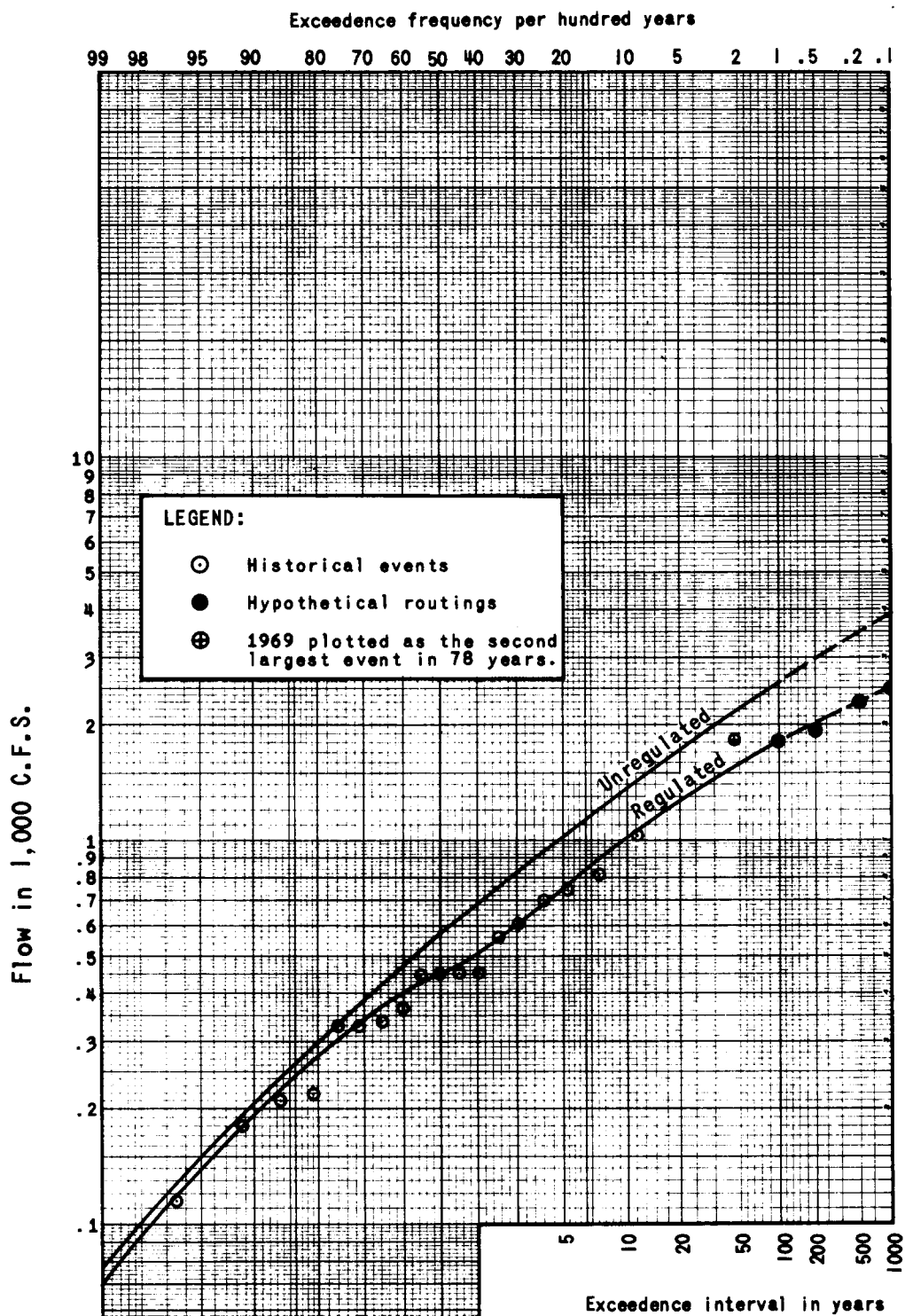
**SUCCESS LAKE
TULE RIVER, CALIFORNIA**

**SNOWMELT FLOW FREQUENCY
UNREGULATED CONDITIONS**

TULE RIVER BELOW SUCCESS DAM

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

Prepared: M.T.M., L.M.C. Date: SEPTEMBER 1981
 Drawn: L.M.C.



Period of Record
1962 - 1980

Drainage Area = 393 sq. mi.

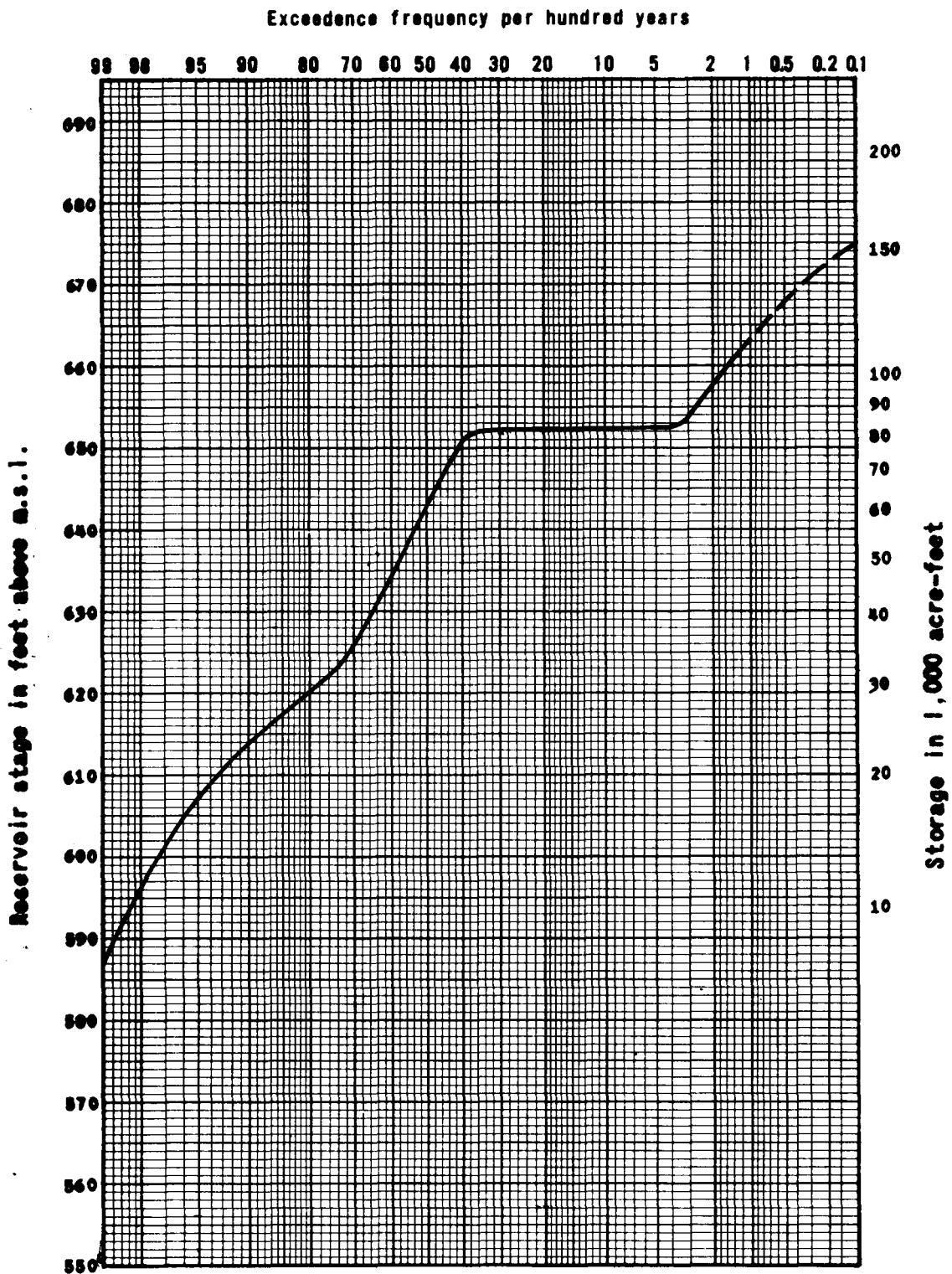
SUCCESS LAKE
TULE RIVER, CALIFORNIA

SNOWMELT FLOW FREQUENCY
REGULATED CONDITIONS

TULE RIVER BELOW SUCCESS DAM

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

Prepared: H.T.M., L.H.C. Date: NOVEMBER 1981
Drawn: L.H.C.

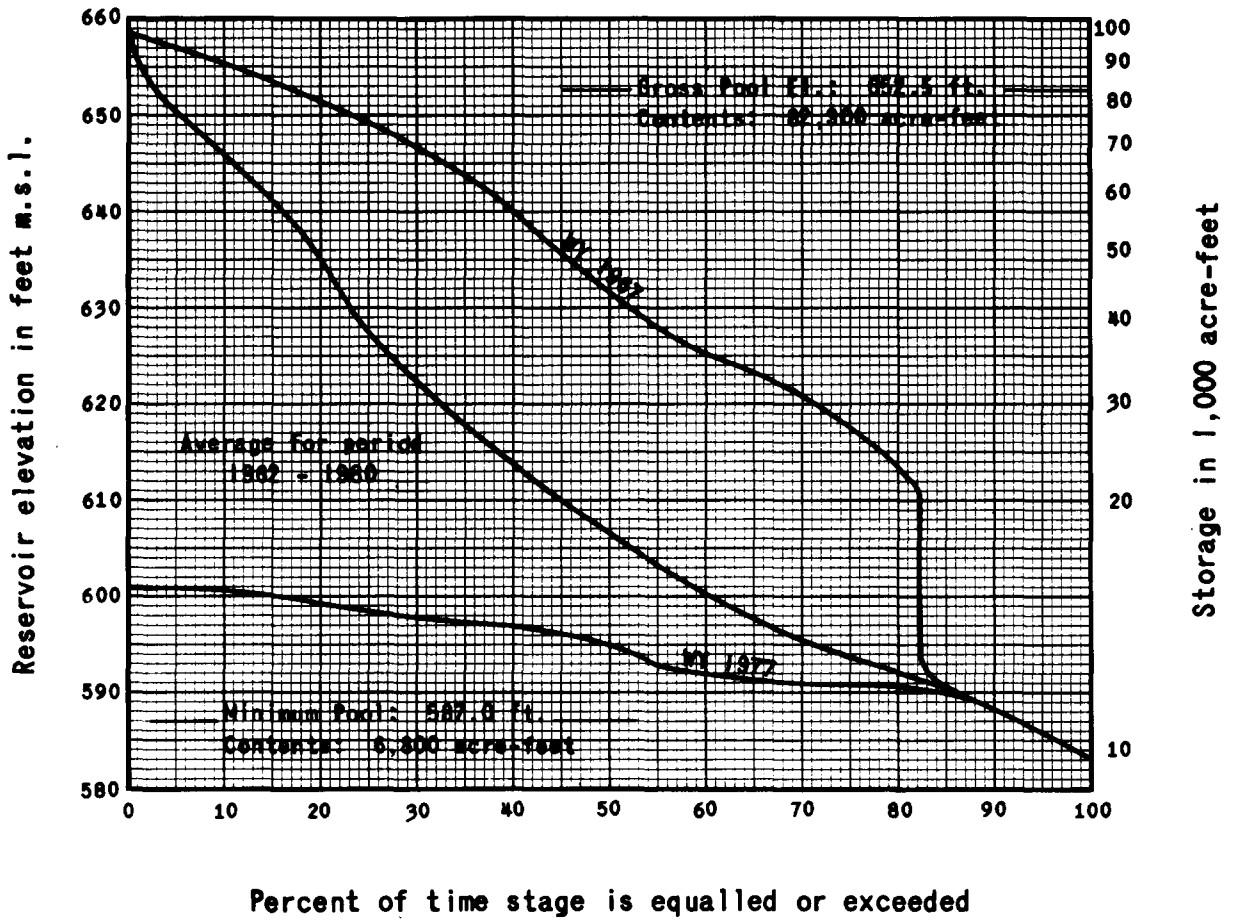


Period of Record
1962 - 1980

SUCCESS LAKE
TULE RIVER, CALIFORNIA

STAGE-FREQUENCY CURVE

CORPS OF ENGINEERS SACRAMENTO, CALIFORNIA
 Prepared: L.H.C., H.T.M. Date: SEP 1981
 Drawn: L.H.C.

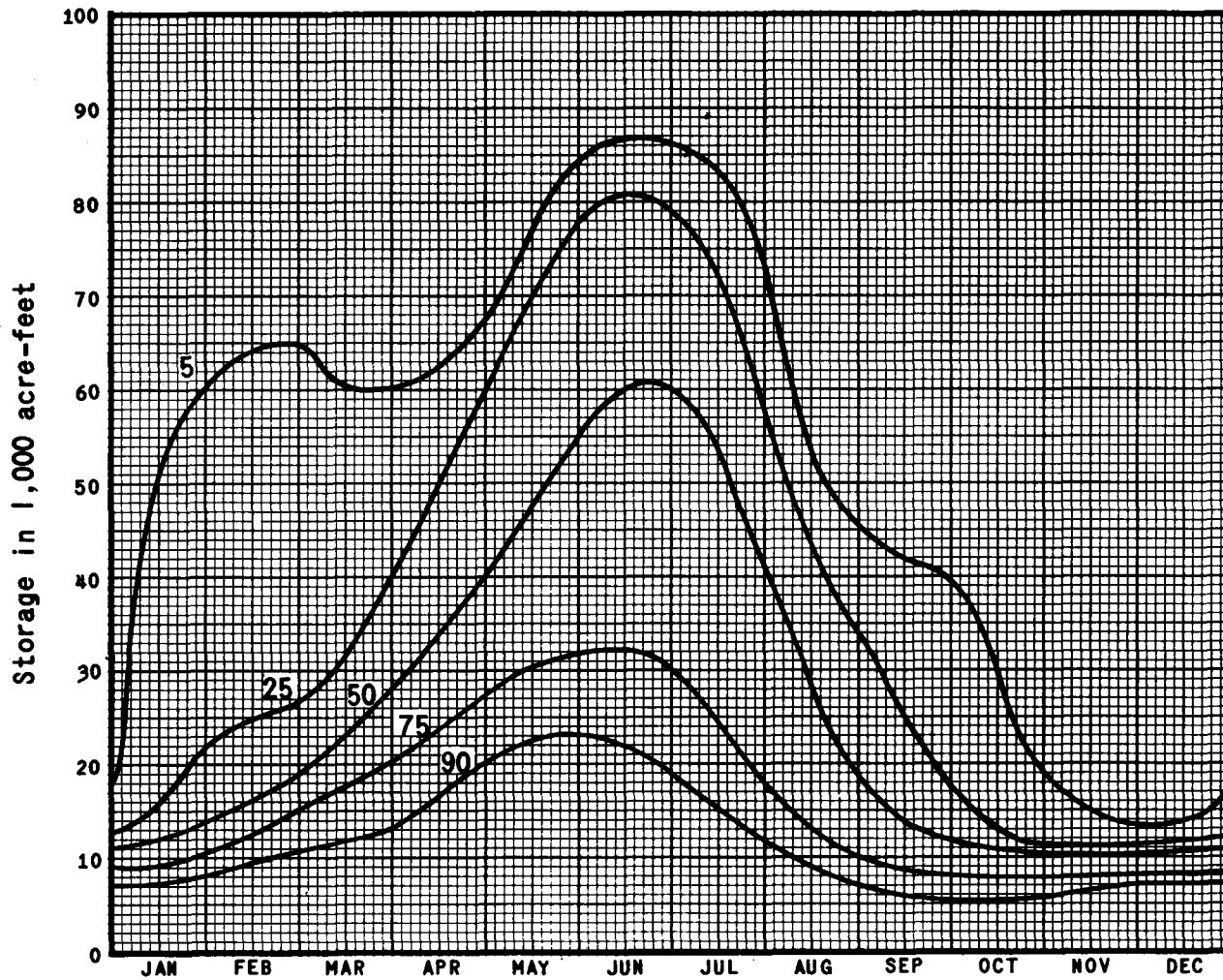


SUCCESS LAKE
TULE RIVER, CALIFORNIA

STAGE-DURATION CURVES

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

Prepared: L.H.C. Date: OCTOBER 1980
Drawn: L.H.C.



NOTE:

Indicated value is percentage of year that the storage is exceeded on a given date based on monthly storage frequency curves for the years 1963-1980. Data was extracted from Corps of Engineers Monthly Report Computations.

SUCCESS LAKE
TULE RIVER, CALIFORNIA

**SEASONAL VARIATION
OF RESERVOIR STORAGE FREQUENCY**

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

Prepared: L.H.C.

Date: DECEMBER 1980

Drawn: L.H.C.

SUCCESS LAKE
TULE RIVER, CALIFORNIA

WATER CONTROL MANUAL

JANUARY 1982

EXHIBIT A
STANDING INSTRUCTIONS TO DAMOPERATOR

Department of the Army
Sacramento District, Corps of Engineers
Sacramento, California

PERSONNEL CONCERNED IN THE OPERATION OF SUCCESS RESERVOIR

	UNIT	OFFICE PHONE	NAME	HOME PHONE
<p>PROJECT OFFICE PORTERVILLE, CALIFORNIA</p>	<p>SUCCESS RESERVOIR</p>	<p>209-784-0215 (Porterville)</p>	<p>B. PROCTER PARK MANAGER</p>	<p>209-784-0575 (Porterville)</p>
<p>DEPARTMENT OF THE ARMY SACRAMENTO DISTRICT CORPS OF ENGINEERS SACRAMENTO, CALIFORNIA</p>	<p>DISTRICT ENGINEER</p> <p>RESERVOIR CONTROL SECTION</p> <p>HYDROLOGIC FACILITIES</p> <p>OPERATIONS BRANCH</p>	<p>916-440-2232x</p> <p>916-440-3405x</p> <p>916-440-3168x 916-440-3167x</p> <p>916-440-2378x</p> <p>916-440-2112x</p> <p>916-440-2327x</p> <p>916-440-2305x</p>	<p>COL. A. E. WILLIAMS DISTRICT ENGINEER</p> <p>R. A. NEAL CHIEF C. D. MATLOCK</p> <p>M. E. VERKE</p> <p>J. T. JOHNSON</p> <p>M. L. HELM CHIEF</p> <p>A. E. SMITH, JR. CHIEF, OPERATIONS & MAINTENANCE SECTION</p>	<p>916-791-0478 (Roseville) 916-487-2985</p> <p>916-967-4994</p> <p>916-687-7212</p> <p>916-961-1918</p> <p>916-652-5280</p>
<p>IRRIGATION INTERESTS</p>	<p>TULE RIVER ASSOCIATION c/o LOWER TULE RIVER IRRIGATION DIST. P.O. BOX 511 WOODVILLE PORTERVILLE, CALIFORNIA</p> <p>TULARE LAKE BASIN WATER STORAGE DIST. 1109 WHITLEY AVE. CORCORAN, CALIFORNIA 93212</p>	<p>209-784-2598 (Porterville)</p> <p>209-686-4716 (Tulare)</p> <p>209-992-4127 (Corcoran)</p>	<p>R. L. SCHAFER WATERMASTER</p> <p>B. GRAHAM MANAGER</p>	<p>209-733-1329 (Visalia)</p> <p>209-582-7603 (Hanford)</p>

FTS: SACRAMENTO 448-2000

NOTE: BETWEEN 4:30 PM AND 7:45 AM, OR ON SATURDAY, SUNDAY OR HOLIDAYS USE 916-452-1535 (FLOOD SEASON ONLY)

SUCCESS RESERVOIR, TULE RIVER, CALIFORNIA

REV. 01-OCT-82

STANDING INSTRUCTIONS TO DAMOPERATOR

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A-2	Area - Capacity Table
A-3	Outlet Rating Curves
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A-8	Flood Control Diagram

EXHIBIT A

STANDING INSTRUCTIONS TO DAMOPERATOR

A-1. General. This exhibit is prepared in accordance with instructions contained in EM 1110-2-3600, paragraph 4-07, (Standing Instructions to Damoperators) and ETL 1110-2-251 and pertains to duties and responsibilities of the damoperators in connection with the operation of Success Lake, and the reporting of required hydrologic data.

Operational instructions to the damoperator, relating to flood control, are outlined with specific emphasis on flood emergencies when communication facilities between him and the Reservoir Control Section have been disrupted. It is designed to be used independently as a flood control guide, or as published, in conjunction with the water control manual. To facilitate independent use of this appendix, plates required for flood control operation (A-1 through A-8) are included herein.

A-2. Operational Responsibilities. The primary responsibilities for operating Success Lake are delegated to units of the Engineering Division and Construction-Operations Division of the Sacramento District, U.S. Army Corps of Engineers, as outlined below. Names and telephone numbers for the individuals whose responsibilities are outlined are given at the front of this exhibit and at the front of the manual.

a. The Hydrology Section (Engineering Division).

- (1) Obtaining current hydrometeorological data and weather forecasts for the region.
- (2) Maintaining hydrologic equipment and supervising its operation.
- (3) Supervising a program of water quality and sediment measurement.

b. The Reservoir Control Section (Engineering Division).

- (1) Analyzing current reservoir and hydrologic data, determining a schedule under which the reservoir shall be operated, and issuing appropriate operating instructions (except for routine day-to-day operations for conservation only) to the reservoir operator.
- (2) Preparing monthly operation and other special reports relative to the operation of the reservoir.
- (3) Advising the District Engineer through the Chief of Engineering Division whenever there has been an unavoidable departure from these operating rules, or when there is a need for making temporary modification of these operating rules.
- (4) Keeping advised at all times of channel and seepage conditions in downstream channels and spreading areas. This will require periodic inspections during years of high runoff.

(5) Maintain a record of nonscheduled operation changes requested by the watermaster and other agencies.

(6) Making necessary revisions to this Water Control Manual and distributing them.

c. The Park Manager (Construction-Operations Division).

(1) Keeping well informed of the operating rules contained in this Water Control Manual and bringing to the attention of the Reservoir Control Section any feature of the manual that may require clarification or revision.

(2) Keeping familiar with the operation of all recording and communication equipment.

(3) Accomplishing the physical operation of the reservoir in accordance with instructions contained in the Water Control Manual or issued by the Reservoir Control Section.

(4) Calculating and maintaining a record of inflows, outflows, storage, weather data, and other data specified by the Reservoir Control Section.

(5) Reporting, by radio or telephone to the Reservoir Control Section, data outlined in this exhibit.

(6) Obtaining necessary information on scheduled downstream irrigation and spreading activities and keeping local interests continuously advised of the routine operation of the reservoir.

(7) Reporting to the Reservoir Control Section any unusual conditions which might interfere with the planned operation of the reservoir.

(8) Maintaining a log of outlet gate operation containing any change in gate position, date, time, and water surface elevation when such changes were made, and initials of the individual accomplishing the change.

(9) Making and recording weekly checks on reservoir and outflow gage readings to assure proper operation of all recording equipment.

(10) Obtaining samples for water quality and sedimentation analysis as required.

(11) Immediately after the end of each month, transmitting to the Reservoir Control Section data specified under reports in paragraph A-6.

(12) Making emergency operation changes when contact with the Reservoir Control Section is broken and a clearly defined change occurs that warrants immediate action.

(13) Maintaining a record of instructions received from the Reservoir Control Section, and requests received from the Tule River Watermaster.

A-3. Computation of Hydrologic Data. During normal operation the following computations are made daily by the indicated personnel.

Reservoir Control Section

Reservoir Operator

Basin Mean Precipitation	Releases from the Reservoir
Basin Wetness Parameter	Inflow to the Reservoir
Evaporation from the Reservoir	Evaporation from the Reservoir
Inflow to the Reservoir	

During emergencies, these computations may be made more frequently as directed by the Reservoir Control Section. The basin mean precipitation, the basin wetness parameter and the reservoir inflow are computed on the HADA computer. Forms are available from the Reservoir Control Section to facilitate manual computations.

a. Mean Daily Releases from the Reservoir.

(1) Check punch tape for errors in gage height and for time. Time is corrected to the current 15 minutes; gage height to the nearest .01 foot.

(2) Tabulate correct gage height readings at odd hours, starting with 0100 hours. Punch tape correction, if any, should be noted.

(3) Enter current rating table, using shifts as applicable, determine and list flow at each odd hour, using the procedure indicated for mean daily flow in (6) below.

(4) Total the 12 flow readings so obtained and divide by 12. This is the mean daily flow.

(5) Mean daily flow will be listed to nearest 0.1 c.f.s. for flows up to 10 c.f.s., and to the nearest 1 c.f.s. for flows above 10 c.f.s. Such values will later be rounded to 3 significant figures by the USGS prior to publication.

(6) When calculating discharge from gage height with a (-) shift correction, enter rating table below the actual height, i.e., if observed gage height is 4.86 and shift is -.02, enter rating table at 4.84 to obtain discharge. For (+) shift, enter rating table above observed gage height.

(7) In order to calculate the gage height for a desired flow under a (-) shift condition, add amount of (-) shift to gage height obtained from table for desired discharge, i.e., if shift is -.03, desired discharge is 5,000 c.f.s., and the rating table shows a gage height of 10.20 = 5,000 c.f.s., the required gage height for 5,000 c.f.s. is $10.20 + .03 = 10.23$. For (+) shift, subtract amount of shift from gage height obtained from table for desired discharge.

b. Evaporation from the Reservoir. Lake evaporation in inches is equal to the pan evaporation in inches multiplied by the evaporation coefficient shown on plate A-6. For this computation, pan evaporation measured at 7:00 a.m. is used to compute lake evaporation for the previous day:

Pan evaporation (inches)

x Gross Evaporation Coefficient

12

x Average Lake Area (acres) = acre-feet

(Round to nearest acre-foot for next
computation)

acre-feet x 0.50417* = s.f.d. = mean c.f.s.
for 24-hours.

*Coefficient shown is for 24-hour day. When changing to daylight savings time or from daylight savings time the coefficients are as follows: for 23-hour day (change to D.S.T.) use 0.52609; for 25-hour day (change from D.S.T.) use 0.48400.

Lake area used when computing evaporation will be the average area for the day; obtained by averaging the midnight areas at the beginning and ending of the period being computed.

c. Inflow to the Reservoir. Computed mean inflow to the lake will be taken as the algebraic sum of the mean outflow, change in lake storage, and evaporation for the lake water surface and will represent mean inflow to the lake from all sources including rainfall on the lake surface.

$$\begin{aligned} &\text{Mean Daily Outflow (c.f.s.)} + \\ &\text{Change in Lake Storage (s.f.d.)} + \\ &\text{Evaporation (s.f.d.)} = \\ &\text{Mean Inflow (c.f.s.)} \end{aligned}$$

d. Basin Mean Precipitation. The approximate basin mean precipitation (BMP) is computed by multiplying the sum of the precipitation at representative rain gages by the conversion factor for the basin and gages. The conversion factor is computed by dividing the basin normal annual precipitation (BNAP) by the sum of the station normal annual precipitation (SNAP)). The computation of the conversion factor (C) for the Tule River Basin and the rain gages normally observed is shown below:

<u>Gage</u>	<u>SNAP</u>
Hossack	42"
Eagle Creek	36"
Rogers Camp	36"
Mountain Home	38"
Success Dam	11"
Sum SNAP	163"

BNAP = 31"

Basin Conversion Factor (C) = 31"/163" = 0.19

e. Basin Wetness Parameter. The basin wetness parameter (PAR) for a given day is the basin mean precipitation (BMP) for that day plus 97 percent

of the previous day's wetness parameter (PAR') and is represented by the equation $PAR = BMP + .97 PAR'$. A sample computation of PAR is shown in paragraph A-3f.

f. Encroachment. As part of Success Lake's drought contingency plan, Schedule 1 releases may be deferred temporarily during the period 10 November to 1 April to allow storage of 3,200 acre-feet in Schedule 1 space above elevation 588.9 feet subject to the following: The amount of encroachment (E) above elevation 588.9 feet will be dependent on the basin wetness parameter (PAR) and will vary proportionately from 3,200 acre-feet when PAR is 2 inches or less to 0 acre-feet when the PAR is 6 inches or more. Values of E and PAR are shown in tabular form below along with an example computation.

EXAMPLE

Given:

Station precipitation for 14 January

Success Dam	1.69 in.
Mountain Home	5.00 in.
Rogers Camp	4.40 in.
Eagle Creek	8.80 in.
Hossack	6.40 in.

Data for BMP, PAR and E for the period 8 Jan through 13 Jan.

<u>Date</u>	<u>BMP</u> (in.)	<u>.97 PAR'</u> (in.)	<u>PAR</u> (in.)	<u>E</u> (ac-ft)
8 Jan	0.20	1.56	1.76	3,200
9 Jan	2.00	1.71	3.71	1,832
10 Jan	2.22	3.60	5.82	144
11 Jan	0.50	5.65	6.15	0
12 Jan	1.00	5.97	6.97	0
13 Jan	8.24	6.76	15.00	0
14 Jan	(5.00)	(14.55)	(19.55)	(0)

Basin conversion factor (C) = $BNAP/SNAP = 31''/163'' = 0.19$

Find:

BMP, PAR and E for 14 January.

$BMP = C (13.29) = 0.19 (13.29) = 5.00 \text{ in.}$

$PAR = BMP + .97 (PAR') = 5.00 + .97 (15.00) = 19.55 \text{ in.}$

(PAR' = previous day's PAR)

$E = [6 - PAR]/4 \text{ } 3,200 \text{ acre-feet} = 0 \text{ acre-feet}$

(E = 0 acre-feet when PAR = 6 in.)

A-4. Outlet Gate Operation. Desired releases through each outlet will be obtained by manipulating the gates until the appropriate stages are obtained as indicated by the current rating curve for Pioneer Ditch (plate A-5) and the current rating curve for the Tule River (plate A-5). The partial gate opening curves on plate A-3 will be used as a guide in estimating gate openings for river outlet releases. Releases to Pioneer Ditch will be regulated by the 42" double disc type gate valve. Other irrigation releases and flood releases below the spillway level will be regulated by the two 5'8" x 10'0" hydraulically operated slide gates. There are no hydraulic limitations on the sequence or arrangement of openings for these two slide gates. However, for larger releases, it is desirable to maintain approximately equal gate openings at the two gates whenever feasible in order to obtain smooth flow through the conduit. Operation of outlets when spillway flows are occurring is described in paragraph A-8.

A-5. Normal Flood Control Operation. Plate A-8 depicts flood control space and flood control release requirements.

a. All inflow in excess of the releases requested by the Tule River irrigation interests will be stored to the extent that conservation space is available.

b. Release of water stored for irrigation will be in accordance with the requests of the Tule River Watermaster, conforming with mutual agreements and stipulations of the water users, unless prior release is required for flood control.

A-6. Reports. The damoperator shall report the following data by radio or telephone to the Reservoir Control Section each work day between 7:30 a.m. and 9:00 a.m.:

a. Reservoir stage as of midnight.

b. Pan evaporation as of 7:00 a.m.

c. Mean daily flows (ending at midnight) of:

(1) Tule River below Success Dam.

(2) Pioneer Ditch below Success Dam

d. Daily precipitation at the dam as measured at 7:00 a.m.

e. Climatological gage readings for precipitation at Eagle Creek, Rogers Camp, Hossack and Mountain Home.

When conditions do not warrant weekend or holiday reports, complete reports for each day shall be made on the first day following the non-reporting period. More frequent reports of the above information and reports of other Tule River data will be made in the same manner when requested by the Reservoir Control Section. Forms furnished to the operators are to be used in computing the above information.

Immediately after the end of each month, the reservoir operator will dispatch to the Reservoir Control Section all original forms used for observations and computations as specified above. The charts and punch tapes for that month from the following instruments will be included.

- a. Recording precipitation gage of Success Lake.
- b. Recording Hygrothermograph at Success Lake.
- c. Reservoir level recorder punch tape.
- d. Stream gages below dam on the Tule River and on Pioneer Ditch.

A-7. Special Weather and Flood Reports. During the rain flood season from 1 October to 1 May the damoperator shall call the Reservoir Control Section whenever any of the following occurs:

- a. One inch or more of rainfall at the project or at any of the radio-reporting precipitation stations during any 6-hour period or 1.5 inches or more of rainfall during any 24-hour period.
- b. An increase in flow at the main Tule River inflow station of 1,000 c.f.s. or more during any 6-hour period.

Any special report based on one of the foregoing criteria should include the latest available data concerning the other item. On nonworking days or at night, these special reports should be telephoned directly to the Chief of the Reservoir Control Section or his designated representative.

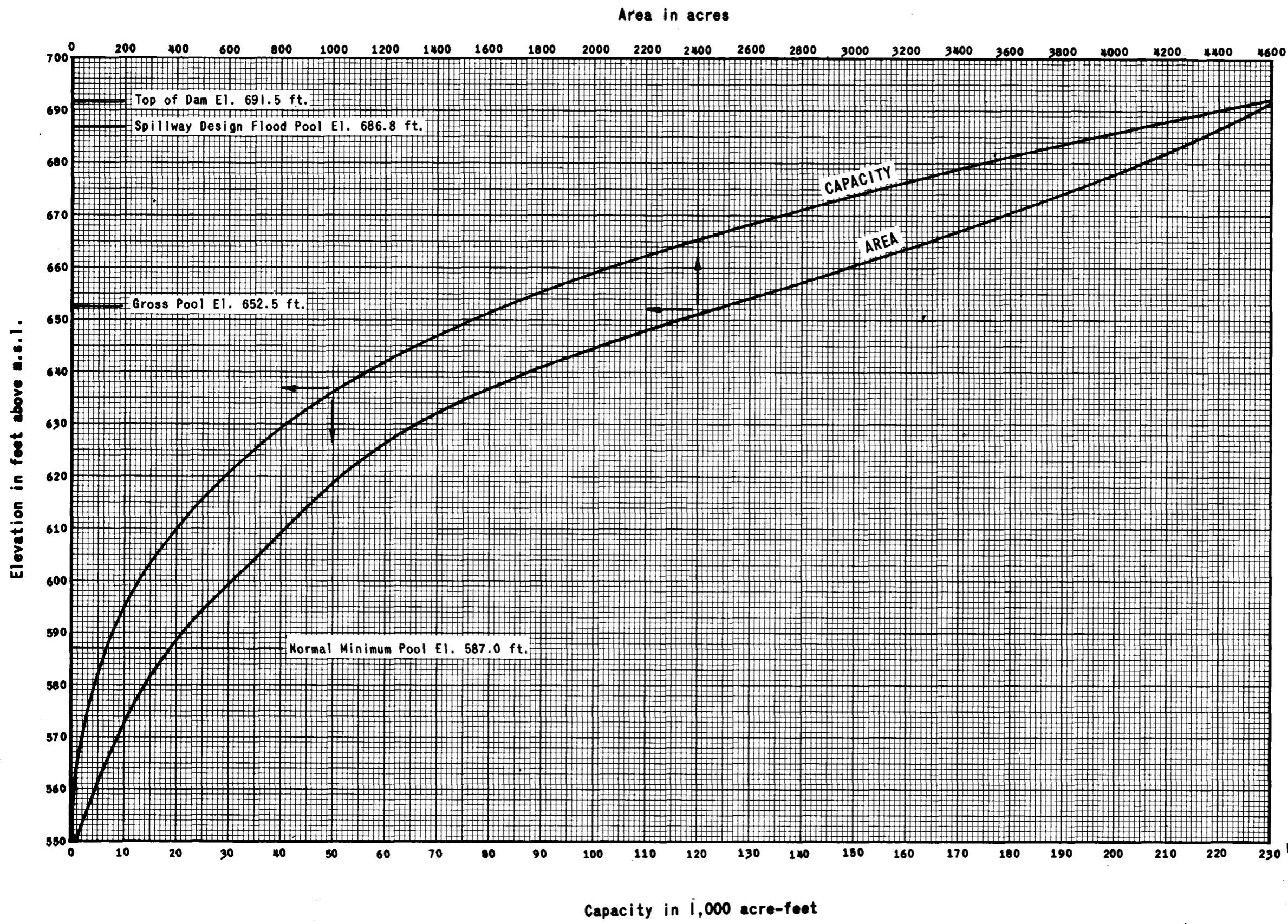
A-8. Standing Instructions During Flood Emergency. Flood control operation shall be in accordance with instructions from the Reservoir Control Section. During flood periods, close contact will be maintained between project and District personnel on a 24-day per day basis or as otherwise required.

If communication is broken between the operating personnel and the Sacramento District Office during a flood emergency, continue releases in accordance with the last instructions received from the Sacramento District unless a clearly defined change occurs that warrants immediate action. Every attempt should be made to reestablish communications.

The maximum design release of 3,200 c.f.s. will not be intentionally exceeded. If flow over the spillway occurs, gate releases will be curtailed so as to maintain a flow of 3,200 c.f.s. or less for as long as possible.

A-9. Emergency Notification. For serious emergencies when large spillway releases or dam failure are eminent, an emergency notification plan is maintained at the Success Lake Project Office. The park manager is responsible for implementing the emergency notification plan; however, such notification should be coordinated with the Reservoir Control Section, if possible.

A-10. Modification of Regulations. The reservoir operator may make emergency departures from the regulations in this manual as required by operating equipment failures, accidents such as drownings or other emergencies that require immediate action. The Reservoir Control Section of the Army Corps of Engineers, Sacramento District should be notified of such departures as soon as possible. The District Engineer, Sacramento District, U.S. Army Corps of Engineers may make temporary modifications to these regulations. Permanent changes are subject to approval by the Division Engineer, South Pacific Division, U.S. Army Corps of Engineers.



Note:
From Area-Capacity tables dated September 1978

SUCCESS LAKE
TULE RIVER, CALIFORNIA

AREA-CAPACITY CURVES

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

Prepared: L.H.C. Date: OCTOBER 1980
Drawn: L.H.C.

SUCCESS RESERVOIR, TULE RIVER, CALIFORNIA - AREA AND CAPACITY TABLE (SEPT 78)

ELEV FEET	CAP AREA .0	CAP AREA .1	CAP AREA .2	CAP AREA .3	CAP AREA .4	CAP AREA .5	CAP AREA .6	CAP AREA .7	CAP AREA .8	CAP AREA .9

550.0	98 24	100 25	103 25	105 26	108 26	111 27	113 27	116 28	119 28	122 29
551.0	125 29	128 30	131 30	134 31	137 31	140 32	143 32	146 33	150 33	153 34
552.0	156 34	160 35	163 36	167 36	171 37	174 37	178 38	182 38	186 39	190 40
553.0	194 40	198 41	202 41	206 42	210 43	215 43	219 44	223 45	228 45	232 46
554.0	237 47	242 47	246 48	251 48	256 49	261 50	266 50	271 51	276 52	282 52

555.0	287 53	292 54	298 55	303 55	309 56	314 57	320 57	326 58	332 59	337 59
556.0	343 60	349 61	356 62	362 62	368 63	374 64	381 64	387 65	394 66	400 67
557.0	407 67	414 68	421 69	428 70	435 70	442 71	449 72	456 73	463 73	471 74
558.0	478 75	486 76	493 76	501 77	509 78	517 79	525 80	533 80	541 81	549 82
559.0	557 83	565 83	574 84	582 85	591 86	599 87	608 87	617 88	626 89	635 90

560.0	644 91	653 91	662 92	671 93	681 94	690 95	700 95	709 96	719 97	729 98
561.0	738 99	748 100	758 100	768 101	779 102	789 103	799 104	810 105	820 105	831 106
562.0	841 107	852 108	863 109	874 109	885 110	896 111	907 112	918 113	930 114	941 114
563.0	952 115	964 116	976 117	987 118	999 119	1011 120	1023 120	1035 121	1047 122	1060 123
564.0	1072 124	1084 125	1097 125	1110 126	1122 127	1135 128	1148 129	1161 130	1174 131	1187 131

565.0	1200 132	1213 133	1227 134	1240 135	1254 136	1267 137	1281 138	1295 138	1309 139	1323 140
566.0	1337 141	1351 142	1365 143	1379 144	1394 144	1408 145	1423 146	1438 147	1452 148	1467 149
567.0	1482 150	1497 151	1512 152	1527 152	1543 153	1558 154	1574 155	1589 156	1605 157	1620 158
568.0	1636 159	1652 160	1668 160	1684 161	1700 162	1717 163	1733 164	1750 165	1766 166	1783 167
569.0	1799 168	1816 169	1833 169	1850 170	1867 171	1884 172	1902 173	1919 174	1936 175	1954 176

SUCCESS RESERVOIR, TULE RIVER, CALIFORNIA - AREA AND CAPACITY TABLE (SEPT 78)

ELEV FEET	CAP AREA .0	CAP AREA .1	CAP AREA .2	CAP AREA .3	CAP AREA .4	CAP AREA .5	CAP AREA .6	CAP AREA .7	CAP AREA .8	CAP AREA .9
570.0	1972 177	1989 178	2007 179	2025 180	2043 181	2061 181	2079 182	2098 183	2116 184	2134 185
571.0	2153 186	2172 187	2190 188	2209 189	2228 190	2247 191	2266 192	2286 193	2305 194	2324 195
572.0	2344 196	2364 197	2383 198	2403 199	2423 200	2443 200	2463 201	2483 202	2504 203	2524 204
573.0	2544 205	2565 206	2586 207	2606 208	2627 209	2648 210	2669 211	2691 212	2712 213	2733 214
574.0	2755 215	2776 216	2798 217	2820 218	2842 219	2864 221	2886 222	2908 223	2930 224	2953 225
575.0	2975 226	2998 227	3021 228	3043 229	3066 230	3089 231	3113 232	3136 233	3159 234	3183 235
576.0	3206 236	3230 237	3254 238	3278 239	3302 241	3326 242	3350 243	3374 244	3399 245	3423 246
577.0	3448 247	3473 248	3498 249	3523 250	3548 252	3573 253	3598 254	3624 255	3649 256	3675 257
578.0	3701 258	3727 260	3753 261	3779 262	3805 263	3831 264	3858 265	3884 267	3911 268	3938 269
579.0	3965 270	3992 271	4019 272	4046 274	4074 275	4101 276	4129 277	4157 278	4185 280	4213 281
580.0	4241 282	4269 283	4298 285	4326 286	4355 287	4384 288	4412 290	4441 291	4471 292	4500 293
581.0	4529 295	4559 296	4588 297	4618 298	4648 300	4678 301	4708 302	4739 304	4769 305	4799 306
582.0	4830 307	4861 309	4892 310	4923 311	4954 313	4986 314	5017 315	5049 317	5080 318	5112 319
583.0	5144 321	5176 322	5209 323	5241 325	5274 326	5306 328	5339 329	5372 330	5405 332	5438 333
584.0	5472 335	5505 336	5539 337	5573 339	5607 340	5641 342	5675 343	5709 344	5744 346	5779 347
585.0	5813 349	5848 350	5883 352	5919 353	5954 355	5990 356	6025 358	6061 359	6097 360	6133 362
586.0	6170 363	6206 365	6242 366	6279 368	6316 369	6353 371	6390 372	6428 374	6465 375	6503 377
587.0	6540 379	6578 380	6616 382	6655 383	6693 385	6732 386	6770 388	6809 389	6848 391	6887 393
588.0	6927 394	6966 396	7006 397	7046 399	7086 400	7126 402	7166 404	7207 405	7247 407	7288 409
589.0	7329 410	7370 412	7411 413	7453 415	7494 417	7536 418	7578 420	7620 422	7662 423	7705 425

SUCCESS RESERVOIR, TULE RIVER, CALIFORNIA - AREA AND CAPACITY TABLE (SEPT 78)

ELEV FEET	CAP AREA .0	CAP AREA .1	CAP AREA .2	CAP AREA .3	CAP AREA .4	CAP AREA .5	CAP AREA .6	CAP AREA .7	CAP AREA .8	CAP AREA .9
590.0	7747 477	7790 478	7833 430	7876 432	7919 433	7963 435	8006 437	8050 438	8094 440	8138 442
591.0	8182 443	8226 445	8271 447	8316 448	8361 450	8406 452	8451 454	8497 455	8542 457	8588 459
592.0	8634 461	8680 462	8726 464	8773 466	8820 468	8867 469	8913 471	8961 473	9008 475	9056 476
593.0	9103 478	9151 480	9199 482	9248 483	9296 485	9345 487	9393 489	9442 491	9492 492	9541 494
594.0	9590 496	9640 498	9690 500	9740 501	9790 503	9841 505	9891 507	9942 509	9993 511	10044 512
595.0	10096 514	10147 516	10199 518	10251 520	10303 522	10355 524	10407 525	10460 527	10513 529	10566 531
596.0	10619 533	10672 535	10726 537	10780 538	10834 540	10888 542	10942 544	10997 546	11051 548	11106 550
597.0	11161 552	11217 553	11272 555	11328 557	11383 559	11440 561	11496 563	11552 565	11609 567	11665 569
598.0	11722 571	11779 573	11837 574	11894 576	11952 578	12010 580	12068 582	12127 584	12185 586	12244 588
599.0	12303 590	12362 592	12421 594	12480 596	12540 598	12600 600	12660 601	12720 603	12781 605	12841 607
600.0	12902 609	12963 611	13024 613	13086 615	13147 617	13209 619	13271 621	13333 623	13396 625	13458 627
601.0	13521 629	13584 631	13647 633	13711 635	13774 637	13838 639	13902 641	13966 643	14031 645	14095 647
602.0	14160 649	14225 651	14290 653	14355 655	14421 657	14487 659	14553 661	14619 663	14685 665	14752 667
603.0	14819 669	14885 671	14953 673	15020 675	15088 677	15155 679	15223 681	15291 683	15360 685	15428 687
604.0	15497 689	15566 691	15635 693	15704 695	15774 697	15844 699	15914 701	15984 703	16054 705	16125 707
605.0	16196 709	16267 711	16338 713	16409 715	16481 717	16553 719	16624 721	16697 723	16769 725	16842 727
606.0	16914 729	16987 731	17061 733	17134 735	17208 737	17281 739	17355 741	17430 743	17504 745	17579 747
607.0	17654 749	17728 751	17804 753	17879 755	17955 757	18031 759	18107 761	18183 764	18259 766	18336 768
608.0	18413 770	18490 772	18567 774	18645 776	18722 778	18800 780	18878 782	18957 784	19035 786	19114 788
609.0	19193 790	19272 792	19351 794	19431 796	19511 799	19591 801	19671 803	19751 805	19832 807	19912 809

SUCCESS RESERVOIR, TULE RIVER, CALIFORNIA - AREA AND CAPACITY TABLE (SEPT 78)

ELEV FEET	CAP AREA .0	CAP AREA .1	CAP AREA .2	CAP AREA .3	CAP AREA .4	CAP AREA .5	CAP AREA .6	CAP AREA .7	CAP AREA .8	CAP AREA .9
610.0	19994 811	20075 813	20156 815	20238 817	20320 819	20402 821	20484 823	20566 826	20649 828	20732 830
611.0	20815 832	20898 834	20982 836	21065 838	21149 840	21233 842	21318 844	21402 847	21487 849	21572 851
612.0	21657 853	21743 855	21828 857	21914 859	22000 861	22086 863	22173 866	22259 868	22346 870	22433 872
613.0	22521 874	22608 876	22696 878	22784 881	22872 883	22961 885	23049 887	23138 889	23227 891	23316 894
614.0	23406 896	23495 898	23585 900	23675 902	23766 904	23856 907	23947 909	24038 911	24129 913	24221 915
615.0	24312 917	24404 920	24496 922	24588 924	24681 926	24774 929	24867 931	24960 933	25053 935	25147 937
616.0	25241 940	25335 942	25429 944	25524 946	25618 949	25713 951	25809 953	25904 955	26000 958	26096 960
617.0	26192 962	26288 964	26385 967	26481 969	26578 971	26676 974	26773 976	26871 978	26969 981	27067 983
618.0	27165 985	27264 988	27363 990	27462 992	27561 995	27661 997	27761 999	27861 1002	27961 1004	28062 1006
619.0	28162 1009	28263 1011	28365 1014	28466 1016	28568 1018	28670 1021	28772 1023	28874 1026	28977 1028	29080 1030
620.0	29183 1033	29286 1035	29390 1038	29494 1040	29598 1043	29703 1045	29807 1048	29912 1050	30017 1053	30123 1055
621.0	30228 1058	30334 1060	30440 1063	30547 1065	30653 1068	30760 1070	30867 1073	30975 1075	31082 1078	31190 1081
622.0	31299 1083	31407 1086	31516 1088	31625 1091	31734 1094	31844 1096	31953 1099	32063 1101	32173 1104	32284 1107
623.0	32395 1109	32506 1112	32617 1115	32729 1118	32841 1120	32953 1123	33065 1126	33178 1128	33291 1131	33404 1134
624.0	33518 1137	33632 1139	33746 1142	33860 1145	33975 1148	34090 1151	34205 1153	34320 1156	34436 1159	34552 1162
625.0	34669 1165	34785 1168	34902 1171	35019 1173	35137 1176	35255 1179	35372 1182	35491 1185	35609 1188	35728 1191
626.0	35848 1194	35967 1197	36087 1200	36207 1203	36328 1206	36449 1209	36569 1212	36691 1215	36812 1218	36934 1221
627.0	37057 1224	37179 1227	37302 1230	37425 1234	37549 1237	37673 1240	37797 1243	37921 1246	38046 1249	38171 1252
628.0	38297 1256	38422 1259	38548 1262	38675 1265	38801 1269	38929 1272	39056 1275	39184 1278	39311 1282	39440 1285
629.0	39569 1288	39697 1292	39827 1295	39956 1298	40087 1302	40217 1305	40348 1309	40479 1312	40610 1316	40742 1319

SUCCESS RESERVOIR, TULE RIVER, CALIFORNIA - AREA AND CAPACITY TABLE (SEPT 78)

ELEV FEET	CAP AREA .0	CAP AREA .1	CAP AREA .2	CAP AREA .3	CAP AREA .4	CAP AREA .5	CAP AREA .6	CAP AREA .7	CAP AREA .8	CAP AREA .9
630.0	40874 1322	41006 1326	41139 1329	41272 1333	41406 1336	41540 1340	41674 1344	41808 1347	41943 1351	42078 1354
631.0	42214 1358	42350 1361	42486 1365	42623 1369	42760 1372	42897 1376	43035 1380	43173 1383	43312 1387	43451 1391
632.0	43590 1395	43730 1398	43870 1402	44010 1406	44151 1410	44292 1414	44434 1418	44576 1421	44718 1425	44861 1429
633.0	45004 1433	45147 1437	45291 1441	45435 1445	45580 1449	45725 1453	45871 1457	46017 1461	46163 1465	46309 1469
634.0	46457 1473	46604 1477	46752 1481	46900 1485	47049 1489	47198 1493	47348 1498	47498 1502	47648 1506	47799 1510
635.0	47950 1514	48102 1519	48254 1523	48406 1527	48559 1531	48713 1536	48866 1540	49021 1544	49175 1549	49330 1553
636.0	49486 1557	49642 1562	49798 1566	49955 1571	50112 1575	50270 1580	50428 1584	50587 1588	50746 1593	50905 1598
637.0	51066 1602	51226 1607	51387 1611	51548 1616	51710 1620	51872 1625	52035 1630	52198 1634	52362 1639	52526 1644
638.0	52691 1648	52855 1653	53021 1658	53187 1663	53354 1667	53521 1672	53688 1677	53856 1682	54024 1687	54193 1691
639.0	54363 1696	54532 1701	54703 1706	54873 1711	55045 1716	55217 1721	55389 1726	55562 1731	55735 1736	55909 1741
640.0	56084 1746	56258 1751	56434 1756	56609 1761	56786 1766	56963 1771	57140 1776	57318 1781	57496 1786	57675 1792
641.0	57855 1797	58034 1802	58215 1807	58396 1812	58578 1818	58760 1823	58942 1828	59125 1834	59309 1839	59493 1844
642.0	59678 1849	59863 1855	60049 1860	60235 1866	60422 1871	60609 1876	60797 1882	60986 1887	61174 1893	61364 1898
643.0	61554 1904	61745 1909	61936 1915	62127 1920	62320 1926	62513 1931	62706 1937	62900 1942	63094 1948	63290 1954
644.0	63486 1959	63681 1965	63878 1970	64075 1976	64273 1982	64472 1987	64671 1993	64871 1999	65071 2005	65272 2010
645.0	65473 2016	65675 2022	65877 2028	66080 2033	66284 2039	66488 2045	66693 2051	66898 2057	67104 2063	67311 2068
646.0	67518 2074	67726 2080	67934 2086	68143 2092	68352 2098	68563 2104	68773 2110	68985 2116	69196 2122	69409 2128
647.0	69622 2134	69836 2140	70050 2146	70265 2152	70480 2158	70697 2164	70913 2170	71130 2176	71348 2182	71567 2188
648.0	71786 2194	72005 2200	72226 2207	72447 2213	72668 2219	72891 2225	73113 2231	73337 2237	73561 2243	73786 2250
649.0	74011 2256	74237 2262	74463 2268	74690 2274	74918 2281	75147 2287	75375 2293	75605 2299	75835 2306	76066 2312

SUCCESS RESERVOIR, TULE RIVER, CALIFORNIA - AREA AND CAPACITY TABLE (SEPT 78)

ELEV FEET	CAP AREA .0	CAP AREA .1	CAP AREA .2	CAP AREA .3	CAP AREA .4	CAP AREA .5	CAP AREA .6	CAP AREA .7	CAP AREA .8	CAP AREA .9

650.0	76298 2318	76530 2324	76763 2331	76996 2337	77230 2343	77465 2350	77700 2356	77936 2362	78172 2369	78410 2375
651.0	78648 2381	78886 2388	79125 2394	79364 2400	79605 2407	79846 2413	80087 2419	80330 2426	80572 2432	80816 2439
652.0	81061 2445	81305 2451	81551 2458	81797 2464	82043 2471	82291 2477	82539 2483	82788 2490	83037 2496	83287 2503
653.0	83538 2509	83788 2516	84041 2522	84293 2528	84546 2535	84800 2541	85054 2548	85310 2554	85565 2561	85822 2567
654.0	86079 2574	86336 2580	86595 2587	86853 2593	87113 2599	87374 2606	87634 2612	87896 2619	88158 2625	88421 2632

655.0	88685 2638	88949 2645	89214 2651	89479 2658	89745 2664	90012 2671	90279 2677	90548 2684	90816 2690	91085 2697
656.0	91356 2703	91626 2710	91897 2716	92169 2723	92442 2729	92715 2735	92989 2742	93264 2748	93538 2755	93814 2761
657.0	94091 2768	94368 2774	94646 2781	94924 2787	95203 2794	95483 2800	95763 2806	96044 2813	96325 2819	96608 2826
658.0	96891 2832	97174 2839	97459 2845	97743 2852	98029 2858	98315 2864	98602 2871	98889 2877	99177 2884	99466 2890
659.0	99756 2896	100045 2903	100336 2909	100627 2916	100919 2922	101212 2928	101504 2935	101798 2941	102092 2947	102388 2954

660.0	102684 2960	102980 2966	103277 2973	103574 2979	103873 2985	104172 2992	104471 2998	104771 3004	105072 3011	105373 3017
661.0	105676 3023	105978 3030	106281 3036	106585 3042	106890 3048	107195 3055	107500 3061	107807 3067	108114 3073	108422 3080
662.0	108730 3086	109039 3092	109348 3098	109658 3104	109969 3111	110281 3117	110592 3123	110905 3129	111218 3135	111532 3141
663.0	111847 3148	112161 3154	112477 3160	112793 3166	113110 3172	113428 3178	113746 3184	114065 3190	114384 3196	114704 3203
664.0	115025 3209	115346 3215	115668 3221	115990 3227	116313 3233	116637 3239	116961 3245	117286 3251	117611 3257	117937 3263

665.0	118264 3269	118590 3275	118919 3281	119246 3287	119576 3293	119906 3299	120235 3305	120566 3310	120897 3316	121229 3322
666.0	121562 3328	121895 3334	122229 3340	122563 3346	122898 3352	123234 3358	123569 3363	123906 3369	124243 3375	124581 3381
667.0	124920 3387	125258 3392	125598 3398	125938 3404	126279 3410	126620 3416	126962 3421	127305 3427	127647 3433	127991 3439
668.0	128335 3444	128680 3450	129025 3456	129371 3462	129717 3467	130065 3473	130412 3479	130760 3484	131109 3490	131458 3496
669.0	131808 3501	132158 3507	132510 3513	132861 3518	133213 3524	133566 3529	133919 3535	134273 3541	134627 3546	134982 3552

SUCCESS RESERVOIR, TULE RIVER, CALIFORNIA - AREA AND CAPACITY TABLE (SEPT 78)

ELEV FEET	CAP AREA .0	CAP AREA .1	CAP AREA .2	CAP AREA .3	CAP AREA .4	CAP AREA .5	CAP AREA .6	CAP AREA .7	CAP AREA .8	CAP AREA .9
670.0	135338 3557	135693 3563	136050 3569	136407 3574	136765 3580	137124 3585	137482 3591	137842 3596	138201 3602	138562 3607
671.0	138923 3613	139284 3619	139647 3624	140009 3630	140372 3635	140736 3641	141100 3646	141466 3652	141830 3657	142197 3662
672.0	142564 3668	142930 3673	143298 3679	143666 3684	144035 3690	144404 3695	144774 3701	145144 3706	145515 3712	145886 3717
673.0	146259 3722	146631 3728	147004 3733	147377 3739	147752 3744	148127 3749	148501 3755	148878 3760	149253 3766	149631 3771
674.0	150008 3777	150386 3782	150765 3787	151143 3793	151523 3798	151903 3803	152283 3809	152665 3814	153046 3820	153429 3825
675.0	153812 3830	154194 3836	154579 3841	154963 3846	155348 3852	155734 3857	156119 3863	156506 3868	156892 3873	157280 3879
676.0	157669 3884	158057 3889	158447 3895	158836 3900	159226 3905	159618 3911	160008 3916	160401 3922	160792 3927	161186 3932
677.0	161580 3938	161973 3943	162368 3948	162763 3954	163159 3959	163555 3964	163951 3970	164349 3975	164746 3980	165145 3986
678.0	165544 3991	165943 3996	166343 4002	166743 4007	167144 4013	167546 4018	167948 4023	168351 4029	168753 4034	169157 4039
679.0	169562 4045	169966 4050	170372 4055	170777 4061	171184 4066	171591 4071	171998 4077	172406 4082	172814 4088	173223 4093
680.0	173633 4098	174043 4104	174454 4109	174865 4114	175277 4120	175689 4125	176101 4130	176515 4136	176928 4141	177343 4146
681.0	177758 4152	178173 4157	178590 4162	179005 4168	179423 4173	179841 4178	180258 4184	180677 4189	181096 4194	181516 4199
682.0	181937 4205	182357 4210	182778 4215	183200 4221	183622 4226	184046 4231	184468 4236	184893 4242	185316 4247	185742 4252
683.0	186168 4257	186593 4262	187020 4268	187446 4273	187874 4278	188303 4283	188731 4288	189160 4293	189589 4298	190020 4303
684.0	190451 4309	190881 4314	191313 4319	191745 4324	192178 4329	192611 4334	193044 4339	193479 4344	193913 4348	194348 4353
685.0	194784 4358	195220 4363	195656 4368	196093 4373	196531 4377	196969 4382	197407 4387	197846 4392	198285 4396	198725 4401
686.0	199166 4405	199606 4410	200048 4414	200489 4419	200932 4423	201375 4428	201817 4432	202261 4436	202704 4441	203149 4445
687.0	203594 4449	204038 4453	204484 4457	204929 4461	205376 4465	205823 4469	206270 4473	206718 4477	207165 4481	207614 4484
688.0	208063 4488	208511 4491	208961 4495	209410 4498	209860 4502	210311 4505	210761 4508	211212 4511	211663 4514	212115 4517
689.0	212567 4520	213019 4523	213472 4526	213924 4528	214377 4531	214831 4533	215284 4536	215738 4538	216191 4540	216646 4542

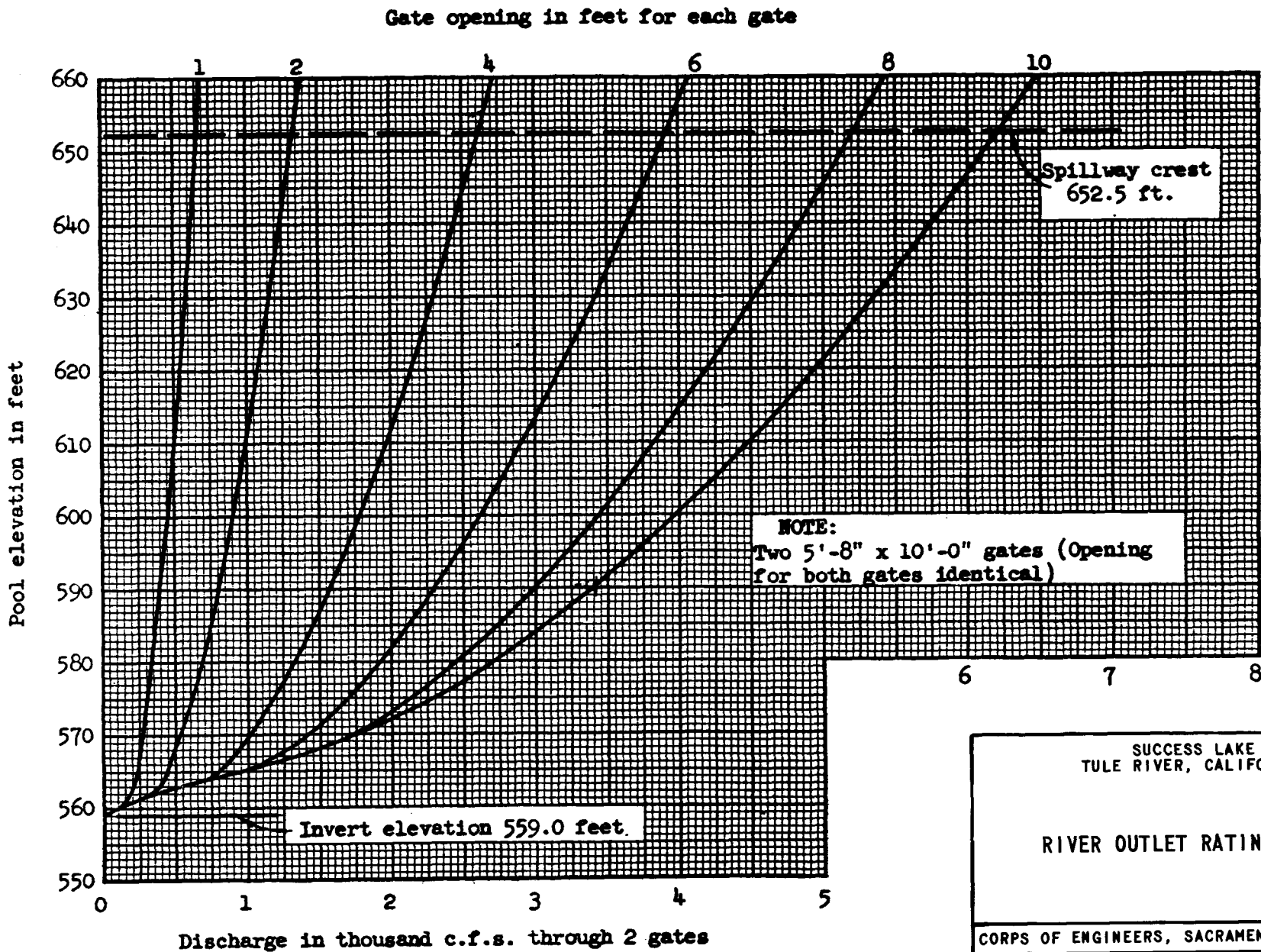


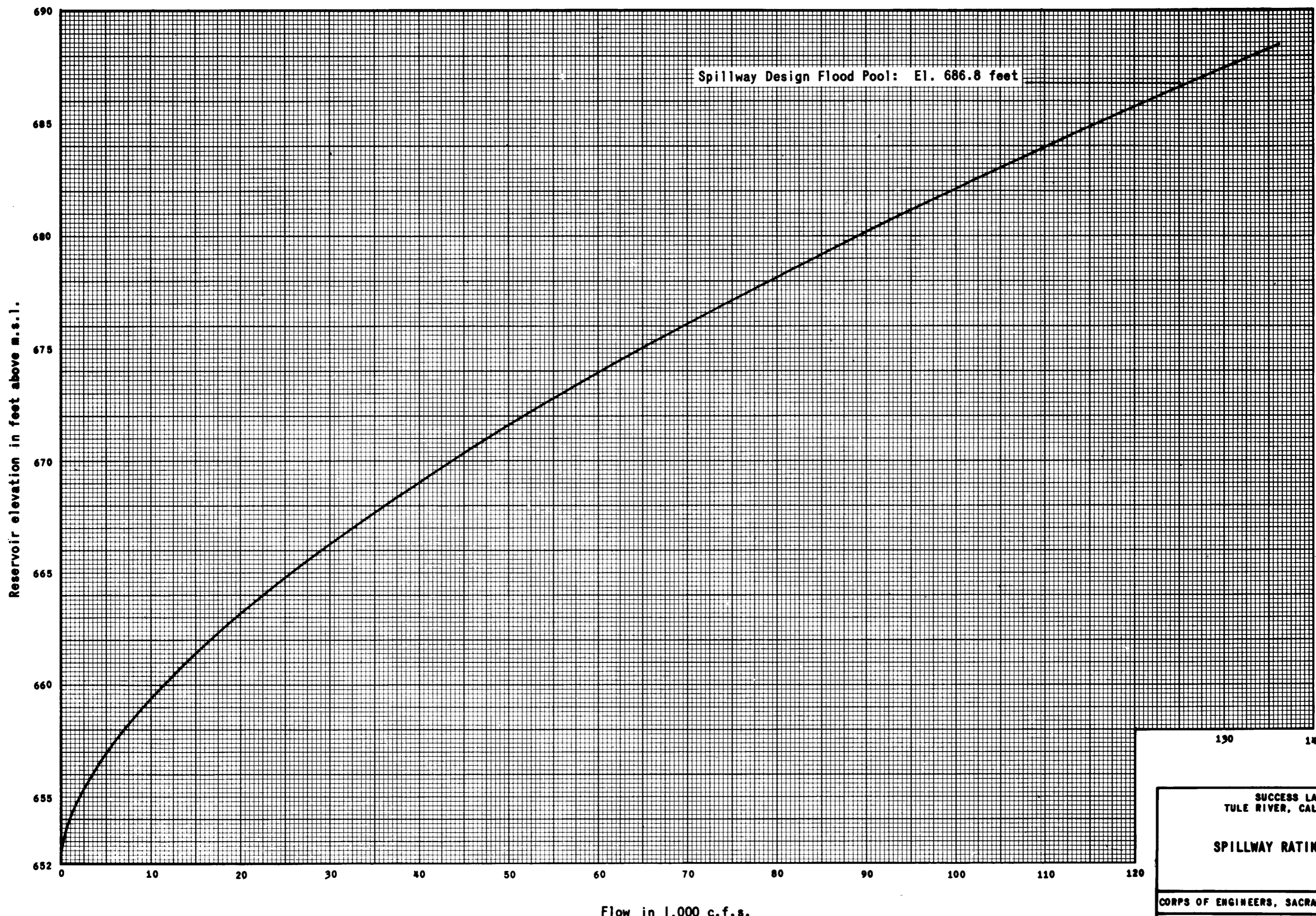
PLATE A-3

SUCCESS LAKE
TULE RIVER, CALIFORNIA

RIVER OUTLET RATING CURVE

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

Prepared: R.E.F. Date: APRIL 1961



Spillway Design Flood Pool: El. 686.8 feet

Reservoir elevation in feet above m.s.l.

Flow in 1,000 c.f.s.

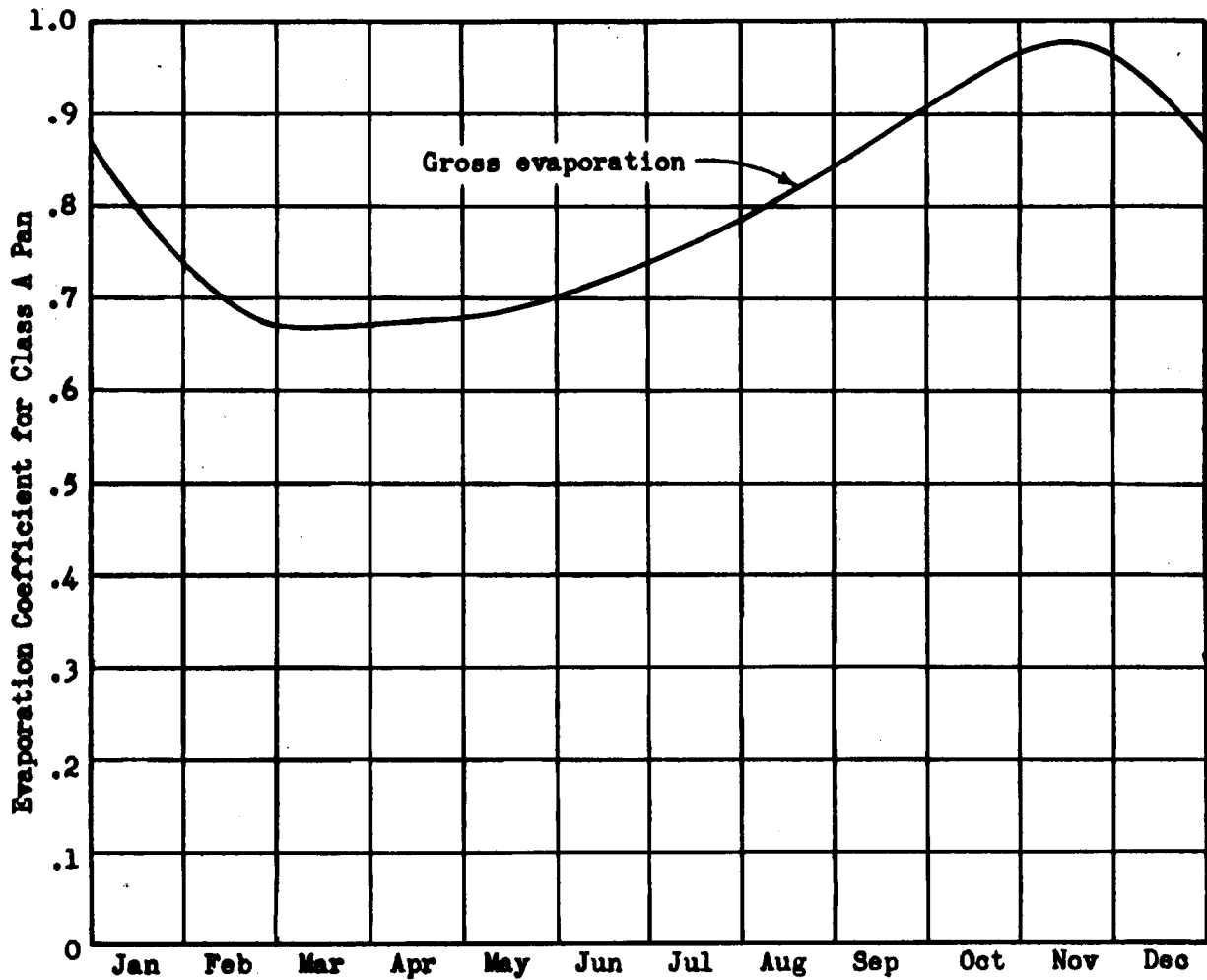
SUCCESS LAKE
TULE RIVER, CALIFORNIA

SPILLWAY RATING CURVE

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

Prepared: D.D.D. Date: JULY 1986

Drawn:



**AVERAGE MONTHLY
EVAPORATION COEFFICIENTS**

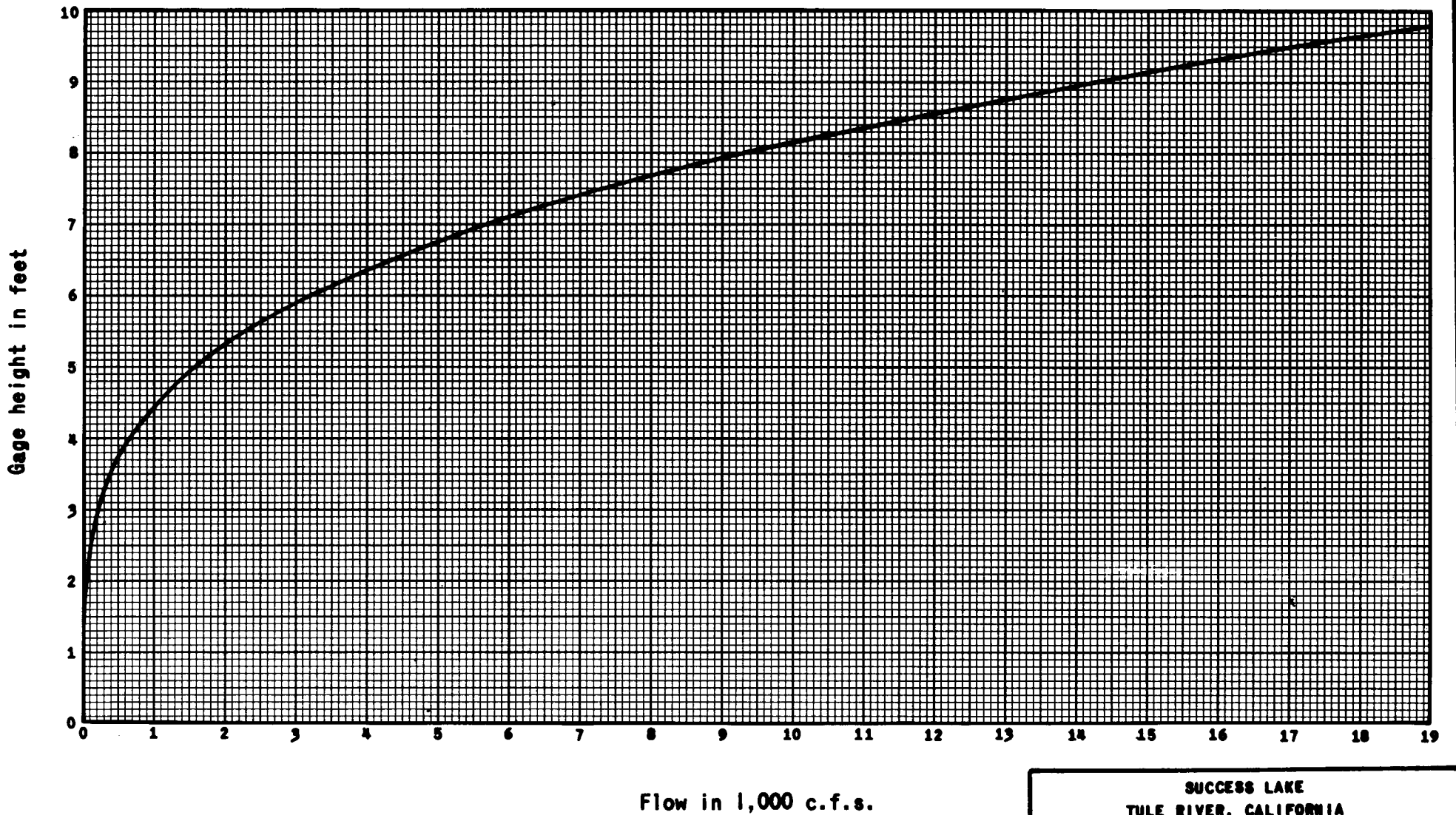
Jan	0.804	Jul	0.768
Feb	0.696	Aug	0.816
Mar	0.672	Sep	0.876
Apr	0.672	Oct	0.936
May	0.684	Nov	0.960
Jun	0.720	Dec	0.924

**SUCCESS LAKE
TULE RIVER, CALIFORNIA**

EVAPORATION COEFFICIENTS

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

Prepared: L.R.B. Date: SEPTEMBER 1955



SUCCESS LAKE
TULE RIVER, CALIFORNIA

DISCHARGE RATING CURVE

TULE RIVER NEAR SPRINGVILLE

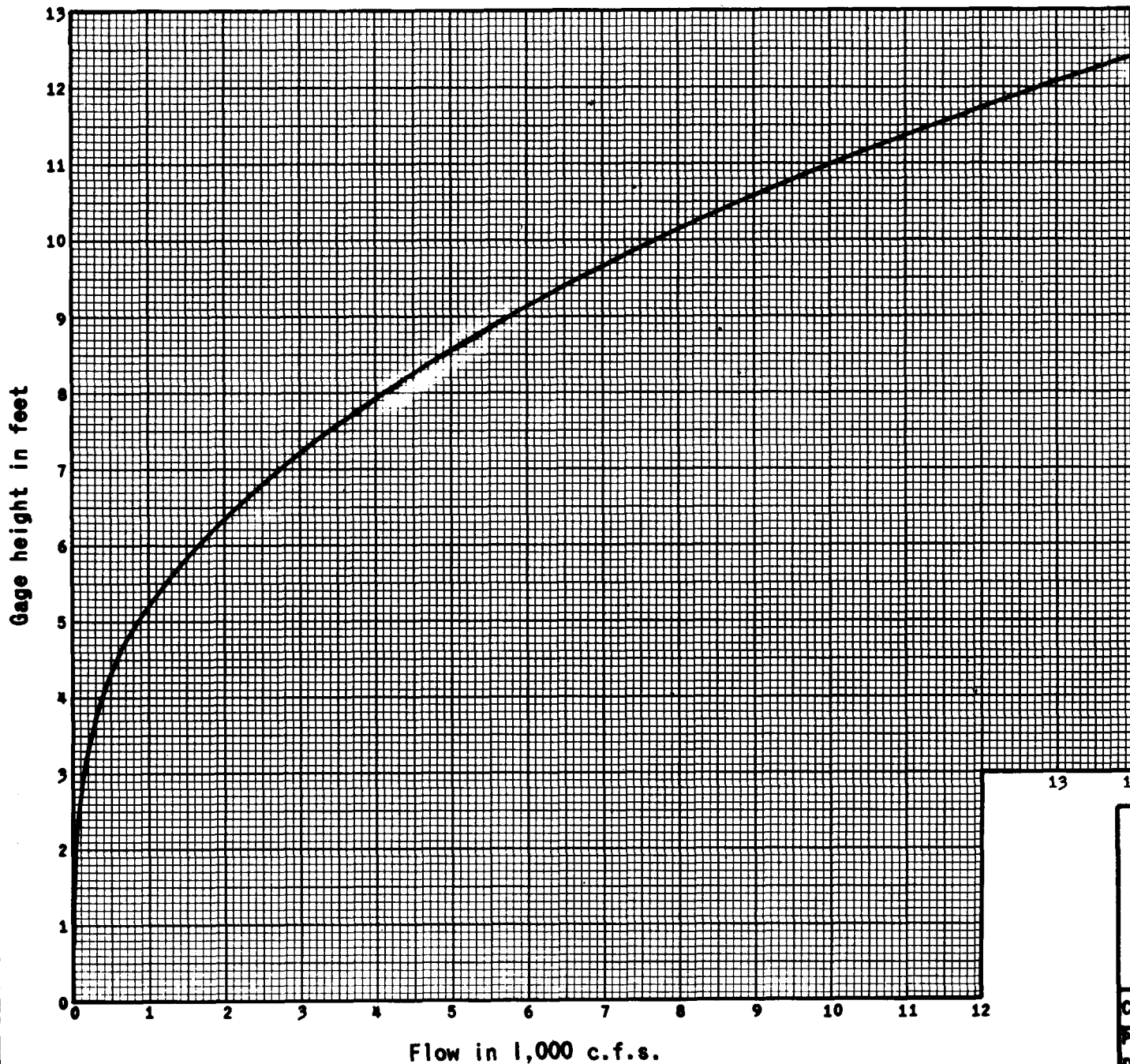
CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

Prepared: L.H.C.

Date: JULY 1980

Drawn: L.H.C.

From U.S.G.S. rating tables No. 12 and 13 printed 22 February 1980 and 18 June 1980 respectively.



From U.S.G.S. rating table No. 16
printed 18 June 1980.

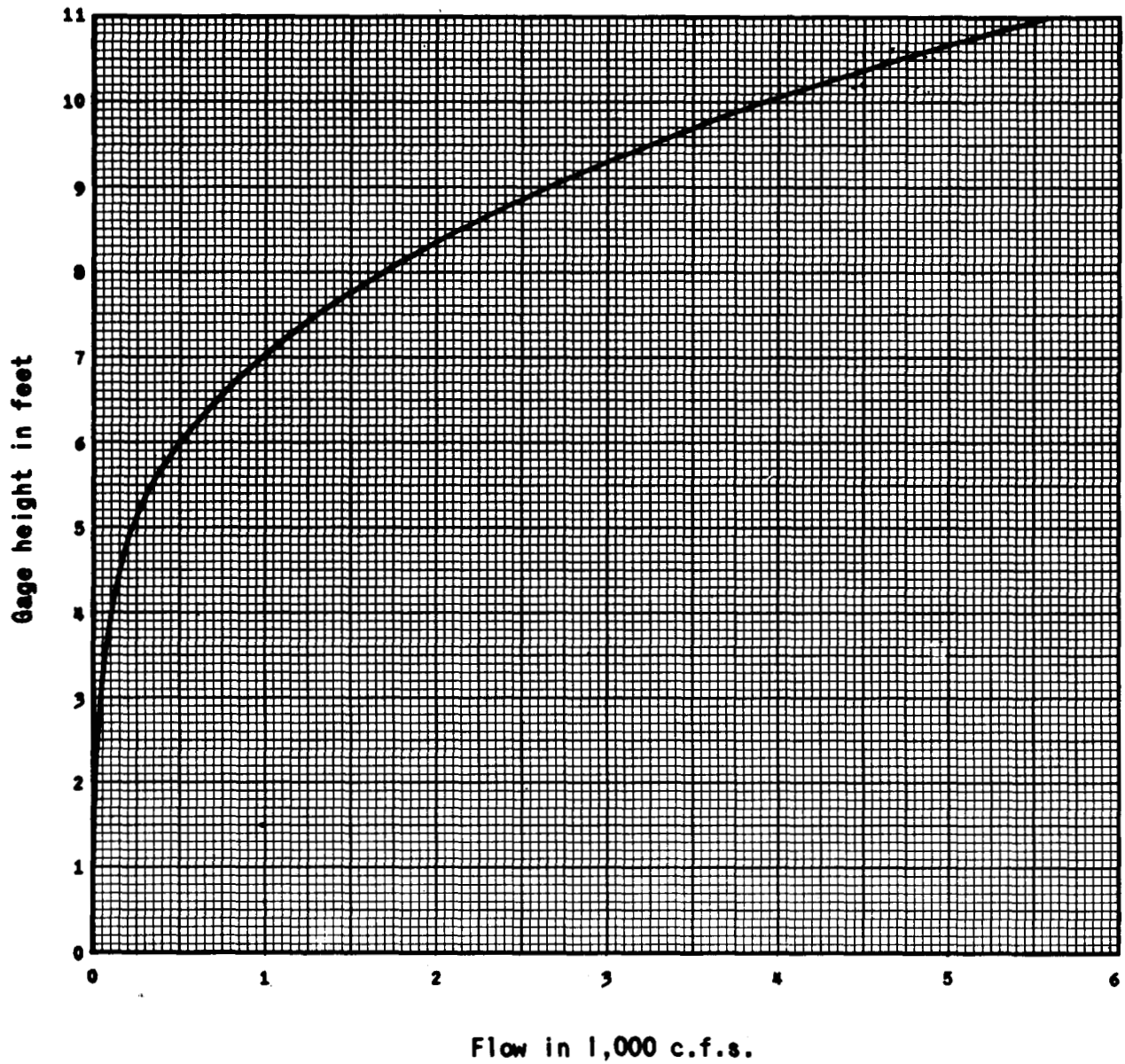
SUCCESS LAKE
TULE RIVER, CALIFORNIA

DISCHARGE RATING CURVE

SOUTH FORK TULE RIVER NEAR SUCCESS

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

Prepared: L.H.C. Date: JULY 1980
Drawn: L.H.C.



From U.S.G.S. rating table No. 8
 printed 18 June 1980.

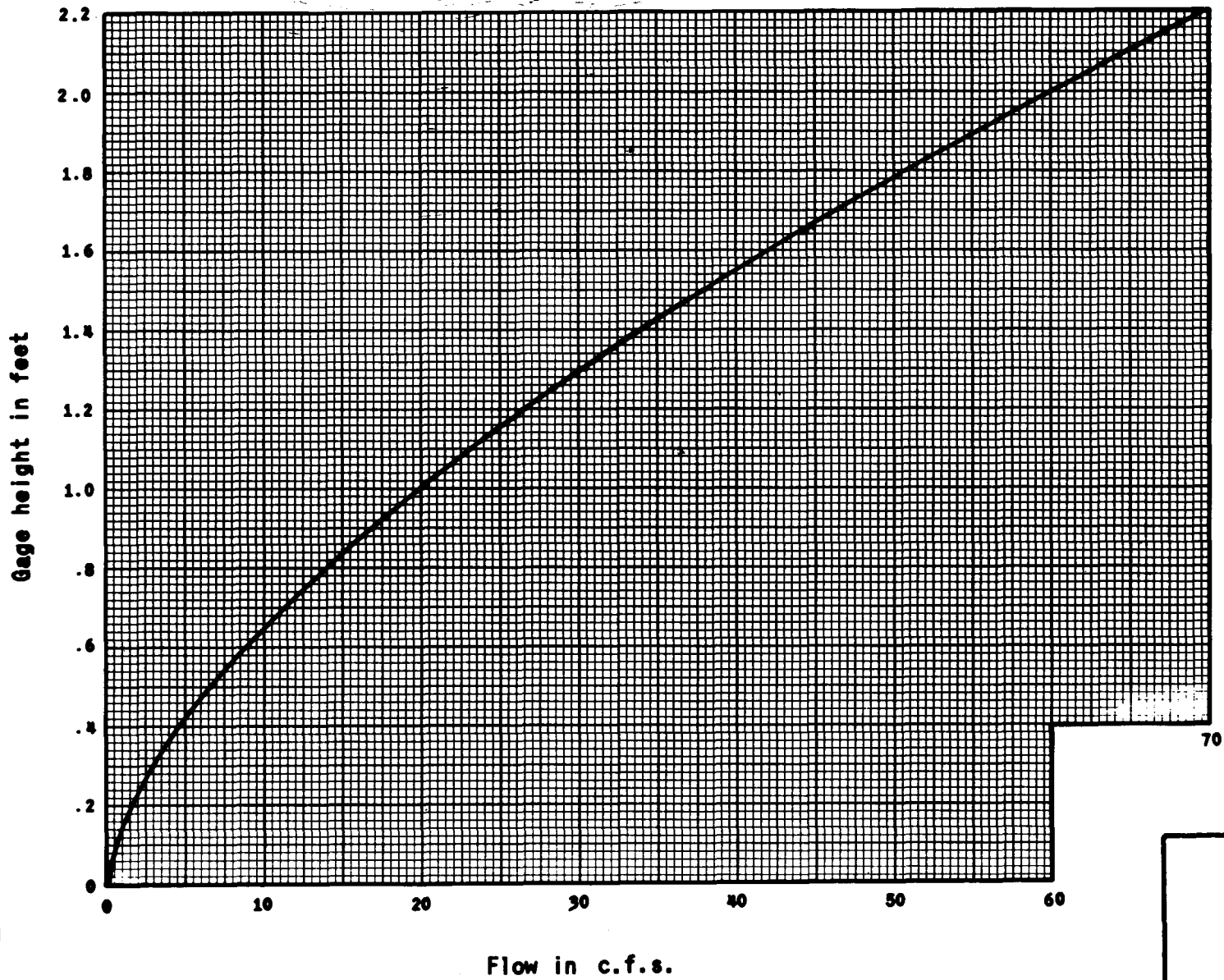
**SUCCESS LAKE
 TULE RIVER, CALIFORNIA**

DISCHARGE RATING CURVE

TULE RIVER BELOW SUCCESS DAM

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

Prepared: L.H.C. Date: JULY 1980
 Drawn: L.H.C.



SUCCESS LAKE
TULE RIVER, CALIFORNIA

DISCHARGE RATING CURVE

PIONEER DITCH

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

Prepared: L.H.C.

Date: APRIL 1980

Drawn: L.H.C.

From U.S.G.S. rating table No.2 printed 18 June 1980.

SHEET 4 OF 4 PLATE A-6

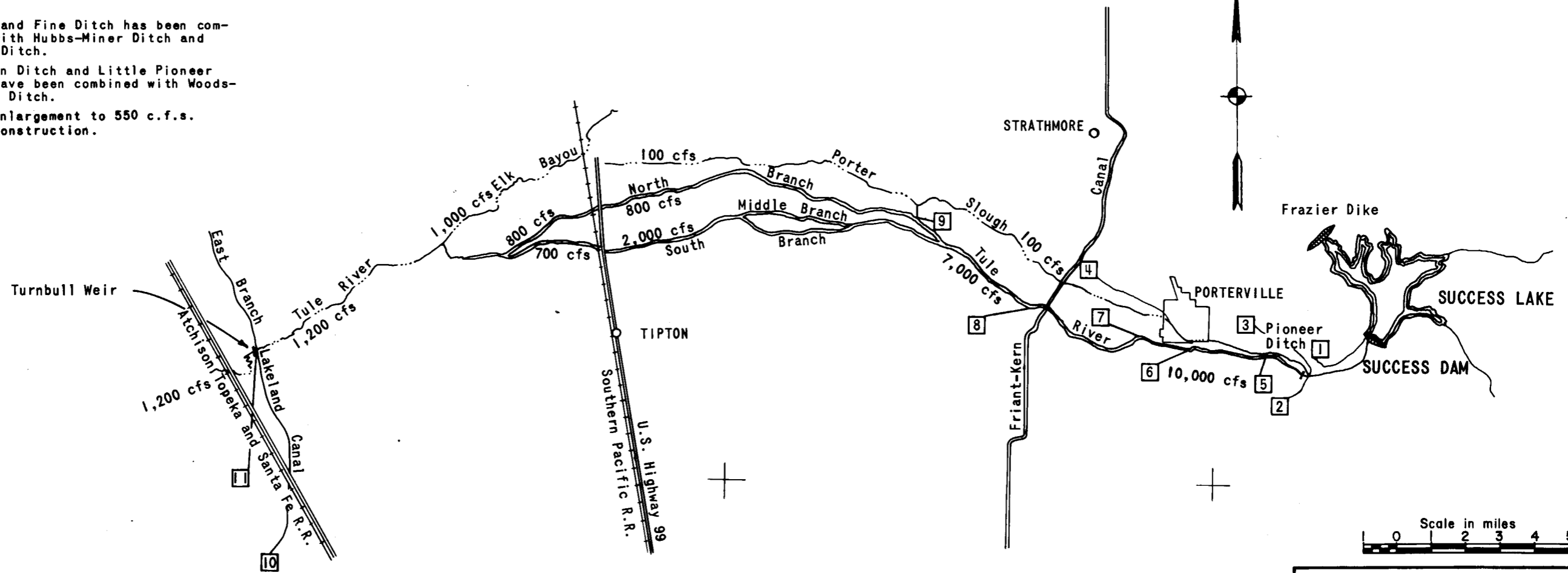
DIVERSIONS AND CAPACITIES

CANAL OR DITCH	CAPACITY (c. f. s.)
1 Pioneer Ditch	35
2 Campbell-Moreland	30
3 Porter Slough	180
4 Porter Slough Ditch	20
5 Vandalia Ditch	9
6 Poplar Ditch	150
7 Hubbs-Miner Ditch	25
Rhodes and Fine Ditch	a/
8 Woods-Central Ditch (Woods-Central Canal)	250
Stockton Ditch	b/
Little Pioneer Ditch	b/
9 North Canal	300
SUBTOTAL	999
10 East Branch Lakeland Canal	c/ 300
11 Taylor Ditch	65
GRAND TOTAL	1,364

a/ Rhodes and Fine Ditch has been combined with Hubbs-Miner Ditch and Poplar Ditch.

b/ Stockton Ditch and Little Pioneer Ditch have been combined with Woods-Central Ditch.

c/ Canal enlargement to 550 c.f.s. under construction.



SUCCESS LAKE
TULE RIVER, CALIFORNIA

DOWNSTREAM CHANNEL CAPACITIES

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA

Prepared: L.H.C. Date: MAY 1981

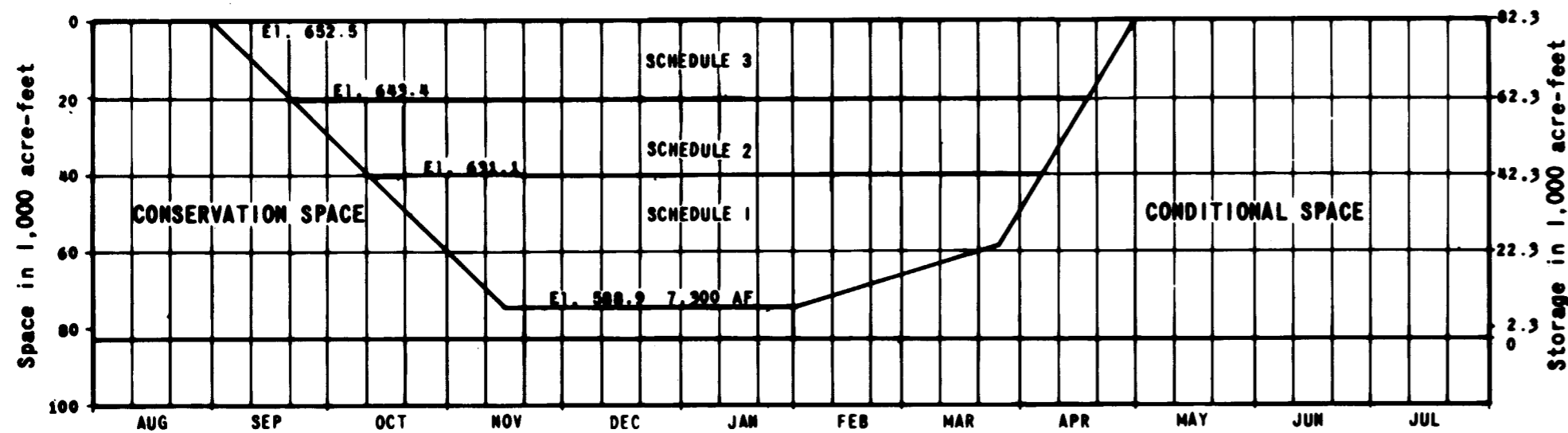


FIGURE 1

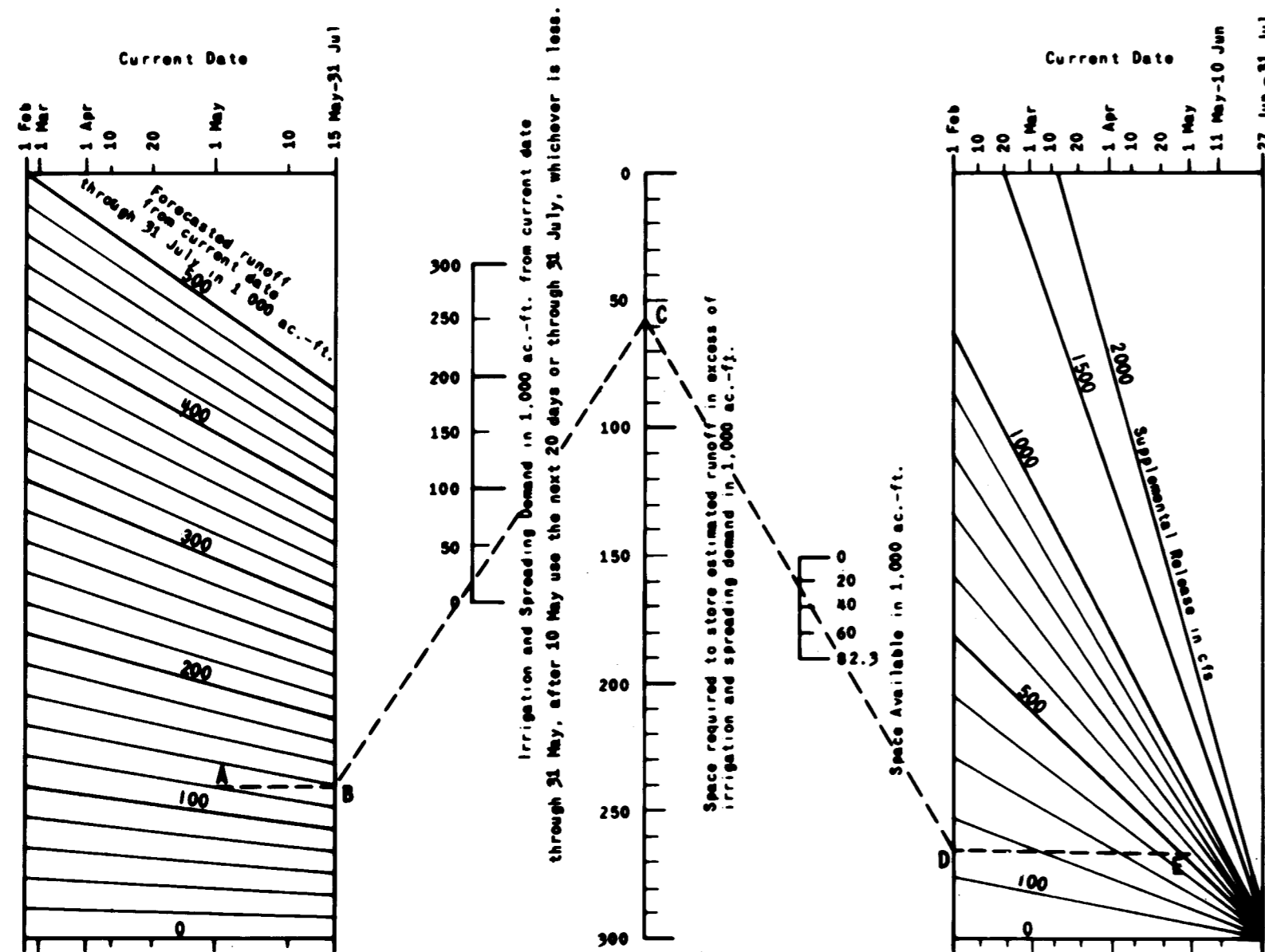


FIGURE 2

USE OF DIAGRAM

1. Water stored in conservation space will be released as requested by the Tule River watermaster.
2. Water stored in Schedule 1, 2 or 3 space will be released in accordance with the schedule that applies to that space.
3. Schedule 1 releases may be deferred temporarily during the rainfall period 11 November through 27 March to allow storage of 3,200 acre-feet in schedule 1 space, subject to the following. The limit on storage (S) in schedule 1 space will be dependent on the basin wetness parameter (Par) and will vary incrementally from 3,200 acre-feet when Par is 2 inches or less, to 0 acre-feet when Par is 6 inches or more. Values of Par and S are shown in tabular form below. The computation of Par is discussed in Exhibit A paragraph 3f.

Basin Wetness Parameter (Par) (inches)	Storage (S) (acre-feet)
Less than 2.00	3,200
2.01 to 3.00	2,800
3.01 to 4.00	2,000
4.01 to 5.00	1,000
5.01 to 6.00	400
More than 6.00	0

Calculation of Par will begin with Par = 0 at midnight on 31 August of each year.

4. Water stored in conditional space that is required for flood control must be released as a supplemental release in addition to releases for irrigation and spreading. The conditional space required for flood control is equal to the space required to store estimated runoff in excess of demand for irrigation and spreading. The space and supplemental release can be determined from figure 2.
5. Estimates of future inflow, for release computations, will be made by the Corps of Engineers.
6. The Corps of Engineers may direct that flood control space and releases be increased or decreased from those required by this diagram based on conditions prevailing at the time.

SCHEDULE 1

Water stored in schedule 1 space will be released at the lesser of A, B, C or D below.

SCHEDULE 2

Water stored in schedule 2 space will be released at the lesser of C or D below.

SCHEDULE 3

Water stored in schedule 3 space will be released in accordance with D below or at a lesser rate determined by the Corps of Engineers.

- A. The estimated release which will evacuate the encroachment plus inflow within the next 5 days. The estimated release shall be maintained for five days unless the desired stage is achieved in less time or inflow is greater than anticipated and a greater release is required.
- B. The release required to provide a quantity of water arriving at Turnbull Weir no greater than the quantity of water requested by the Tule Lake interests for irrigation, spreading and flood control.
- C. The "base release" from figure 3 plus the estimated average inflow for the next 5 days. The computed release shall be maintained for 5 days unless the desired stage is achieved in less time or inflow is greater than anticipated and a greater release is required.
- D. The "maximum release" specified in figure 3.

SAMPLE CONDITIONAL SPACE COMPUTATION

Given Data:

Date.....1 May
 Forecasted runoff from 1 May through 31 July.....120,000 acre-feet
 Forecasted irrigation and spreading demand from 1 May through 31 May.....18,450 acre-feet
 Irrigation and spreading demand on 1 May.....250 c.f.s.
 Space available in Success Lake.....25,000 acre-feet

Computation of Space Required to Store Runoff Exceeding Irrigation and Spreading Demand:

Enter Figure 2 at "A" with current date (1 May) and forecasted runoff from current date through 31 July (120,000 acre-feet) and move horizontally to "B".

From "B" extend a line through the irrigation and spreading demand (18,450 acre-feet) to "C" and read the space required to store the runoff exceeding irrigation and spreading demand (57,600 acre-feet).

Computation of Supplemental Release:

Extend a line from "C" through the space available (25,000 acre-feet) to "D".

From "D" move horizontally to "E" below the current date (1 May) and read the supplemental release (550 c.f.s.).

Computation of Total Release:

Add the supplemental release (550 c.f.s.) to the irrigation and spreading release (250 c.f.s.) to get a total release of 800 c.f.s..

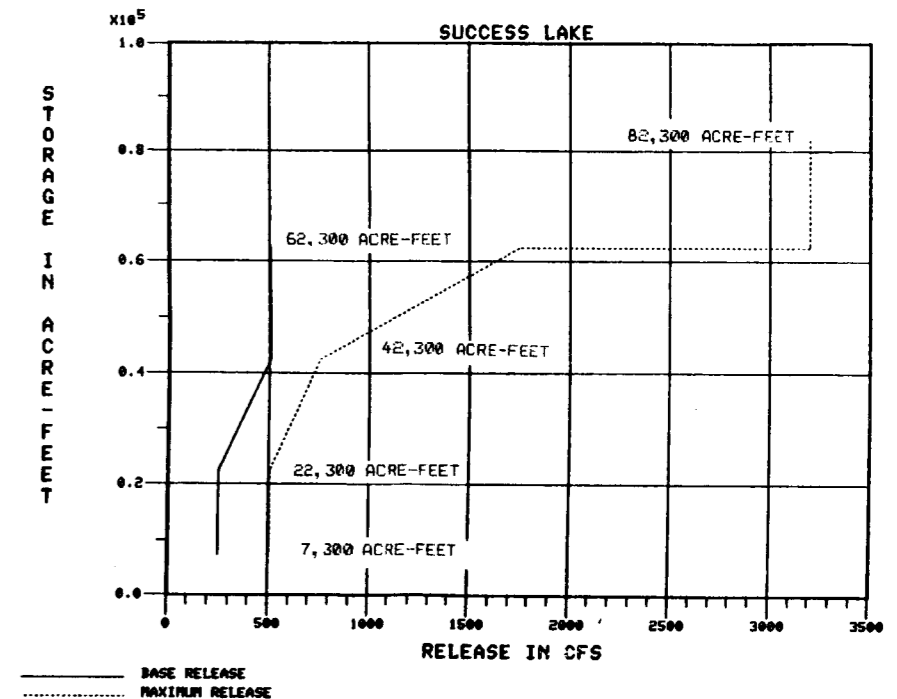


FIGURE 3

**SUCCESS LAKE
TULE RIVER, CALIFORNIA**

FLOOD CONTROL DIAGRAM

CORPS OF ENGINEERS, SACRAMENTO, CALIFORNIA
 Prepared: N.T.M., M.E.V. Date: JULY 1981
 Drawn: L.H.C.